

## Stormwater Division

#### MEMORANDUM

**DATE:** 

March 11, 2010

TO:

Michael J. Gillis, Virginia Correctional Enterprises Document Management Services

FROM:

Jo Anna Ripley, Stormwater

PO:

270712

RE:

Files Approved for Scanning

**Box** 18

Y

General File ID or BMP ID:

PC203

**PIN:** 3831800001

Subdivision, Tract, Business or Owner

Name (if known):

News Company LLC

**Property Description:** 

Windsormeade Marketplace

**Site Address:** 

4900 Monticello Ave

(For internal use only)

Drawer: N/A

Agreements: (in file as of scan date)

Book or Doc#:

040021396

Page:

809

797

Comments

Get Last BMP No	EMERG ACTION PLAN	MAINT AGREEMENT		OWNER PHONE	CITY-STATE-ZIP CODE	OWNER ADDRESS 2	OWNER ADDRESS	OWNED ADDRESS	CURRENT OWNER	CITY-STATE	FACILITY LOCATION	PROJECT NAME	CONSTRUCTION DATE	PIN NO	TAX PARCEL	PLAN NO	BMP ID NO	WATERSCHED	Created By:	Date Record Created:
Return to Menu	No.	Yes		804-320-7600	E 23235	Suite 110	9211 Forest Hill Ave		SLN Williamsburg Associates, LCC	Williamsburg, VA	4900 Monticello Ave & Windsor Meade Way	WindsorMeade Marketplace		3831800001	(38-3)(1-2)(38-4)	SP-150-03	203	0		
							cal fact		is, LCC		dsor Meade Way					2:57:29 PM	Thursday, March 11, 2010	PRINTED ON		WS_BMPNO: Print
	GEOTECH REPORT	SW/FLOOD CONTROL	CHAN PROT VOL acre-ft	CHAN PROT CTRL	WTR QUAL VOL acre-ft	EXT DET-WQ-CTRL	RECV STREAM	IMPERV AREA acres	SERVICE AREA DESCRI			SVC DRAIN AREA acres			POINT VALUE	JCC B	old BMP TYP	LAND USE	SITE AREA acre	MAINTENANCE PLAN
	Yes	No		No		No LAS	Powhatan Creek Watershed	15.53	I Parking Lot and green space			20.9				A3 Wet ED Pond	Wet Pond	Commerical Retail	31.44	Yes
<b>K</b> .		BMP #1.	MISC/COMMENTS	HISCOOMMENTS	INTERNAL RATING	LAST INSP DATE 11/5/2007	Vatershed	CONSTR CERTIF	een space	REC DRAWING	10-YR OUTFLOW cfs	2-YR OUTFLOW cfs	PERM POOL ELEV	DESIGN HW ELEV	EMERG SPILLWAY		OTLT BARRL SIZE inch	OTLT BARRL DESC	CTRL STRUC SIZE inches	CTRL STRUC DESC
	All Sales			, market	4	inspected by:		Yes		Yes	25.80	0.35	77.45	83.70	Yes		36	RCP	es 48	RCP Riser



#### COUNTY OF JAMES CITY, VIRGINIA

#### **DECLARATION OF COVENANTS**

#### INSPECTION/MAINTENANCE OF DRAINAGE SYSTEM

THIS DECLARATION, made this // day of Au Gust, 2004 between C.C. CASEY LIMITED COMPANY, a Virginia limited liability company, and all successors in interest ("COVENANTOR(S)"), owner(s) of the following property: Intersection of WindsorMeade Way & Monticello Avenue – 4800 thru 4970 Monticello Ave.

Street Address: preliminary addresses established for WindsorMeade Marketplace
Legal Description: New Town West - See attached Exhibit "A" (the "Property")
Project Name: WindsorMeade Marketplace, Site Plan JCC #SP-150-03 dated 7-9-04 (the "Plan")
Document No.: see Exhibit "A", Deed Book: see Exhibit "A", Page No.: see Exhibit "A"
Instrumetn No.: see Exhibit "A", and the County of James City, Virginia ("COUNTY").

#### WITNESSETH:

We, the COVENANTOR(S), with full authority to execute deeds, mortgages, other covenants, and all rights, titles and interests in the property described above, do hereby covenant with the COUNTY as follows:

- 1. The COVENANTOR(S) shall provide maintenance for the drainage system shown on the Plan, including any runoff control facilities, conveyance systems and associated easements, hereinafter referred to as the "SYSTEM," located on and serving the above-described property to ensure that the SYSTEM is and remains in proper working condition in accordance with approved design standards, and with the law and applicable executive regulations. The SYSTEM shall not include any elements located within any Virginia Department of Transportation rights-of-way.
- 2. If necessary, the COVENANTOR(S) shall levy regular or special assessments against all present or subsequent owners of property served by the SYSTEM to ensure that the SYSTEM is properly maintained.
- 3. The COVENANTOR(S) shall provide and maintain perpetual access from public right-of-ways to the SYSTEM for the COUNTY, its agent and its contractor.
- 4. The COVENANTOR(S) shall grant the COUNTY, its agent and its contractor a right of entry to the SYSTEM for the purpose of inspecting, operating, installing, constructing, reconstructing, maintaining or repairing the SYSTEM.
- 5. If, after reasonable notice by the COUNTY, the COVENANTOR(S) shall fail to maintain the SYSTEM in accordance with the approved design standards and with the law and applicable executive regulations, the COUNTY may perform all necessary repair or maintenance work, and the COUNTY may assess the COVENANTOR(S) and/or all property served by the SYSTEM for the cost of the work and any applicable penalties.

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1-595009.2 08/04/2004

Instrument # 040021396 Ricarded on acig. 23, 2004

- 6. The COVENANTOR(S) shall indemnify and save the COUNTY harmless from any and all claims for damages to persons or property arising from the installation, construction, maintenance, repair, operation or use of the SYSTEM.
- 7. The COVENANTOR(s) shall promptly notify the COUNTY when the COVENANTOR(s) legally transfers any of the COVENANTOR(s) responsibilities for the SYSTEM. The COVENANTOR(s) shall supply the COUNTY with a copy of any document of transfer, executed by both parties. COVENANTOR(s) contemplate conveying the Property to SLN Casey Associates, L.L.C. (the "Shopping Center Owner"), the developer of the shopping center to be built per the Plan, on which the SYSTEM is to be constructed. Anything herein to the contrary notwithstanding, in the event that the COVENANTOR(s) provides the COUNTY with a deed conveying to the Shopping Center Owner the Property, which deed is executed by both COVENANTOR(s) and the Shopping Center Owner and confirms the assumption of the maintenance responsibilities for the SYSTEM by the Shopping Center Owner, COVENANTOR(s) and its successors and assigns (other than the Shopping Center Owner and the Shopping Center Owner's successors in title to the Property), shall be released from any liabilities and obligations under this Declaration which accrue subsequent to the assumption by the Shopping Center Owner of the maintenance responsibilities of the SYSTEM.
- 8. The covenants contained herein shall run with the land and shall bind the COVENANTOR(S) and the COVENANTOR(S)' heirs, executors, administrators, successors and assignees, and shall bind all present and subsequent owners of property served by the SYSTEM.
  - 9. This COVENANT shall be recorded in the County Land Records.

IN WITNESS WHEREOF, the COVENANTOR(S) have executed this DECLARATION OF COVENANTS as of the date first above written.

COVENANTOR(S)

C. CASEY LIMITED COMPANY

Robert T. Casey, Secretary

ATTEST

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COMMONWEALTH OF VIRGINIA (	
CITY/COUNTY OF James City	
I hereby certify that on this // day of <u>Aug</u> Notary Public of the State of <u>Virginia</u>	with, 2004, before the subscribed, a
Notary Public of the State of Wiginia	, and for the <del>City</del> /County of
, aforesaid personally appear	ed Robert T. Casey, Secretary of C.C.
Casey Limited Company and did acknowledge the foregoi	ng instrument to be their Act.
	114
IN WITNESS WHEREOF, I have hereunto set my Ougust, 2004	hand and official seal this /// day of
august , 2004	
	Internal Detistra
Not	Pary Public
1100 000E	ary Tubile
My Commission expires: My Commission Expires April 30, 2005	
	The state of the s
Approved as to form:	
1	

This Declaration of Covenants prepared by:

James M. Gresock Senior Vice President S.L. Nusbaum Realty Co. 9211 Forest Hill Avenue, Suite 110 Richmond, VA 23235 804/320-7600

drainage.pre

County Attorney

#### **EXHIBIT A**

#### Description of the Property

All those certain lots, parcels or tracts of land, situate and lying in the Powhatan District of James City County, Virginia, containing a total of 34.48 acres more or less and being the same properties designated as a portion of James City County Tax Map Parcels #(38-3)(1-2), #(38-3)(1-5), #(38-3)(1-6), (38-3)(1-7), #(38-3)(1-8), and a Portion of Tax Map Parcel #(38-3)(1-34);

Said parcels are more particularly described by metes and bounds as follows:

All of James City County Tax Map Parcels #(38-3)(1-2), #(38-3)(1-5), #(38-3)(1-6), (38-3)(1-7), #(38-3)(1-8) and a Portion of Tax Map Parcel #(38-3)(1-34) Owned by C. C. Casey Limited Company:

Beginning at a point on the northerly right-of-way line of Monticello Avenue Extended, State Route #321, said point being \$28°41'04"W, 358.65' from the intersection of the westerly right-ofway line of State Route #199 and the northerly right-of-way line of said Monticello Avenue Extended, State Route #321, a corner to the property described hereon and the property now or formerly standing in the name of the Commonwealth of Virginia; thence leaving said corner of the property now or formerly standing in the name of the Commonwealth of Virginia and lying along the right-of-way line of Monticello Avenue Extended, State Route #321, S46°23'51"W, 530.33' to a point; thence along a curve to the right, having a radius of 869.93' and an arc length of 91.40' to a point; said point being at the intersection of the northerly right-of-way line of said Monticello Avenue Extended, State Route #321 and the easterly right-of-way line of what is now known as Old News Road; thence leaving said right-of-way line of Monticello Avenue Extended, State Route #321 and lying along the easterly right-of-way line of what is now known as Old News Road, N34°54'22"W, 480.33' to a point; thence N33°17'29"W, 275.90' to a point; thence along a curve to the left, having a radius of 400.00' and an arc length of 62.99' to a point; thence N42°18'49"W, 9.79' to a point; thence along a curve to the left, having a radius of 251.53' and an arc length of 40.04' to a point; said point being a corner to the properties described hereon and the remaining portion of James City Tax Map Parcel #(38-3)(1-34) now or formerly standing in the name of C. C. Casey Limited Company; thence along the line of the remaining portion of James City Tax Map Parcel #(38-3)(1-34) now or formerly owned by C. C. Casey Limited Company and an existing 40' private right-of-way, N43°12'19"E, 178.71' to a point; thence leaving said 40' private right-of-way and continuing along the line of the remaining portion of James City County Tax Map Parcel #(38-3)(1-34), now or formerly owned by C. C. Casey Limited Company, N36°30'08"W, 123.42' to a point; thence along a curve to the right, having a radius of 790.50' and an arc length of 214.79' to a point; thence along a curve to the right, having a radius of 587.50' and an arc length of 101.13' to a point; thence N11°04'18"W, 34.77' to a point; thence along a curve to the right, having a radius of 787.50' and an arc length of 246.68' to a point; thence along a curve to the right, having a radius of 1387.50' and an arc length of 46.69' to a point; thence N89°13'21"E, 746.48' to a point; thence N63°40'56"E, 565.00' to a point on the westerly right-of-way line of State Route #199, a corner to the properties described hereon and the remaining portion of James City County Tax Map Parcel #(38-3)(1-34) now or formerly owned by C. C. Casey Limited Company; thence leaving said corner

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of the remaining portion of James City Tax Map Parcel #(38-3)(1-34) now or formerly standing in the name of C. C. Casey Limited Company and lying along the westerly right-of-way line of State Route #199, S08°18'36"E, 171.61' to a point; thence S04°50'02"W, 654.04' to a point; thence along a curve to the left, having a radius of 903.51' and an arc length of 235.65' to a point, said point being a corner to the property described hereon, the property now or formerly standing in the name of the Commonwealth of Virginia and the intersection of the right-of-way line State Route #199 and Monticello Avenue Extended, State Route #321; thence along the line of the property now or formerly owned by the Commonwealth of Virginia, S28°41'04"W, 358.65' to the aforesaid point of beginning. The properties described above contain an aggregate area of 34.13 acres more or less.

#### And the following parcel:

Beginning at a point at the intersection of the westerly right-of-way line of State Route #199 and the northerly right-of-way line of Monticello Avenue Extended, State Route #321; thence lying along the northerly right-of-way line of said Monticello Avenue Extended, State Route #321, S46°23'51"W, 276.71' to a point, a corner to the property described hereon and the properties now or formerly owned by C. C. Casey Limited Company; thence leaving said corner of the properties now or formerly owned by C. C. Casey Limited Company and lying along the property owned by the Commonwealth of Virginia, N28°41'04"E, 358.65' to a point, said point being on the westerly right-of-way line of State Route #199; thence lying along the westerly right-of-way line of State Route #199, S13°36'06"E, 71.92' to the aforesaid point of beginning. The property described hereon contains an area of 0.35 acres more or less.



# Windsormeade Marketplace James City County Environmental

December 29, 2003

SP-150-03

Prepared by:



AES Consulting Engineers 5248 Olde Towne Road. Suite 1 Williamsburg, VA 23188 (757) 253-0040 Fax: (757) 220-8994



614 Moorefield Park Drive Richmond, VA 23236 (804) 330-8040 • Fax (804) 330-9840

December 23, 2003

Mr. Scott Thomas Environmental Division Director James City County P.O. Box 8784, Building E Williamsburg, Virginia 23187

RE: Windsormeade Marketplace AES Project No. 9069

Dear Mr. Thomas:

AES Consulting Engineers, on behalf of SLN Williamsburg, LLC, respectfully requests an exception from the Director of the Environmental Division for the James City County 10 point Environmental requirement. Included with this report is a James City County BMP worksheet indicating that we are able to obtain 9.75 points for the conditions of our site.

The 10 point extended wet pond (BMP #1) located behind the shopping center is designed to treat all of the impervious area that we are developing with these plans east of Windsormeade Way. The limits of the site extend to parcels between Windsormeade Way and News Road. Most of the drainage from these parcels is treated in BMP's submitted with Windsormeade Way plans.

We appreciate your help with this matter and hope you will not hesitate to call if you have any further questions.

Sincerely,

**AES Consulting Engineers** 

Bryan W. Stevenson NPC

Bryan W. Stevenson Project Engineer

NOT RECESSARY.

SITE 31.44AC

## Table 2

# Worksheet for BMP Point System

A. STRUCTURAL BMP POINT ALLOCATION

ВМР	BMP Points		Fraction of Site Served by BMP		Weighted BMP Points
#1-WETED		x	20.90/31.44	=	6.65
		X		=	
		X		=	
<del></del>		X		=	

TOTAL WEIGHTED STRUCTURAL BMP POINTS: 6.65

B. NATURAL OPEN SPACE CREDIT

	Fraction of Site	Natural  Open Space Credit	and a superproper	Points for Natural Open Space
	1.24/31.44 - 3942 x	• see on .	=	0.39
need nones	5.69/31.44 = 19.10 X	(0.1 per 1%) /5 (0.15 per 1%)		2.72

TOTAL NATURAL OPEN SPACE CREDIT: \_\_\_\_\_311

C. TOTAL WEIGHTED POINTS

$$\frac{6.65}{\text{Structural BMP Points}} + \frac{3.17}{\text{Natural Open Space Points}} = \frac{9.76}{\text{Total}}$$



## James City County, Virginia Environmental Division

# **Erosion and Sediment Control and Stormwater Management Design Plan Checklists**

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Project Lo Tax Map County P: County B Other info	arer: Arch Marston Email: amarston@aesva.com  ocation: Intersection of Monticello and Windsormeade Way Roads  / Parcel: lan No. (if known): MP Type: ( - )  ormation submitted in addition to this checklist (Check all that apply): Design or Construction Drawings (Plans, Profiles, Details, etc.).  Erosion & Sediment Control Plan (Plan, Details, etc.).	
	Erosion & Sediment Control Plan Design Report.  Stormwater Management Design Plan (Plans, Profiles, Details, etc.).  Stormwater Management Design Report.  Other, List:	

March 1, 2001

#### JAMES CITY COUNTY, VIRGINIA ENVIRONMENTAL DIVISION

## EROSION AND SEDIMENT CONTROL PLAN CHECKLIST

I.		<u>GENERAL</u>	<u>4</u> :
Yes ⊠	No	<b>N/A</b>	FAMILIARITY with current versions of Chapter 8, Erosion and Sedimentation Control and Chapter 23, Chesapeake Bay Preservation ordinances of the Code of James City County, Virginia and the Virginia Erosion and Sediment Control Handbook (VESCH).
			LAND DISTURBING PERMIT AND SILTATION AGREEMENT with surety are required for the project.
			VARIANCE if necessary, requested in writing, for the plan approving authority to waive or modify any of the minimum standards and specifications of the VESCH deemed inappropriate based on site conditions specific to this review case only. Variances which are approved shall be properly documented in the plan and become part of the approved erosion and sediment control plan for the site.
II.		SITE PLA	<u>N</u> :
Yes	No	N/A	VICINITY MAP locating the site in relation to the surrounding area. Include any major landmarks which might assist in physically locating the site.
$\boxtimes$			INDICATE NORTH direction in relation to the site.
$\boxtimes$			LIMITS OF CLEARING AND GRADING for the site including that required for implementation of erosion and sediment controls, stockpile areas and utilities.
$\boxtimes$			DISTURBED AREA ESTIMATES in acres or square feet for the project.
$\boxtimes$			EXISTING TOPOGRAPHY or contours for the site at no more than 5 foot contour interval.
			FINAL TOPOGRAPHY, contours or proposed site grading in accordance with the design plan which indicates changes to existing topography and drainage patterns at no more than 2 foot contour interval (or 1 foot contours where required).
			EXISTING AND PROPOSED SPOT ELEVATIONS to supplement existing and proposed contours, topography or site grading information. Spot elevations may replace final contours in some instances, especially if terrain is in a low lying area or relatively flat.
		$\boxtimes$	EXISTING VEGETATION including existing tree lines, grassed or unique vegetation areas

¥ es ⊠	No	N/A	EXISTING SITE FEATURES including roads, buildings, homes, utilities, streams, fences, structures and other important surface features of the site.
$\boxtimes$			SOILS MAP with soil symbols, boundaries and legend in accordance with the current Soil Survey of James City and York Counties and the City of Williamsburg, Virginia.
			ENVIRONMENTAL INVENTORY in accordance with Section 23-10(2) of the Chesapeake Bay Preservation Ordinance of James City County. Inventory generally includes: tidal shores and wetlands, non-tidal wetlands, resource protection area, hydric soils and slopes steeper than 25 percent. For wetlands, provide a copy of issued permits or satisfactory evidence that appropriate permits are being pursued for the entire project.
			100-YEAR FLOODPLAIN LIMITS or any special flood hazard areas or flood zones based on appropriate Federal Management Agency Flood Insurance Rate Maps (FIRMs) or Flood Hazard Boundary Maps (FHBMs) of James City County, Virginia.
$\boxtimes$			DRAINAGE AREAS for offsite and onsite areas, existing or proposed as applicable. Include drainage divides and directional labels for all subareas at points of interest and size (in acres), weighted runoff coefficient or curve number and times of concentration for each subarea.
			CRITICAL EROSION AREAS which require special consideration or unique erosion and sediment control measures. Refer to the VESCH, Chapter 6 for criteria.
			DEVELOPMENT PLAN for the site showing all improvements such as buildings, structures, parking areas, access roadways, above and below ground utilities, stormwater management and drainage facilities, trails or sidewalks, proposed vegetation and landscaping, amenities, etc.
$\boxtimes$			LOCATION OF PRACTICES proposed for erosion and sediment control, tree protection and temporary stormwater management due to land disturbance activities at the site. Use standard abbreviations, labels and symbols consistent for plan views based on minimum standards and specifications in Chapter 3 of the VESCH.
$\boxtimes$			TEMPORARY STOCKPILE AREAS or staging and equipment storage areas as required for onsite or offsite construction activities or indicate that none are anticipated for this project.
			OFFSITE LAND DISTURBING AREAS including borrow sites, waste areas, utility extensions, etc. and required erosion and sediment controls. If none are anticipated for the project, then indicate on the plans by general or erosion and sediment control notes.
			DETAILS or alternately, appropriate reference to current minimum standards and specifications of the VESCH for each measure proposed for the project. Non-modified, standard duplicated details (silt fence, diversion dikes, etc.) may be referenced to the current version of the VESCH. Specific dimensional or modified standards (basins, traps, outlet protections, check dams, etc.) require presentation on detail sheets. Schedules or tables may be used for multiple site measures such as sediment traps, basins, channels, slope drains, etc. Any modification to standard details should be clearly defined, explained and illustrated.

$\boxtimes$			MAINTENANCE PLAN or alternately, appropriate reference to current minimum standards and specifications of the VESCH, outlining the inspection frequency and maintenance requirements for all erosion and sediment control measures proposed for the project.
		$\boxtimes$	TRENCH DEWATERING methods and erosion and sediment controls, if anticipated for the project.
$\boxtimes$			CONSTRUCTION SEQUENCE outlining the anticipated sequence for installation of erosion and sediment controls and site, grading and utility work to be performed for the project by the site contractor.
$\boxtimes$			PHASING PLAN if required for larger project sites that are to be developed in stages or phases.
$\boxtimes$			STANDARD COUNTY NOTES are required to be placed on the erosion and sediment control plan. Refer to the standard James City County Erosion and Sediment Control Notes dated May 5, 1999.
$\boxtimes$			PROFESSIONAL SEAL AND SIGNATURE required on final and complete approved plans, drawings, technical reports and specifications.
III.		<u>NARRATI</u>	<u>ve</u> :
Yes ⊠	No	N/A	PROJECT DESCRIPTION briefly describing the nature and purpose of the land disturbing activity and the acreage to be disturbed.
	No	N/A	•
	No	N/A	activity and the acreage to be disturbed.  EXISTING SITE CONDITIONS description of existing topography, land use, cover and
	No	N/A	activity and the acreage to be disturbed.  EXISTING SITE CONDITIONS description of existing topography, land use, cover and drainage patterns at the site.  ADJACENT AREA descriptions of neighboring onsite or offsite areas such as streams, lakes, property, roads, etc. and potential impacts due to concentrated flow or runoff from
	No		activity and the acreage to be disturbed.  EXISTING SITE CONDITIONS description of existing topography, land use, cover and drainage patterns at the site.  ADJACENT AREA descriptions of neighboring onsite or offsite areas such as streams, lakes, property, roads, etc. and potential impacts due to concentrated flow or runoff from the land disturbing activity.  OFFSITE DISTURBED AREA descriptions of proposed borrow sites, water or surplus

Yes		N/A	PROPOSED EROSION & SEDIMENT CONTROL MEASURES inclusive to the specific erosion and sediment control plan as proposed for the land disturbing activity. Measures should be consistent with those proposed on the site drawings. Address general use, installation, limitations, sequencing and maintenance requirements for each control measure.
$\boxtimes$			STABILIZATION MEASURES required for the site, either temporary or permanent, and during and following construction including temporary and permanent seeding and mulching, paving, stone, soil stabilization blankets and matting, sodding, landscaping or special stabilization techniques to be utilized at the site.
$\boxtimes$			STORMWATER MANAGEMENT CONSIDERATIONS for the site, either of temporary or permanent nature, and strategies, sequences and measures required for control. May reference the stormwater management plan for the site, if prepared, for permanent stormwater management facilities and control of drainage once the site is stabilized.
IV.		CALCULA	<u>ITIONS</u> :
Yes ⊠	No	N/A	CALCULATIONS AND COMPUTATIONS associated with hydrology, hydraulics and design of proposed temporary and permanent erosion and sediment control measures
			including: sediment traps and basins, diversions, stormwater conveyance channels, culverts, slope drains, outlet protections, etc. Computations are not required on the construction plan and may be attached in a supplemental erosion and sediment control plan design report, if presented in a clear and organized format.

#### JAMES CITY COUNTY, VIRGINIA ENVIRONMENTAL DIVISION

## STORMWATER MANAGEMENT DESIGN PLAN CHECKLIST

I.		<u>GENERAL</u>	<u>L</u> :
Yes	No	N/A	FAMILIARITY with current versions of the James City County Guidelines for Design and Construction of Stormwater Management BMPs manual; Chapter 8, Erosion and Sediment Control and Chapter 23, Chesapeake Bay Preservation ordinances of the Code of James City County, Virginia; the Virginia Erosion and Sediment Control Handbook (VESCH); and the Virginia Stormwater Management Handbook (VSMH).
			WAIVER OR EXCEPTION if necessary, requested in writing, for the plan approving authority to waive or except the requirements of Chapter 23, Chesapeake Bay Preservation ordinance in accordance with procedure established in Sections 23-14 through 23-17 of the ordinance. Applies to the review case only.
			VARIANCE REQUEST if necessary, requested in writing for the plan approving authority to waive or modify any of the minimum standards and specifications of the VESCH deemed inappropriate based on site conditions specific to this review case only. Variances which are approved shall be properly documented in the plan and become part of the approved erosion and sediment control plan for the site.
$\boxtimes$			PROFESSIONAL SEAL AND SIGNATURE required on final and complete approved stormwater management plans, drawings, technical reports and specifications.
			WORKSHEET FOR BMP POINT SYSTEM to ensure the stormwater management plan for the project attains at least 10 BMP points (New Development) or traditional pollutant load reduction computations per the Chesapeake Bay Local Assistance Manual (Redevelopment Only)
		$\boxtimes$	PROPOSED CONSERVATION EASEMENT AREAS for any natural open space points claimed in the BMP worksheet.
	$\boxtimes$		INSPECTION/MAINTENANCE AGREEMENT is required to be prepared and executed with the County for the project.
			FEMA FIRM PANEL reference with designated special flood hazard areas or zone designations associated with the site, as applicable.
			DRAINAGE AREA MAP at a maximum scale of 1"=200' scale showing drainage area boundaries for pre- and postdevelopment conditions and associated time of concentration flow paths. Labels to include drainage area size, runoff coefficient or curve number and time of concentration for each subarea shown on the map.

Xes No N/A	SOILS MAP with soil symbols, boundaries and legend in accordance with the current Soil Survey of James City and York Counties and the City of Williamsburg, Virginia with approximate locations of the project site, BMPs and applicable drainage basins.
	STORMWATER MANAGEMENT NARRATIVE in a brief and simple format which describes the project; location; site and drainage basin soil characteristics; receiving water or drainage facility; existing site and drainage basin conditions (topography, land use, cover, slopes, etc.); proposed site development; proposed stormwater management and drainage plan including County BMP type selected; summary of hydrology and hydraulics; maintenance program; and any special assumptions utilized for development of the stormwater management and drainage design plan or computations.
	TEMPORARY STORMWATER MANAGEMENT (if applicable) for control of stormwater runoff encountered during construction activities in addition to measures provided in the erosion and sediment control plan or stormwater management/drainage plan for the site. Adequate protection measures or sequencing provided.
	MODIFICATION PLAN clearly defined for temporary sediment control structures which will be converted to permanent SWM/BMP structures. Includes appropriate hydrologic and hydraulic computations, conversions, sequencing and cleanout information or details. Normally related to primary control structures associated with dry detention or wet retention ponds. Normally not permitted for Group C or D categories such as bioretention, infiltration and filtering system facilities.
	STORMWATER MANAGEMENT and DRAINAGE DESIGN REPORT in a bound 8-1/2 x 11 inch size format. Report shall generally include a title sheet, date, project identification, owner and preparer information, table of contents, narrative, summaries and computations as required. Computations may include: backwater, closed conduit, headwater, hydraulic, hydraulic grade line, hydrology, inlet, open channel, storm sewer, water quality, extended detention or stream channel protection and multi-stage storm routing calculations, as applicable, for the project. Computation data may include hand or computer generated computations, maps or schematics. All information should be presented in a clear, easy to follow format and should closely match construction plan information.
	PLAN VIEW at 1 inch = 50 ft. scale or less (1" = 40', 1" = 30', etc.)  North arrow and plan legend.  Property lines.  Adjacent property information.  Existing site features and existing impervious cover areas.  Impervious cover tabulations.  Existing drainage facilities (natural or manmade)  Existing environmentally sensitive areas (RPA, wetlands, floodplain, steep slopes, critical soils, buffers, etc.)  Existing and proposed contours (1' or 2' contour interval) and spot elevations as necessary to define high and low topography.  Existing and proposed easement locations.

	Yes No N/A	Proposed site improvements and proposed impervious cover areas. Proposed stormwater conveyance, drainage and management facilities with appropriate labeled construction data and information. Proposed landscaping and seeding plans (disturbed areas, pond interior, etc.)  Proposed slope stabilization areas (riprap, blankets, mattings, walls, etc.)  Delineation of permanent pools and the 1-, 2-, 10- and 100-year Design Water Surface Elevations.  Delineation of ponding, headwater, surcharge or backwater areas which may affect adjacent existing or proposed buildings, structures or upstream adjacent properties.  Test boring locations with reference surface elevations (if known). Risers, barrels, underdrains, overflows and outlet protections.  Emergency spillway level section and outlet channel.  Existing and proposed site utilities and protection measures.  Erosion and sediment control measures (for site or BMP).  Maintenance or access corridors to permanent stormwater management, BMP or drainage facilities.
II. <u>STORMW</u>	ATER CONVEYAL	NCE SYSTEMS:
Yes No N/A  □ □	PLAN VIEWS  □ □  □  □ □  □	Storm drain lengths, sizes, types, classes and slopes for all segments. Label directly on plan or use structure/pipe schedule.  Access structure (inlets, manholes, junctions, etc.) rim elevations, inverts, type and required grate or top unit and lengths labeled.  All structure numbers labeled.  Adequate horizontal clearance from other site utilities or structures.
	provided, ensure a	ally are not required but are encouraged to expedite review. If not all pipe segments have adequate minimum cover, do not exceed of cover for the type/class of pipe specified and do not conflict with other eavation areas.
	DETAILS  DET	Typical storm drain bedding details or reference note.  Standard details or reference note for all proposed access structure types (inlets, manholes, junctions, etc.).  Inlet shaping detail or applicable reference note.  Step detail or applicable reference note (if depth 4 ft. or more).  Typical open channel details with designation, location, shape, type, bottom width, top width, lining, slope, length, side slope, and installation depth required for construction. Channel design data as necessary may also be included.  Outlet protections at all pipe outfalls.

Tes No IN/A		Storm Sewer Design computations based on 10-year design event. Hydraulic Grade Line computations based on 10-year design event. Inlet computations based on current VDOT procedure for spread, ponding depth and grate size required.  Culvert Headwater computations. Design based on 10-year design storm event and check only for 100-year storm event.  Open Channel computations based on 2-year design event for velocity and 10-year design event for capacity.  Standard outlet protection or special energy dissipators.  Pipe thickness design computations, as required, for selected pipe type (live load, minimum cover, maximum height of cover, etc.).  Adequate channel computations for receiving channels (based on field measured channel section data).
III. <u>ST</u>	<u>ORMWATER MANAGEI</u>	MENT/BMP FACILITIES:
Yes No N/A ⊠ □ □	HYDROLOGY – management/BM Under 20 acres, o	An SCS based methodology is required for the design of stormwater P facilities with watersheds exceeding 20 acres. ther generally accepted methodologies such as the modified rational, allowable. Refer to Chapter 5 of the VESCH or Chapter 5 of the VSMH.
		Runoff Curve Number or Coefficient determinations: predeveloped and ultimate development land use scenarios.  Time of concentration: predeveloped and ultimate development indicating overland, shallow concentrated, and channel flow components (200 ft. maximum length for overland flow).  Hydrograph generation (tabular or graphical): pre- and postdevelopment conditions for the 1-, 2-, 10- and 100-year design storm events.
	FACILITY CONF	Screening and layout consistent with Section 24-98(d) of the Chapter 24 Zoning ordinance (landscaping, screening, visibility, etc.).  Basic considerations for safety and unauthorized entry.  Proper length to width ratio (Typically 2H:1V).  Facilities with deep pools (4 feet or more in depth) provided with two benches. Fifteen (15) ft. safety bench outward from normal pool at maximum 6 percent slope and aquatic bench inward from normal
		shoreline below normal pool. Narrower widths may be considered on a case-by-case basis.  Pond buffer minimum 25 feet outward from maximum design WSEL. Additional setbacks may be required to permanent structures.  No trees, shrubs or woody plants within 15 feet of embankment toe or 25 feet from principal spillway structure.  Infiltration and filtering system facilities generally located at least 100 feet horizontally from any water supply well; 100 feet from any downslope building; and 25 feet from any upslope buildings, unless site specific investigation allows for reduced separation.

Yes No N/A		
	HYDRAULIC CO.	Elevation- or Stage-Storage curve and/or tabular data.  Weir / Orifice Control – Extended Detention.  Weir / Orifice Control – riser 1-year control for channel protection.  Weir / Orifice Control – riser 2-year control for quantity (if required).  Weir / Orifice Control – riser 10-year control for quantity (if required).  Inlet / Outlet (barrel) control – (All Storms).  Check for barrel control prior to riser orifice flow to prevent slug flowwater hammer conditions.  Emergency spillway capacity and depth of flow.  Elevation – Discharge (Outlet Rating) curve and/or table. Provide all supporting calculations and/or design assumptions.  Adequate channel computations for receiving channel. May be waived if facility is designed based on current Stream Channel Protection criteria.
	POND or RESERI	Storage-Indication Routing of postdeveloped inflow hydrographs for the 1-, 2-, 10-, and 100-year design storms. Preference is for structure to discharge up to the 10-year storm through the principal spillway and pass the 100-year storm with a minimum 1 foot of freeboard through a combination principal and emergency spillways. If no emergency spillway is provided, riser must be large enough to pass the design high water flow and trash without overtopping the facility, have 3 square fee or more of cross-sectional area, contain a hood type inlet and have a minimum freeboard of 2 feet. Token spillways with minimum 8 ft. width are also recommended at or above the design 100-year storm elevation.  Downstream hydrographs at established study points, if conditions warrant (i.e. facility discharge combined with uncontrolled bypass).
	MISCELLANEOU  MI	Water quality volume for permanent pool based on selected BMP treatment volume (WQv).  Water quality volume for extended detention base on selected BMP treatment volume (WQv) with drawdown computations.  Drawdown computations for the 1-year, 24 hour detention for stream channel protection criteria.  Pond drain computations (within 24 hours).  Anti-seep collar design (concrete preferred) or match material type.  Filter diaphragm design (or alternative method of controlling seepage).  Riser / base structure flotation analyses. FS = 1.25 minimum.  Downstream danger reach study and/or emergency action plan (if conditions warrant).  Upstream backwater analyses onto offsite adjacent property (if conditions warrant).

Yes No N/A	*	
lacktriangled		REQUIREMENTS
		Geotechnical Report with recommendations specific to BMP facility
		type selected. Report prepared by a registered professional engineer.
		Requires submission, review and approval prior to issuance of Land
		Disturbance Permit.
		Initial Feasibility Testing requirements satisfied as per Appendix E of
		the James City County Guidelines fro Design and Construction of Stormwater Management BMPs manual. (Infiltration, Bioretention and
		Filtering System BMP types only).
	$\sqcap$ $\square$	Concept Design Testing requirements satisfied as per Appendix E of
		the James City County Guidelines for Design and Construction of
		Stormwater Management BMPs manual (Infiltration, Bioretention
		and Filtering System BMP types only).
		Minimum Boring locations: borrow area, pool area, principal control
		structure, top of facility near one abutment and emergency spillway if
	- <b>-</b> -	provided.
		Boring logs with Unified Soil Classification (ASTM D2487), soils
		descriptions and depths to bedrock and the seasonal water table
		indicated. Standard County Record Drawing/Construction Certification note
		provided on plan. Note: It is understood that preparation of record
		drawings and construction certifications as required for project
		facilities may not necessarily be performed by the plan preparer. These
		components may be performed by others.
$A \square \square$	PRINCIPAL SPIL	LWAY PROFILE AND ASSOCIATED DETAILS
	$\bowtie \sqcap \sqcap$	EXISTING GROUND AND PROPOSED GRADE
		Embankment or excavation side slopes labeled
		(3H:1V maximum).
		Minimum top width labeled (per VESCH or VSMH
		requirements).
		Removal of unsuitable material under proposed
		facility (per Geotechnical Report requirements).

Yes No N/A	CORE TRENCH	Bottom width (4' n recommendations). Side slopes (1:1 ma	
	PRINCIPAL CON REQUIRED FOR  CONTROL CO	ALL ITEMS) Durable, watertigh Riser diameter is a All pertinent dimer Control orifice or v Trash rack – remov Anti-vortex device Riser base structure	e with dimensions and embedment specifications
		4 feet in height. Exerterior access on	ps, ladders, etc.) for maintenance for structures over accessively high risers may need some form of
	PRINCIPAL CON	Material (ASTM C Prior approval requ CMP, CPP, PVC, o	
		as recommended b Pipe inverts, length	ng requirements for barrel – concrete cradles, etc. or y the Geotechnical Report.  n, size, class and slope shown.  or endwall provided on barrel outlet.
	SEEPAGE CONTI	Phreatic line show	n (4:1 slope measured from the intersection of the he principal spillway design high water).
		ANTI-SEEP COLL  Co	ARS Anti-seep collar, concrete preferred. Size – 15 percent increase in length of saturation using outside pipe diameter. Spacing and location on barrel (located at least 2 feet from a pipe joint).
		FILTER DIAPHRA	AGMS  Design based on latest NRCS design methods and certified by a professional engineer.

Yes No N/A		
	ELEVATION AND	D DIMENSIONAL DESIGN DATA  Top of facility – construction height and settled height (10 percent
		settlement).  Crest of principal control structure spillway at least one (1) foot below crest of emergency spillway, if provided.
		Minimum freeboard of one (1) foot above the 100-year design high
		water elevation for facilities <u>with</u> an emergency spillway.  Minimum freeboard of two (2) feet above the 100-year design high water elevation for facilities <u>without</u> an emergency spillway or in accordance with the SCS National Engineering Handbook (prior
		approval required). Basin Sediment Clean-Out elevation (permanent mode). Typically 10 to 25 percent of water quality volume.
	CROSS SECTION  CROSS SECTION  CROSS SECTION  CROSS SECTION	THROUGH FACILITY Existing Ground. Proposed grade. Top of facility – constructed and settled. Location of emergency spillway with side slopes labeled (emergency
		spillway in cut).  Bottom of core trench (4' minimum).  Location of each soil boring.  Barrel location.  Existing and proposed utility location/protection.
	EMERGENCY SP	Existing ground. Inlet, level (control) and outlet sections per SCS. Spillway and crest elevations.
	pretreatment volume to: sediment foreb	TDEVICES of adequate depth and properly designed using required mes for the selected County BMP facility type. Including, but not limited ays, sediment basins, sumps, grass channels, gravel diaphragms, plunge parators, manufactured systems or other acceptable methods.

ies no n/A	001/0mp1/0m	I ODDOUGLO ATTOMO
		SPECIFICATIONS and NOTES
		Anticipated sequence of construction for BMP (consistent with erosion
		and sediment control plan).
		Provisions to control base stream or storm flow conditions encountered during construction.
	$\boxtimes \sqcap \sqcap$	Site and subgrade preparation requirements.
		Embankment, fill and backfill material soil and placement (lift) thickness requirements.
	$\square$ $\square$ $\square$	Compaction and soil moisture content requirements.
	HHH	Geosynthetics for drainage, filtration, moisture barrier, separation, and
		reinforcement purposes.
		Clay or synthetic (PVC or HDPE) pond liners.
	MHH	Storm drain, underdrain and pipe conduit requirements.
		Minimum depth of pipe cover for temporary (construction) and final
		cover conditions.
	$\boxtimes$ $\Box$ $\Box$	Permanent shutoff valve and pond drain.
	M H H	Concrete requirements for structural components.
		Riprap and slope protection.
		Access or maintenance road surface, base, subbase.
		Temporary and permanent stabilization measures.
	HHH	Temporary or permanent safety fencing.
	HHH	
		BMP Landscaping (deep, shallow, fringe, perimeter, etc.)
	HHH	Dust and traffic control (if warranted).
	님 님	Construction monitoring and certification by professional.
		Other:
		Other:
	1.4.43200031432000	DD OWG ONG
	MAINTENANCE I	
		Entity responsible for maintenance identified.
	$\bowtie$ $\sqcup$ $\sqcup$	Maintenance Plan which outlines the long-term schedule for
		inspection/maintenance of the facility and forebays.
		Maintenance access from public right-of-way or publicly traveled road.
		Maintenance easement provided encompassing high water pool and
		buffer, principal and emergency spillways, outlet structures, forebays,
		embankment area and possible sediment-removal stockpile areas.
		Minimum 6 foot wide public safety shelf (landing) or alternative
		fencing.

#### IV. <u>OUTLET PROTECTIONS</u>:

Yes No N/A	
	Sized for maximum design release (generally 10-year storm).
	Flared end section or endwall.
	Dimensions.
	Rock or riprap size, quantity and placement thickness.
	Slope at 0 percent (Level Grade).
	Geotextiles (nonwoven).
	Special energy dissipators are required for design discharge velocities that
	exceed eighteen (18) feet per second; or if use of standard outlet protection
	would result in velocities exceeding permissible channel velocities; or if
	space restricts or limits their use.

#### IV. ADDITIONAL COMMENTS OR INFORMATION SPECIFIC TO THE PLAN:

Plan I	Preparer:	
Date:		

Copy of JCC: SWMProg/BMP/Checklist/ChkList

#### **AES CONSULTING ENGINEERS**

Engineering, Surveying, and Planning 5248 Olde Towne Road, Suite 1 WILLIAMSBURG, VIRGINIA 23188

LETTER OF TRANSMITTAL

Phone: (757) 253-0040 Fax: (757) 220-8994

ATTN:	Jason Beck			DATE	JOB NO.	
	Environmental Inspector			11/06/2007 9069-02 FROM:		
CO.:	JCC			Matt Good		
00	P.O. Box	8784		RE		
	101-E Mounts Bay Road				RAWINGS (MYLAR	
Address:	Williamsburg, Virginia 23187-			COPY)	`	
	8784			ſ	DECENTED !	
	Mail for s	signatures			RECEIVED	
cc:						
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WE ARE	SENDING 1	TOU THE FOL	LOWING HEMS:	☐ Attached☐ Under separate co	DIVISION ver via	
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L	Original(s)	) 🛛 Print(s)	☐ Plan(s)	☐ Specification(s)	Change Order	
	☐ Copy of le	tter(s)	Other:			
COPIES	DATE	No. of Pages		DESCRIPTION		
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THESE A	RE TRANSI	MITTED as ch	ecked below:			
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☐ For your approvar ☐ For your signature ☐ For review and confinent			and comment			
☐ For your use ☐ As you requeste			As you requested	☐ As request	ed by:	
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#### CALCULATION FOR SCS HYDROGRAPH GENERATION AND CHANNEL PROTECTION FOR SWMP POND #1

#### WINDSORMEADE MARKETPLACE

AES Project No.:9069-02 December 20, 2003

PRE-DEVELOPMENT CONDITIONS TO POINT OF CONCERN Pre-Development Drainage Area to Point of Concern = Pre-development Land Use, Soil Classification and Calculation of Composite Curve Number B.

1)

3)

13.90 Acres

60

Wooded, B and C soils Pre-Development Time of Concentration Calculations C.

Overland Flow (maximum 300 feet) Surface description (table 5-7) Manning's roughness coefficient., n (table 5-7) Length of overland flow, L 2-year 24-hour rainfall, P2 Average slope of overland flow , s Travel time,  $Tt = (0.007*(n*L)^0.8)/(P2^0.5*s^0.4)$ 

Woods, Good Cond. 0.4 250 Feet 3.5 inches 0.04 feet per foot 0.54 hours

Shallow concentrated flow (maximum 300 feet) 2) Surface description, paved or unpaved Length of shallow concentrated flow, L Average slope of shallow concentrated flow, s

Average velocity, v
Travel time, Tt = L/(3600\*v)

Wooded, Good Cond. 300 Feet 0.03 feet per foot 2.8 feet per second 0.03 hours

Channel or Pipe Flow Length of channel flow, L Average velocity of channel flow, v Travel time, Tt = L/(3600\*v)

0 Feet 2.5 feet per second 0.00 hours

NECO

Total Time of Concentration =

POST-DEVELOPMENT CONDITIONS TO POINT OF CONCERN (for total site and

Post-Development Drainage Area to Point of Concern =
Post-development Land Use, Soil Classification and Calculation of Composite Curve Number B.

C. Post-Development Time of Concentration Calculations

Overland Flow (maximum 300 feet) Surface description (table 5-7) Manning's roughness coefficient., n (table 5-7) Length of overland flow, L 2-year 24-hour rainfall, P2 Average slope of overland flow , s

Travel time, Tt = (0.007\*(n\*L)^0.8)/(P2^0.5\*s^0.4)

2) Shallow concentrated flow (maximum 300 feet) Surface description, payed or unpayed Length of shallow concentrated flow, L Average slope of shallow concentrated flow, s Average velocity, v Travel time, Tt =  $L/(3600^*v)$ 

3) Channel or Pipe Flow Length of channel flow, L Average velocity of channel flow, v Travel time, Tt = L/(3600\*v) 0.57 hours 34 minutes

Woods, good condition

0.4 100 Feet 3.5 inches

0.03 feet per foot 0.29 hours

paved

comps seems Low for A 89.600 Imperv 115 Feet 0.01 feet per foot 2.00 feet per second 0.02 hours

812 Feet 5.6 feet per second 0.04 hours

Total Time of Concentration =

or

or

20.90 Acres 20.970 mperv. 89-670 imperv.

#### III. PROPOSED ESTIMATED POND(S) VOLUME

				Inc. Volume	Sum	Sum
		Area	Incremental Volume	(cu. yd.)	Volume	Volume
Elevation	<u>Depth</u>	<u>(sq. ft.)</u>	(cu. ft.)		(cu. ft.)	(cu. yd.)
<u>73</u>	$_{\underline{o}}$	<u>6701</u>	<u>0</u>	0	0	0
74	1	12,612	9,657	358	9,657	358
75	1	13,689	13,151	487	22,807	845
76	1	14,799	14,244	528	37,051	1,372
77	. 1	15,942	15,371	569	52,422	1,942
78	1	22,057	19,000	704	71,421	2,645
79	1	28,821	25,439	942	96,860	3,587
80	1	30,977	29,899	1,107	126,759	4,695
81	1	33,191	32,084	1,188	158,843	5,883
82	1 /	35,463	34,327	1,271	193,170	7,154
.83	1 /	37,794	36,629	1,357	229,799	8,511
84	1 3	40,219	39,007	1,445	268,805	9,956

 $\frac{77}{787} = \frac{52422}{71421}$   $\frac{77}{7877} = \frac{4-52422}{718-77}$   $\frac{71421-52421}{78-77} = \frac{4-52422}{18999}$ 

#### **DETERMINING REQUIRED WATER QUALITY VOLUME**

Due to preliminary considerations, it is desired to provide this site extended detention wet pond to achieve a 10 point BMP rating for the facility. Under the James City County guide lines for storm water management BMPs, the extended detention wet pond may have one half of the water quality volume stored in the permanent pool and one half of the water quality volume released in a 24-hour period.

0.7 x=65721

Percent Impervious of the BMP Watershed, Post-Development

Drainage Area of the BMP Watershed

Impervious Acres of BMP Watershed

Calculation for Water Quality Volume, WQ

WQ<sub>v</sub> = (2.0 inches per impervious acre) \*( impervious acres of BMP watershed)

WQv = (2.0 inches)\*(1 ft / 12 inches) \* (43560 sq. Ft per acre) \* (impervious acres of BMP watershed)

A-3 ox

 $WQ_v = (2.0 \text{ inches})^*(1 \text{ ft} / 12 \text{ inches})^* (43560 \text{ sq. Ft per acre})^*$ 

WQ.. =

Elevation of total WQv =

WQ., (provided)=

Elevation of release inlet for 1/2 water quality volume =

Average head, in feet, on release inlet =

Average release rate calculation

18.10

65703 cu. Ft ✓ 65703 cu. Ft

65718 cu. Ft 67137 cu. Ft

132855

131406 cu. Ft

Required Volume for Permanent Pool Design Volume for Dry Storage (1" per Impervious Acre)

Water Quality Volume Provided for Wet pool 7 7, 7, 9/L Water Quality Volume Provided for Dry pool Total Water quality volume

80.2

1.2

6104/ cust

Calculation of size of release inlet for 1/2 Water Quality Volume

Diameter of Release Inlet = 2 \* ( Q / ((64.32 \* (h / 2)) ^ (1/2) \* 0.6 \* 3.14))) ^ (1/2)

where, Q equals Average Release Rate, in cfs h equals Average Head, in feet

Diameter of Release Inlet =

Note: A design with an orifice size of 3" will

0.50

67,137.0 cubic feet

feet, or

be used for channel protection requirements

(24 hours x 60 minutes/hour x 60 seconds/ minute)

0.8 cfs 0.77

0.77 CFS 0.6 V by.4 (1.2) 0.146 5F

 $\int_{CJ}^{2} d^{2} = 0.14b$   $\int_{CJ}^{2} d^{2} = 0.1859$ 

Page 2

AES Projet No.:

9069

Project Title:

BMP No. 1



#### **Channel Protection**

#### **Channel Protection Volume**

#### **Post Development Watershed Data**

Area = 20.90 Acres

0.0327sq.mi.

Runoff Curve No.(= 70 Time of Concentration = 0.260 hr.

Return Period = 1 Yr.

Runoff Depth =

2.8 in.

#### **Initial Abstraction (From TR55 Equation 2-2)**

Ia = (200/CN)-2

Ia = 0.857

#### Unit Peak Discharge (From TR55 Equation for Exhibit 4)

 $log(Qu) = C0+C1 log(Tc)+C2(log(Tc))^2$ Qu = 719.46 csm/in

### Ratio of Peak Outflow Discharge to Peak Inflow Discarge

(From Maryland Stormwater Design Manual Figure D.11.2)

Qo/Qi = 0.024

### Ratio of Volume of Storage to Volume of Runoff (From TR55 Figure 6.1)

 $Vs/Vr = C0+C1(Qo/Qi)+C2(Qo/Qi)^2+C3(Qo/Qi)^3$ 

Vs/Vr = 0.648

Vs = 0.684 Ac-Ft

Vs = 29792 cu.ft.

Table F-2				
Coefficients for the equations used to generate figure 6-1				
Rainfall Dist.	C0	C1	C2	C3
I, IA	0.66	-1.76	1.96	-0.73
II, III	0.682	-1.43	1.64	-0.804

#### **Average Release Rate**

Qi = 14.24 cfs

 $Q_0/Q_i = 0.02$ 

 $Q_0 = 0.35 \text{ cfs}$ 

AES Project No. 9069 Job Title BMP No. 1

Area=	20.90 Acres	0.0327sq.mi.
CN=	70	
Tc=	0.260 hr.	
P=	2.8 in.	Rainfall depth for 1yr return period
la=	0.857	Initial abstraction is all losses before runoff begins. le surface depressions, water intercepted by vegitation, evaporatation(SeeTR55 Chapter 2, Equation 2-1)
Qu=	719.46 csm/in	Unit Peak Discharge - Peak discharge per square mile per inch of runoff (Units are "cubic square miles per ing
Direct Runoff=	0.6 in.	Runoff in inches (See TR55 Chapter 2, Equation 2-1)
Qi=	14.24 cfs	Peak Inflow Discharge
Qo/Qi=	0.024	Ratio of Peak Inflow Discharge to Peak Outflow Discharge (See TR55 Chapter 6)
Qo=	0.35 cfs	Peak Outflow Discharge (See TR55 Chapter 6) Taken from Maryland Dept. of Stormwater Management Appendix D.11, figured.11.2. The curve for 24hr detention used in Chart 1 was scaled and a curve was fit to the data points. The resulting equation, which appears on the chart yeilds a very good fit.
	0.648 0.684 Ac-Ft 29,792 cu.ft.	Ratio of Volume Stored to Volume Realeased (See TR55 Chapter 6). Value Computed using equation for Figure 6-1 as shown in Appendix F. Required Storage Volume

Average Flow Rate (Qo) 0.35 cfs Average head= 1.25 ft.

Area of orifice= 0.06 sq.ft.

Orifice diameter = 0.29 ft.
Orifice diameter = 3.4 in.

This offers a place to start. After routing the 1yr storm through the oriface check the out put to make sure that the Required Storage Volume is actually detaind for 24 hours. If not adjust the orifice size and recompute.

# Hydrograph Return Period Recap

lyd.	Hydrograph	Inflow				Hydrograph					
o.	type (origin)	Hyd(s)	1-Yr	2-Yr	3-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr	description
	SCS Runoff		1.35	3.92			18.17	22.72		35.81	PRE-DEVELOPMENt
	SCS Runoff		11.28	20.72			58.48	69.46		99.85	9069POST-DEVELOPMENT
	Reservoir	2	0.27	0.35			25.80	38.22		43.82	wet pond
											*
						·					
											• *
			1								
1											
			-								
		*									
				<u> </u>			1				te: 12-22-2003

Hydraflow Hydrographs by Intelisolve

#### Reservoir No. 2 - WET POND

#### **Pond Data**

Pond storage is based on known contour areas. Average end area method used.

Stage	/ Storage	Table
-------	-----------	-------

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)	
0.00	73.00	6,701	0	0	
1.00	74.00	12,612	9,657	9,657	
2.00	75.00	13.689	13,151	22,807	100
3.00	76.00	14,799	14,244	37,051	11 6 11
4.00	77.00	15,942	15,371	52,422	36
5.00	78.00	22,057	19,000	71,421	7 ()
6.00	79.00	28,821	25,439	96,860	
7.00	80.00	30,977	29,899	126,759	
8.00	81.00	33,191	32,084	158,843	
9.00	82.00	35,463	34,327	193,170	
10.00	83.00	37.794	36,629	229,799	
11.00	84.00	40,219	39,007	268,805	

Culvert / Or	ifice Structui	es			Weir Struct	ures			
	[A]	[B]	[C]	[D]		[A]	[B]	[C]	[D]
Rise in	= 24.0 🗸	3.0	0.0	0.0	Crest Len ft	= 18.00	0.00	0.00	0.00
Span in	= 24.0 🗸	3.0	0.0	0.0	Crest El. ft	= 80.19	0.00	0.00	0.00
No. Barrels	= 1 /	1 /	0	0	Weir Coeff.	= 3.33	3.33	0.00	0.00
Invert El. ft	= 72.72 V	77.70	0.00	0.00	Weir Type	= Riser			
Length ft	= 61.0	0.0	0.0	0.0	Multi-Stage	= Yes	No	No	No
Slope %	= 1.18	0.00	0.00	0.00					
N-Value	= .013	.013	.000	.000					

 Orif. Coeff.
 = 0.60
 0.60
 0.00
 0.00

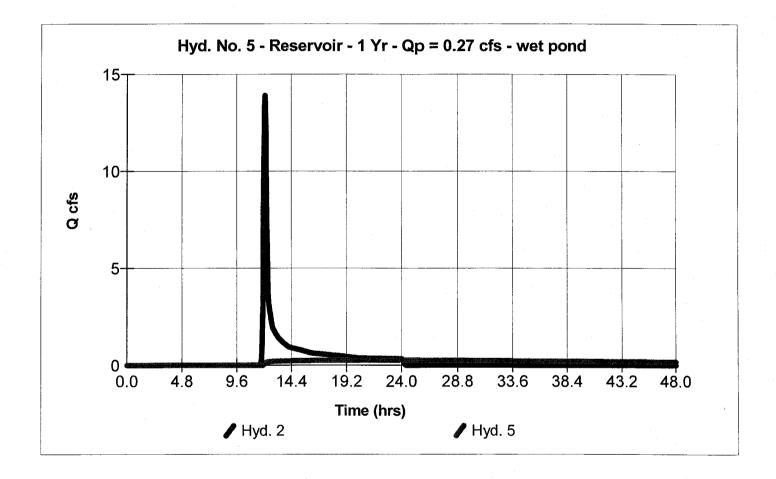
 Multi-Stage
 = n/a
 No
 No
 No
 Exfiltration Rate
 = 0.00 in/hr/sqft
 Tailwater Elev.
 © 0.00 ft

Note: All outflows have been analyzed under inlet and outlet control.

Stage /	Storage /	Discharge	Table									
Stage ft	Storage cuft	Elevation ft	Clv A cfs	CIv B cfs	Clv C cfs	Clv D cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Total cfs
0.00	, 0	73.00	0.00	0.00			0.00					0.00
1.00	9.657	74.00	0.51	0.00			0.00					0.00
2.00	22,807	75.00	0.51	0.00			0.00					0.00
3.00	37,051	76.00	0.51	0.00			0.00					0.00
4.00	52,422	77.00	0.51	0.00			0.00					0.00
5.00	71,421	78.00	0.51	0.10			0.00					0.10
6.00	96,860	79.00	0.51	0.26			0.00					0.26
7.00	126,759	80.00	0.51	0.35			0.00	-				0.35
8.00	158.843	81.00	39.38	0.42			39.38					39.80
9.00	193,170	82.00	43.38	0.48			43.36					43.84
10.00	229.799	83.00	46.03	0.54			46.01					46.55
11.00	268,805	84.00	48.48	0.59			48.39					48.98

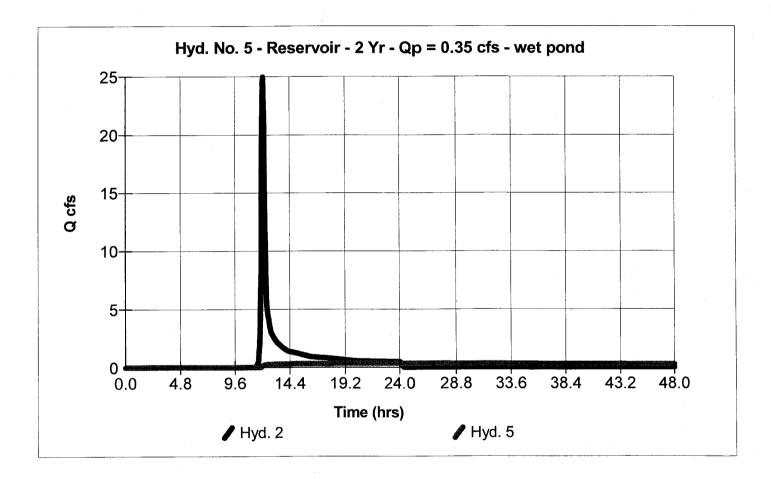
# **Hydrograph Summary Report**

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Maximum storage (cuft)	Hydrograph description
1	SCS Runoff	1.35	2	744	13,193			****	PRE-DEVELOPMENt
2	SCS Runoff	11.28	2	728	46,799				9069POST-DEVELOPMENT
5	Reservoir	0.27	2	1450	30,547	2	79.15	101,418	wet pond
						-			
				:					
						-			
						:			
					1				
Proi	i. file: bmp	#1 GPV	⊥ <b>V</b>	   F	⊥Return P∉	⊥ eriod: 1 y	r	Run da	te: 12-22-2003
1 10]	. mo. binp	,, i.o. v		'			·	1	Hydraflow Hydrographs by Inteligolya



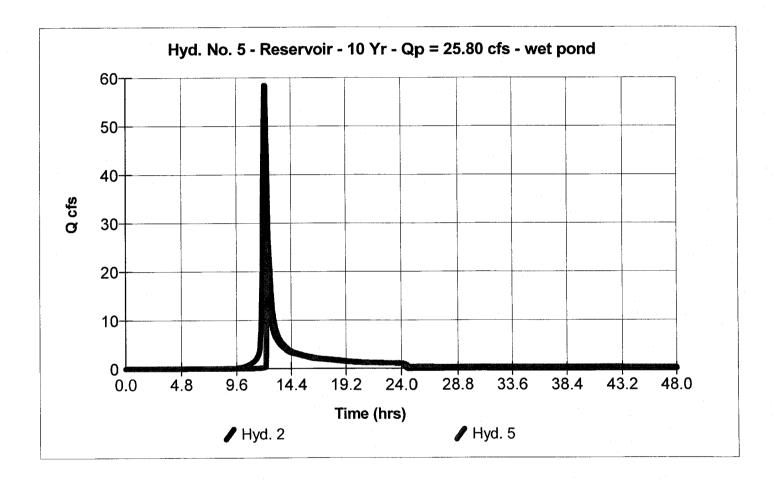
# **Hydrograph Summary Report**

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Maximum storage (cuft)	Hydrograph description			
1 2 5	SCS Runoff SCS Runoff Reservoir	3.92 20.72 0.35	2 2 2	738 728 1452	26,510 77,847 41,418	  2	80.07	  128,965	PRE-DEVELOPMENT 9069POST-DEVELOPMENT wet pond			
							÷					
						·						
	·											
Tanahara ayan ayan ayan ayan ayan ayan ayan a												
Pro	j. file: bmp	#1.GP\	<b>N</b>	F	Return Pe	eriod: 2 y	r	Run date: 12-22-2003				



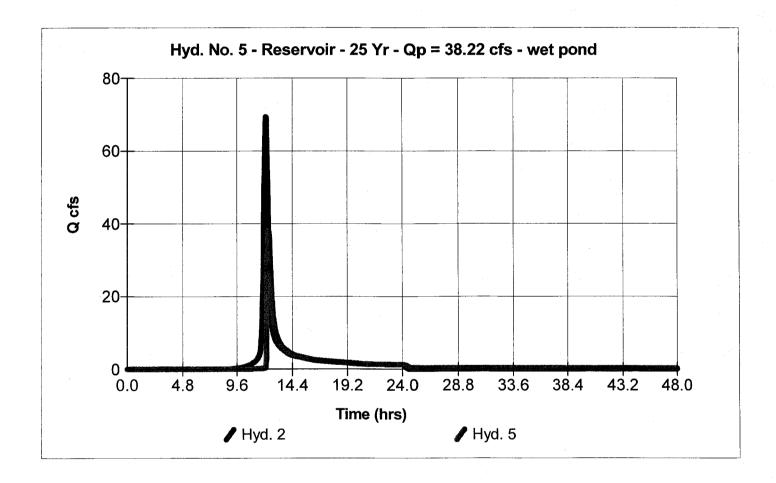
### **Hydrograph Summary Report**

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Maximum storage (cuft)	Hydrograph description
1	SCS Runoff	18.17	2	736	89,392			<del></del>	PRE-DEVELOPMENt
2	SCS Runoff	58.48	2	726	204,438			<del></del>	9069POST-DEVELOPMENT
5	Reservoir	25.80	2	744	164,551	2	80.75	150,920	wet pond
									·
Pro <sub>.</sub>	j. file: bmp	#1.GP\	W		Return P	eriod: 10	yr	Run da	te: 12-22-2003



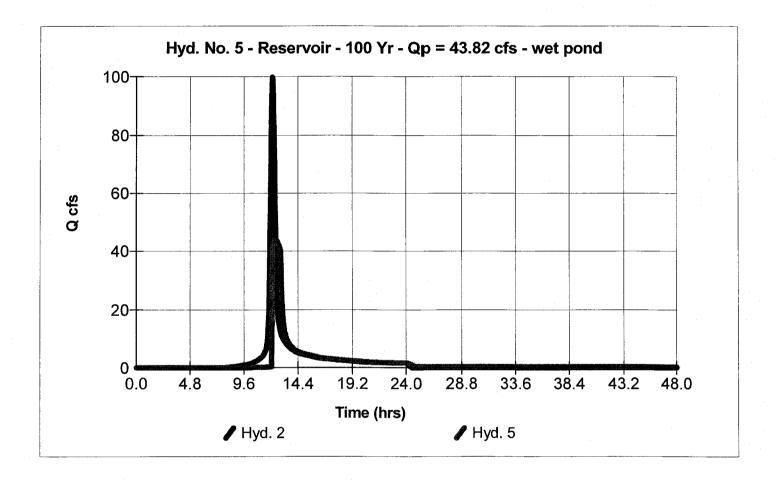
### **Hydrograph Summary Report**

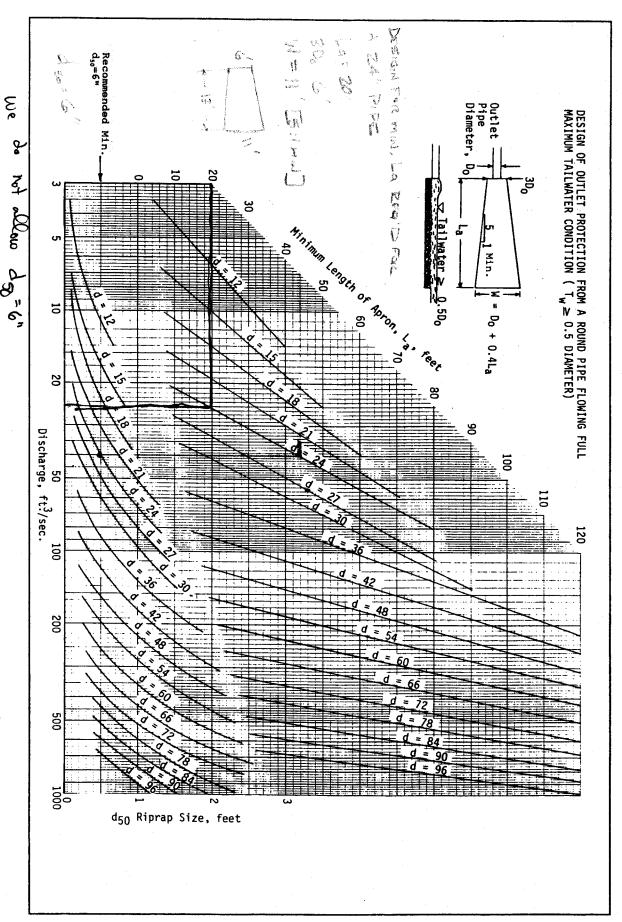
lyd. lo.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Maximum storage (cuft)	Hydrograph description
	SCS Runoff	22.72	2	736	109,139				PRE-DEVELOPMENt
	SCS Runoff	69.46	2	726	241,388				9069POST-DEVELOPMENT
	Reservoir	38.22	2	740	201,446	2	80.96	157,404	wet pond
	·								
							1		
	. file: bmp#	44 CDV	·		Return Pe	riod: OF		Dun de	te: 12-22-2003



### **Hydrograph Summary Report**

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Maximum storage (cuft)	Hydrograph description
1	SCS Runoff	35.81	2	736	166,279				PRE-DEVELOPMENt
2	SCS Runoff	99.85	2	726	344,740				9069POST-DEVELOPMENT
5	Reservoir	43.82	2	744	304,675	2	81.99	192,827	wet pond
				·					
Proi	j. file: bmp	#1.GPV	٧	F	Return Po	eriod: 100	) yr	Run da	te: 12-22-2003





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### Windsormeade Marketplace **BMP #1 BOUYANCE CALCULATIONS**

December 19, 2003

### Note: THESE CALCULATIONS PROVIDED ARE TO INSURE THE PRINCIPAL SPILLWAY / RISER DOES NOT HAVE THE TENDENCY TO FLOAT.

**ELEVATION OF RISER CREST =** 

**ELEVATION OF INVERT OF RISER =** 

AREA OF INSIDE DIMENSION OF RISER

7.1 square feet

(Diameter = 36" riser)

OUTSIDE DIMENSION OF RISER =

8.7 square feet

(Outside Diameter= 40") WEIGHT OF WATER DISPLACED BY AIR

Inside area of Riser \* (El. Of Riser Crest - El. Of riser invert)

\* Weight of water per cu. Ft. (62.4# / c.f.)

Neight of water displaced by air = (1 c.f. equals 62.4 Pounds)

Weight of water displaced by air 1,103 lbs.

**WEIGHT OF PRINCIPAL SPILLWAY / RISER** 

(Outside area of riser - Inside area of riser) \* (El. Of Riser Crest -El. Of riser invert) \* Weight of concrete per cu. Ft. (150# / c.f.)

Weight of Concrete Riser =

598 lbs.

Weight of Grouted Section=

5,212 lbs.

Weight of Extended Base Only =

4,579 lbs.

(Weight of Extended Base= 6.75' x 6.75' x 0.67' x 150# / c.f.)

Total Weight of Riser =

10,389 lbs.

Total Weight of Principal Spillway / Riser > Weight of Water Displaced. The riser will not float

The weight of the spillway grate, soil, and friction of soil was not taken into account. Riser weight at this point exceeds the bouyance uplift force.

### TEMPORARY SEDIMENT BASIN DESIGN DATA SHEET

(with or without an emergency spillway)

Project <u>V</u>	VINDSORMEDICE MARKETHAKE
Basin #	Location BEHALD SHOPPING CENTER
Total area o	draining to basin: 14.88 acres.  Show BE SIZED  FOR ZO. 90 ACRES ROLEIVE  WHICH IT Z.  IN 1977 Z.
Basin Volur	ne Design Which of 2.
Wet Storage	
1.	Minimum required volume = 67 cu. yds. x Total Drainage Area (acres).
	67 cu. yds. x $14.88$ acres = $997$ cu. yds.
2.	Available basin volume = 2434 cu. yds. at elevation 77.70. (From storage - elevation curve)
3.	Excavate cu. yds. to obtain required volume*.
	* Elevation corresponding to required volume = invert of the dewatering orifice.
4.	Available volume before cleanout required.
i	33 cu. yds. x $14.88$ acres = $491$ cu. yds.
5.	Elevation corresponding to cleanout level = $74.27$ .
	(From Storage - Elevation Curve)
6.	Distance from invert of the dewatering orifice to cleanout level = 3.5 ft (Min. = 1.0 ft.)
Dry Storage	
7.	Minimum required, volume = 67 cu. yds. x Total Drainage Area (acres).
	67 cu. yds. x 14.88 acres = 997 cu. yds.

- 8. Total available basin volume at crest of riser\* = 4920 cu. yds. at elevation 9019. (From Storage Elevation Curve)
  - \* Minimum = 134 cu. yds./acre of total drainage area.
- 9. Diameter of dewatering orifice = 3 in. DESIGNED WITH BANK.

  DESIGNED AND DOES NOT DESIGNED DAY DOWN TO ME TO THE TRANSPORT DAY THE TRANSPORT DAY TO THE T
- 10. Diameter of flexible tubing = \_\_\_\_\_ in. (diameter of dewatering orifice plus 2 inches).

### Preliminary Design Elevations

11. Crest of Riser = 30,19

Top of Dam = 31,00

Design High Water = 30.96

Upstream Toe of Dam = 72.00

### Basin Shape

12. Length of Flow Effective Width We We If > 2, baffles are not required Z./

If < 2, baffles are required

### Runoff

13.  $Q_2 = \frac{5.41}{4.73}$  cfs (From Chapter 5) 14.  $Q_{25} = \frac{44.73}{4}$  cfs (From Chapter 5)

### Principal Spillway Design

With emergency spillway, required spillway capacity Q<sub>p</sub> = Q<sub>2</sub> = \_\_\_\_\_ cfs. (riser and barrel)
 Without emergency spillway, required spillway capacity Q<sub>p</sub> = Q<sub>25</sub> = 44.73cfs. (riser and barrel)

16.	With	emergency	spillway
10.	4 4 1 7 1 1	Ciliciacine	Spinion ay

Assumed available head (h) = \_\_\_\_\_ ft. (Using  $Q_2$ )

h = Crest of Emergency Spillway Elevation - Crest of Riser Elevation

Without emergency spillway:

Assumed available head (h) =  $\frac{77}{80.19}$  ft. (Using Q<sub>25</sub>)

h = Design High Water Elevation - Crest of Riser Elevation

17. Riser diameter  $(D_r) = 36$  in. Actual head (h) = 1.9 ft. (From Plate 3.14-8.)

Note: Avoid orifice flow conditions.

- 18. Barrel length (l) = 61 ft.

  Head (H) on barrel through embankment = 9 ft.

  (From Plate 3.14-7).
- 19. Barrel diameter = 24 in. (From Plate 3.14-B [concrete pipe] or Plate 3.14-A [corrugated pipe]).
- 20. Trash rack and anti-vortex device

Diameter = 54 inches.

Height = 17 inches.

(From Table 3.14-D).

head token

### Emergency Spillway Design Nor REQUISED

- 21. Required spillway capacity  $Q_e = Q_{25} Q_p =$ \_\_\_\_cfs.
- 22. Bottom width (b) = \_\_\_\_ ft.; the slope of the exit channel (s) = \_\_\_\_ ft./foot; and the minimum length of the exit channel (x) = \_\_\_\_ ft. (From Table 3.14-C).

### Anti-Seep Collar Design

- 23. Depth of water at principal spillway crest (Y) = 9 ft.

  Slope of upstream face of embankment (Z) = 3 :1.

  Slope of principal spillway barrel  $(S_b) = 1.18$  %

  Length of barrel in saturated zone  $(L_s) = 3$  ft.
- 24. Number of collars required =  $\frac{Z}{d}$  dimensions =  $\frac{6' \times 6'}{d}$  (from Plate 3.14-12).

### Final Design Elevations

Design High Water = 90.96

Emergency Spillway Crest = Principal Spillway Crest = 90.19

Dewatering Orifice Invert = 77.70

Cleanout Elevation = 74.27

Elevation of Upstream Toe of Dam or Excavated Bottom of "Wet Storage Area" (if excavation was performed) = 73.0

### STORAGE ELEVATION TABLE FOR SEDIMENT BASIN 2 WINDSORMEADE MARKETPLACE AES Project No.:9069-02 December 20, 2003

### PROPOSED ESTIMATED POND(S) VOLUME

Elevation	<u>Depth</u>	Area (sq. ft.)	Incremental Volume (cu. ft.)	Inc. Volume (cu. yd.)	Sum Volume (cu. ft.)	Sum Volume (cu. yd.)
<u>85</u>	<u>0</u>	<u>6743</u>	<u>Q</u>	0	0	0
86	1	7,390	7,067	262	7,067	262
87	• 1	8,072	7,731	286	14,798	548
88	1	8,765	8,419	312	23,216	860
89	1	9,490	9,128	338	32,344	1,198
90	1	. 10,238	9,864	365	42,208	1,563

### TEMPORARY SEDIMENT BASIN DESIGN DATA SHEET

(with or without an emergency spillway)

Project WINDSORMER DE	MARKETPLACE
Basin #	Location FRANT OF SITE
Total area draining to basin: _	5.39 acres.
Basin Volume Design	

### Wet Storage:

- 1. Minimum required volume = 67 cu. yds. x Total Drainage Area (acres).

  67 cu. yds. x 5.39 acres = 36/ cu. yds.
- 2. Available basin volume = 361 cu. yds. at elevation 86.35. (From storage elevation curve)
- 3. Excavate \_\_\_\_ cu. yds. to obtain required volume\*.
  - \* Elevation corresponding to required volume = invert of the dewatering orifice.
- 4. Available volume before cleanout required.

- 5. Elevation corresponding to cleanout level = <u>95.50</u>.

  (From Storage Elevation Curve)
- 6. Distance from invert of the dewatering orifice to cleanout level = ft. (Min. = 1.0 ft.)

### **Dry Storage:**

7. Minimum required volume = 67 cu. yds. x Total Drainage Area (acres).

67 cu. yds. x 5 30 acres = 361 cu. yds.

8. Total available basin volume at crest of riser\* = 722 cu. yds. at elevation <u>\$7.55</u>. (From Storage - Elevation Curve)

- \* Minimum = 134 cu. yds./acre of total drainage area.
- 9. Diameter of dewatering orifice = \_\_\_\_\_\_in. Mill
- 10. Diameter of flexible tubing = \_\_\_\_\_in. (diameter of dewatering orifice plus 2 inches).

### Preliminary Design Elevations

11. Crest of Riser = 97.55

Top of Dam = 90.50

Design High Water = <u>88.35</u>

Upstream Toe of Dam =  $g_{c.0.0}$ 

### Basin Shape

12. <u>Length of Flow</u> <u>L</u> = <u>2</u>
Effective Width We

If > 2, baffles are not required \_\_\_\_\_

If < 2, baffles are required

### Runoff

13.  $Q_2 = cfs$  (From Chapter 5)

14.  $Q_{25} = 700$  cfs (From Chapter 5)

### Principal Spillway Design

15. With emergency spillway, required spillway capacity  $Q_p = Q_2 =$ \_\_\_\_ cfs. (riser and barrel)

Without emergency spillway, required spillway capacity  $Q_p = Q_{25} = \frac{1}{2}$  cfs. (riser and barrel)

10. With Chick Court, Spinson	16.		Vith	emergency	spillway
-------------------------------	-----	--	------	-----------	----------

Assumed available head (h) = \_\_\_\_\_ ft. (Using  $Q_2$ )

h = Crest of Emergency Spillway Elevation - Crest of Riser Elevation

Without emergency spillway:

Assumed available head (h) = 0.8 ft. (Using  $Q_{25}$ )

h = Design High Water Elevation - Crest of Riser Elevation

17. Riser diameter  $(D_r) = 34$  in. Actual head (h) = 6 ft. (From Plate 3.14-8.)

Note: Avoid orifice flow conditions.

- 18. Barrel length (l) = 148 ft.

  Head (H) on barrel through embankment = 3.5 ft.

  (From Plate 3.14-7).
- 19. Barrel diameter = \_\_\_\_\_ in.

  (From Plate 3.14-B [concrete pipe] or Plate 3.14-A [corrugated pipe]).
- 20. Trash rack and anti-vortex device

  Diameter = 42 inches.

  Height = 13 inches.

  (From Table 3.14-D).

### Emergency Spillway Design

NOT REQUIRED

- 21. Required spillway capacity  $Q_e = Q_{25} Q_p =$ \_\_\_\_cfs.
- 22. Bottom width (b) = \_\_\_\_ ft.; the slope of the exit channel (s) = \_\_\_\_ ft./foot; and the minimum length of the exit channel (x) = \_\_\_\_ ft. (From Table 3.14-C).

### Anti-Seep Collar Design Not Required

- 23. Depth of water at principal spillway crest  $(Y) = ____ ft$ .

  Slope of upstream face of embankment  $(Z) = ____ :1$ .

  Slope of principal spillway barrel  $(S_b) = ____ %$ Length of barrel in saturated zone  $(L_s) = ____ ft$ .
- 24. Number of collars required = \_\_\_\_\_ dimensions = \_\_\_\_\_ (from Plate 3.14-12).

### Final Design Elevations

Design High Water = 90.50

Design High Water = 90.55

Emergency Spillway Crest = 91.55

Principal Spillway Crest = 91.55

Dewatering Orifice Invert = 95.35

Cleanout Elevation = 95.35

Elevation of Upstream Toe of Dam or Excavated Bottom of "Wet Storage"

Area" (if excavation was performed) =  $\mathcal{G}(s, 0)$ 

12-22-2003

No. Lines: 17

Project file: stormsystem#1.stm

### **Storm Sewer Tabulation**

																				· · · · · · ·
	17	16	5	4	<del>ن</del> 3	12	<u> </u>	10	9	∞	7	<u>თ</u>	თ	4	ω 	2	<u> </u>		Line	Station
	6	Ωı	14	13	12	4	6	4	000		o	ڻ.	4	ω	2	_	End	<u>.</u>	7	ġ
j	138.0	24.0	151.0	170.0	109.0	300.0	58.0	24.0	56.0	64.0	24.0	252.0	252.0	149.0	243.0	203.0	192.0	(ft)		Len
	0.62	2.15	1.70	0.66	0.00	0.00	0.61	1.25	0.45	1.80	1.46	1.14	1.25	1.63	0.00	0.66	1.11	(ac)	Incr	Drng
	0.62	2.15	1.70	2.36	2.36	2.36	0.61	1.86	0.45	2.25	1.46	3.22	6.62	12.47	12.47	13.13	16.49	(ac)	Total	Drng Area
	0.70	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	(C)	0	Rnoff
	0.43	1.94	1.53	0.59	0.00	0.00	0.55	1.13	0.41	1.62	1.31	1.03	1.13	1.47	0.00	0.59	1.00		Incr	
	0.43	1.94	1.53	2.12	2.12	2.12	0.55	1.67	0.41	2.03	1.31	2.77	5.83	11.10	11.10	11.69	14.72		Total	Area x C
	5.0	5.0	5.0	5.0	5.0	5:0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	(min		
	5.0	5.0	5.0	5.7	6.4	6.8	5.0	ე ა	5.0	5.4	5.0	5.9	7.5	8.3	8.8	9.5	10.1			Тс
	7.0	7.0	7.0	6.8	6.7	6.6	7.0	6.9	7.0	6.9	7.0	6.8	6.4	6.2	6.1	6.0	5.9			Rain
	3.04	13.5	10.7	14.4	14.1	13.9	3.84	11.5	2.83	13.9	9.19	18.7	37.2	69.0	68.0	69.9	86.4			n Total
	_	_	$\overline{}$	6 15.9	_	$\overline{}$	$\overline{}$	_	_		_			$\overline{}$		<del></del>	1 106.	<u> </u>		Cap
																<u></u> თ				Vel
																•			<u>v</u>	<u>-</u>
																				Pipe
																			-	
																		(₹)	<u></u>	Invert Elev
	82.72	81.46	83.76	82.91	82.37	80.20	80.97	80.20	79.00	77.15	82.72	81.46	80.20	79.45	78.23	77.15	76.10	∄	Dn	Elev
	86.93	86.35	88.11	87.36	86.53	85.96	85.41	84.89	82.84	82.58	86.66/	86.46/	85.61	84.31	83.89	82.82	81.42	Æ	두	픙
	86.6	86.2														82.3	80.7	(#		HGL Elev
			_					<sup>2</sup> 8	3 				`	_	7					G
	9.00	7.80	9.60	0.90	3.50	1.50	9.40	8.29	6.50	5.50	8.10	8.10	7.80	8.29	1.00	0.00	3.50	<b>£</b>	두	rnd / Ri
I	88.10	87.80	90.90	93.50	91.50	88.29	88.29	88.29	85.50	86.50	88.10	87.80	88.29	91.00	90.00	86.50	0.00	( <del>t</del> )	Dn	Grnd / Rim Elev
	1-18 to	1-17 t	1-16 to	1-15 to	1-14 to	1-13 t	1-12 to	1-11 to	1-10 tc	1-9 to	1-7 to	1-6 to	1-5 to	1-4 to	1-3 to	1-2 to	1-1 to			Ţ.
	0 1-7	ე 1-6	o 1-15	0 1-14	ວ 1-13	ა 1-5	5 1-11	o 1-5	ວ 1-9	1-2	1-8	1-7	1-6	1-5	1-4	<del>1</del> -3	1-2			Line ID
		6 138.0 0.62 0.62 0.70 0.43 0.43 5.0 5.0 7.0 3.04 8.30 2.47 15 1.65 85.00 82.72 86.93 86.62 89.00	5 24.0 2.15 2.15 0.90 1.94 1.94 5.0 5.0 7.0 13.54 39.18 4.31 24 3.00 82.18 81.46 86.35 86.26 87.80 87.80 6 138.0 0.62 0.62 0.70 0.43 0.43 5.0 5.0 7.0 3.04 8.30 2.47 15 1.65 85.00 82.72 86.93 86.62 89.00 88.10	14       151.0       1.70       1.70       0.90       1.53       1.53       5.0       5.0       7.0       10.70 15.83       3.41       24       0.49       84.50       83.76       88.11 27.77 89.60       90.90         5       24.0       2.15       2.15       0.90       1.94       1.94       5.0       5.0       7.0       13.54 39.18       4.31       24       3.00       82.18       81.46       86.35 86.26 87.80       87.80         6       138.0       0.62       0.62       0.70       0.43       0.43       5.0       5.0       7.0       3.04 8.30       2.47       15       1.65       85.00       82.72       86.93 86.62 89.00       88.10	13 170.0 0.66 2.36 0.90 0.59 2.12 5.0 5.7 6.8 14.46 15.99 4.60 24 0.50 83.76 82.91 87.36 86.67 90.90 93.50 14 151.0 1.70 1.70 0.90 1.53 1.53 5.0 5.0 7.0 10.70 15.83 3.41 24 0.49 84.50 83.76 88.11 87.77 89.60 90.90 5 24.0 2.15 2.15 0.90 1.94 1.94 5.0 5.0 7.0 13.54 39.18 4.31 24 3.00 82.18 81.46 86.35 86.26 87.80	12 109.0 0.00 2.36 0.90 0.00 2.12 5.0 6.4 6.7 14.14 15.92 4.50 24 0.50 82.91 82.37 86.53 86.10 93.50 91.50 13 170.0 0.66 2.36 0.90 0.59 2.12 5.0 5.7 6.8 14.46 15.99 4.60 24 0.50 83.76 82.91 87.36 86.67 90.90 93.50 14 151.0 1.70 1.70 0.90 1.53 1.53 5.0 5.0 7.0 10.70 15.83 3.41 24 0.49 84.50 83.76 88.11 87.77 89.60 90.90 5 24.0 2.15 2.15 0.90 1.94 1.94 5.0 5.0 7.0 13.54 39.18 4.31 24 3.00 82.18 81.46 86.35 86.26 87.80 87.80 6 138.0 0.62 0.62 0.70 0.43 0.43 5.0 5.0 7.0 3.04 8.30 2.47 15 1.65 85.00 82.72 86.93 86.62 89.00 88.10	4 300.0 0.00 2.36 0.90 0.00 2.12 5.0 6.8 6.6 13.94/19.24 4.44 24 0.72 82.37 80.20 85.96 84.82 91.50 88.29  12 109.0 0.00 2.36 0.90 0.00 2.12 5.0 6.4 6.7 14.14/15.92 4.50 24 0.50 82.91 82.37 86.53 86.10 93.50 91.50  13 170.0 0.66 2.36 0.90 0.59 2.12 5.0 5.7 6.8 14.46/15.99 4.60 24 0.50 83.76 82.91 87.36 86.67 90.90 93.50  14 151.0 1.70 1.70 0.90 1.53 1.53 5.0 5.0 7.0 10.70 15.83 3.41 24 0.49 84.50 83.76 88.11 87.77 89.60 90.90  5 24.0 2.15 2.15 0.90 1.94 1.94 5.0 5.0 7.0 13.54 39.18 4.31 24 3.00 82.18 81.46 86.35 86.26 87.80 87.80  6 138.0 0.62 0.62 0.70 0.43 0.43 5.0 5.0 7.0 3.04 8.30 2.47 15 1.65 85.00 82.72 86.93 86.62 89.00 88.10	10 58.0 0.61 0.61 0.61 0.90 0.55 5.0 5.0 7.0 3.84 13.22 3.13 15 4.19 83.40 80.97 85.41 85.20 89.40 88.29 4 300.0 0.00 2.36 0.90 0.00 2.12 5.0 6.8 6.6 13.94 19.24 4.44 24 0.72 82.37 80.20 85.96 48.82 91.50 88.29 12 109.0 0.00 2.38 0.90 0.00 2.12 5.0 6.4 6.7 14.14 15.92 4.50 24 0.50 82.91 82.37 86.53 86.10 93.50 91.50 13 170.0 0.66 2.38 0.90 0.59 2.12 5.0 5.7 6.8 14.46 15.99 4.60 24 0.50 83.76 82.91 87.36 86.67 90.90 93.50 14 151.0 1.70 1.70 0.90 1.53 1.53 5.0 5.0 7.0 10.70 15.83 3.41 24 0.49 84.50 83.76 82.91 87.36 86.67 90.90 93.50 5 24.0 2.15 2.15 0.90 1.94 1.94 5.0 5.0 7.0 13.54 39.18 4.31 24 3.00 82.18 81.46 86.35 86.26 87.80 87.80 6 138.0 0.62 0.62 0.70 0.43 0.43 5.0 5.0 7.0 3.04 8.30 2.47 15 1.65 85.00 82.72 86.93 86.62 89.00 88.10	4       240       1.25       1.86       0.90       1.13       1.67       5.0       5.3       6.9       11.58       40.51       3.68       24       3.21       80.97       80.20       84.89       84.82       88.29       88.29       88.29         10       58.0       0.61       0.61       0.90       0.05       5.5       5.0       7.0       3.84       13.22       3.13       15       4.19       83.40       80.97       85.41       85.20       89.40       88.29         12       109.0       0.00       2.36       0.90       0.00       2.12       5.0       6.4       6.7       14.14       15.92       4.44       24       0.72       82.37       80.20       85.96       84.82       91.50         13       170.0       0.66       2.36       0.90       0.59       2.12       5.0       5.7       6.8       14.46       15.99       4.60       24       0.50       82.91       82.37       86.53       86.10       93.50       91.50         14       151.0       1.70       1.53       1.53       5.0       5.0       7.0       10.70       15.83       3.41       24       0.49       84.50 <t></t>	8 56.0 0.45 0.45 0.45 0.90 0.41 0.41 5.0 5.0 7.0 2.83 8.63 2.31 15 1.79 80.00 79.00 82.84 82.73 88.50 85.50 10.51	1 64.0 1.80 2.25 0.90 1.62 2.03 5.0 5.4 6.9 13.95 38.45 4.44 24 2.89 79.00 77.15 82.58 82.33 85.50 86.50 8 56.0 0.45 0.45 0.45 0.45 0.90 0.41 0.41 5.0 5.0 7.0 2.83 8.63 2.31 15 1.79 80.00 79.00 82.84 82.73 86.50 85.50 10 58.0 0.61 0.90 0.41 0.41 5.0 5.0 5.3 6.9 11.58 40.51 3.68 24 3.21 80.97 80.20 84.89 84.82 88.29 88.29 10 58.0 0.61 0.90 0.55 0.55 5.0 5.0 5.0 7.0 3.84 13.22 3.13 15 4.19 83.40 80.97 80.20 84.89 84.82 88.29 88.29 12 10 10 10 10 10 10 10 10 10 10 10 10 10	6 24.0 1.46 1.46 0.50 1.31 1.31 5.0 5.0 7.0 9.19 38.63 2.93 24 2.92 83.42 82.72 86.66 86.62 88.10 1 1 64.0 1.80 2.25 0.90 1.62 2.03 5.0 5.4 6.9 13.95 38.45 4.44 24 2.80 79.00 77.15 82.58 82.33 85.50 86.50 85.50 1.25 1.26 0.45 0.45 0.90 0.41 0.41 5.0 5.0 7.0 2.83 8.63 2.31 15 1.79 80.00 79.00 82.84 82.73 86.50 85.50 1 1 58.0 0.61 0.61 0.61 0.90 0.55 0.55 5.0 5.0 7.0 3.84 13.22 3.13 15 1.79 80.00 79.00 82.84 82.73 88.29 88.29 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	5         252.0         1.14         3.22         0.90         1.03         2.77         5.0         5.9         6.8         18.75         47.16         2.65         36         0.50         22.77         8.0         6.9         18.75         47.16         2.65         36         0.50         82.72         81.46         88.46         88.26         88.10         87.80           6         24.0         1.46         1.46         0.90         1.62         20.3         5.0         5.0         7.0         9.19         38.83         2.93         24         2.82         28.342         82.72         86.86         38.60         88.10           8         56.0         0.45         0.45         0.90         0.41         5.0         5.0         7.0         2.83         8.63         2.31         1.5         1.79         80.00         77.15         82.59         88.50         88.50           4         24.0         1.25         1.86         0.90         0.41         5.0         5.0         5.0         7.0         3.84         13.22         3.1         1.5         4.19         83.40         89.97         88.27         88.50         88.29           10         <	4 2520 1.25 6.62 0.90 1.13 5.83 5.0 7.5 6.4 37.29 47.16 5.28 36 0.50 81.46 80.20 85.81 84.82 87.90 88.29 5.220 1.14 3.22 0.90 1.03 2.77 5.0 5.9 6.8 18.75 47.16 2.65 36 0.50 82.72 81.46 86.46 86.26 88.10 87.80 6.240 1.46 1.46 0.90 1.31 1.31 5.0 5.0 7.0 9.19 38.63 2.83 2.4 2.92 83.42 82.72 86.666 86.26 88.10 87.80 6.25 8.20 1.25 1.80 0.90 1.42 2.03 5.0 5.4 6.9 13.95 38.45 4.44 24 2.89 79.00 77.15 82.58 82.33 85.50 85.50 85.50 85.50 1.25 1.86 0.90 0.41 0.41 5.0 5.0 7.0 2.83 8.63 2.31 15 1.79 80.00 79.00 82.84 82.73 86.50 85.50 85.50 1.25 1.86 0.90 0.55 0.55 5.0 5.0 5.0 5.0 7.0 3.84 13.22 3.13 15 1.79 80.00 79.00 82.84 82.73 86.50 88.29 1.25 1.25 1.25 1.25 1.25 1.25 1.25 1.25	3 1490 183 1247 090 1.47 11.10 6.0 8.3 6.2 6907 101.9 5.50 48 0.50 80.20 79.45 84.31 83.96 68.29 91.00 4 282.0 1.25 862 0.90 1.13 5.83 5.0 7.5 6.4 37.29 47.16 5.28 36 0.50 81.46 80.20 85.61 86.27 81.40 82.29 5 282.0 1.14 3.22 0.90 1.03 2.77 5.0 5.9 6.8 18.75 47.16 2.65 36 0.50 81.46 80.20 85.61 86.26 88.29 6 24.0 1.46 1.46 0.90 1.31 1.31 5.0 5.0 7.0 9.19 38.63 2.83 24 2.82 83.42 82.72 81.46 86.46 86.26 88.10 87.90 8 56.0 0.45 0.45 0.90 0.41 0.41 5.0 5.0 7.0 2.83 8.63 2.83 2.83 2.83 2.83 2.83 2.83 2.83 2.8	2 243.0 0.00 12.47 0.90 0.00 11.10 5.0 8.8 6.1 68.05 101.8 5.42 49 0.50 79.45 78.23 83.89 83.35 91.00 90.00 3 1440 1630 12.47 0.90 1.47 11.10 5.0 8.3 6.2 69.07 101.9 5.50 48 0.50 80.20 79.46 64.31 83.96 83.95 91.00 90.00 142 252.0 12.5 662 0.90 1.33 5.83 5.0 7.5 6.4 37.29 47.16 5.28 36 0.50 81.46 90.20 88.61 84.22 87.80 88.29 91.00 142 252.0 11.44 3.22 0.90 1.03 2.77 5.0 5.9 6.8 11.87 47.16 5.28 36 0.50 82.72 81.46 90.40 86.26 88.10 87.80 11.10 1	1 2030 0.66 13.13 0.90 0.59 11.69 5.0 9.5 6.0 69.99 10.48 5.57 48 0.53 77.15 22.82 62.33 90.00 66.50 2 2430 0.00 12.47 0.90 11.10 5.0 8.8 6.1 68.05 101.8 5.42 48 0.50 78.45 78.23 83.89 63.35 91.00 90.00 3 1440 1.63 12.47 0.90 11.13 5.83 5.0 7.5 8.4 37.29 47.16 5.28 36 0.50 81.46 80.20 79.45 84.31 83.98 83.89 63.35 91.00 90.00 65.20 11.14 322 0.90 11.13 5.83 5.0 7.5 8.4 37.29 47.16 5.28 36 0.50 81.46 80.20 79.45 84.31 83.98 83.89 63.35 91.00 90.00 65.20 11.14 322 0.90 11.13 5.0 5.0 7.5 8.4 37.29 47.16 5.28 36 0.50 81.46 80.20 79.45 84.31 83.98 83.89 83.29 91.00 65.20 11.14 32.2 0.90 11.31 1.31 5.0 5.0 7.0 91.9 38.63 2.93 24 2.92 83.42 82.72 81.48 88.49 88.25 88.10 87.80 82.29 85.00	End 1920 1.11 1 16.49 0.90 1.00 14.72 5.0 10.1 5.9 86.41 106.2 6.89 48 0.55 77.15 76.10 81.42 20.72 80.50 0.00 1 1 10 5.0 8.8 16.1 88.06 101.8 5.7 4.8 0.55 77.15 76.10 81.42 20.72 80.50 0.00 88.50 1 10.00 11.10 5.0 8.8 6.1 88.06 101.8 5.7 4.8 0.55 77.15 76.10 81.42 20.00 88.50 1 1.00 11.10 5.0 8.8 6.1 88.06 101.8 5.42 48 0.55 77.15 82.82 27 82.33 80.00 88.50 1 10.00 11.10 5.0 8.8 6.1 88.06 101.8 5.42 48 0.50 77.15 82.82 27 82.30 80.00 88.29 10.00 11.10 5.0 8.3 6.2 88.07 101.9 5.50 48 0.50 77.15 82.80 82.20 10.00 11.10 5.0 8.3 6.2 88.07 101.9 5.50 48 0.50 77.15 82.80 82.20 10.00 82.20 82.20 11.10 11.10 5.0 8.3 6.2 88.07 101.9 5.50 48 0.50 82.72 81.46 80.45 88.25 91.00 82.20 82.20 11.10 11	China   (th)   (ac)   (ac)   (c)   (cin)   (	Trans   Trans   Trans   Trans   Incr   Incr

NOTES: Intensity = 140.36 / (Inlet time + 19.80) ^ 0.93; Return period = 10 Yrs.



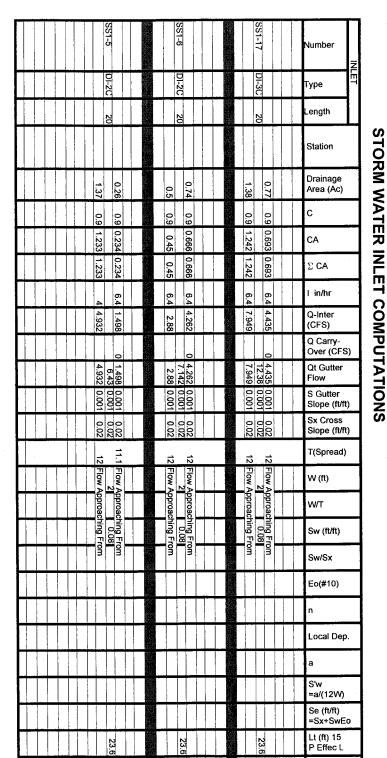
5248 Olde Towne Road, Suite 1 Williamsburg, Virginia 23188 (757) 253-0040 Fax: (757) 220-8994

PROJECT
PROJECT NO.
SUBJECT
SHEET NO.
DATE
BY

WINDSORMEADE MARKETPLACE
9069
Spread Calc's
1

## STORM WATER INLET COMPUTATIONS

SS1-7	SS1-8	SS1-16	SS1-15	Number ≅
DI-2C	DI-2C	DI-ZC	DI-2B	Type Z
20	20	20	6	Length
				Station
0.51 0.63	0.71	0.97	0.66	Drainage Area (Ac)
0.9	0.9	0.9	0.9	С
0.459	0.639	0.873 0.657	0.594	CA
0.459 0.567	0.639	0.873	0.594	Σ CA
6.4	6.4	6.4	6.4	l in/hr
2.938 3.629	4.09 4.262	5.587 4.205	3.802	Q-Inter (CFS)
0 0		1.248	o	Q Carry- Over (CFS)
2.938 6.566 3.629	4.09 8.352 4.262	6.835 11.04 4.205	3.802	Qt Gutter Flow
0.001 0.001	0.001 0.001 0.001	0.001 0.001 0.001	0.01	S Gutter Slope (ft/ft)
0.02	0.02 0.02 0.02	0.02 0.02 0.02	0.02	Sx Cross Slope (ft/ft)
12	12 12	12 12	10	T(Spread)
Flow A	Flow A	Flow A	2	W (ft)
Approaching 2. 0.1 Approaching	рргоас	Approaching Approaching Approaching	0.2	W/T
Flow Approaching From 0.08	low Approaching From 2   0.08   100	low Approaching From 21 0.08 low Approaching From	0.08	Sw (ft/ft)
From .08	om	om	4	Sw/Sx
			0.564	Eo(#10)
			0.015	n
			2	Local Dep.
			3.44	а
			0.143	S'w =a/(12W)
			0.101	Se (ft/ft) =Sx+SwEo
23.6	23.6	23.6	13	Lt (ft) 15 P Effec L
0.245	0.287	0.346	0.462	L/Lt d (ft)
0.46	0.46	0.46	0.672	E(#16) h (ft)
0.532	0.624	0.752	2.554	Q Int CFS d/h
12.23	14.36	17.29	1.248	Q Carryover Spread
				Remark



0.241

0.524

0.259

0.46

0.562

12.93

0.373

0.46

0.812

18.67

L/Lt

E(#16)

Q Int CFS d/h

Q Carryover

Spread

(ft)

(ft)

ď

### CONSULTING ENGINEERS

5248 Olde Towne Road, Suite 1 Williamsburg, Virginia 23188 (757) 253-0040 Fax: (757) 220-8994

PROJECT NO. SUBJECT SHEET NO. DATE

BWS

Spread Calc's

	SS1-18	SS1-9	SS1-3 SS1-10	SS3-2 SS1-2	881-11	1-12	Number
	DI-7	DI-2C	DI-28	DI-28 DI-28	D1-2C	DI-20	Type Z
	2.5	20	8	88 88	20		Length
							Station
	0.31	0.96 0.84	0.66	1.11 0.54	0.61	0.64	Drainage Area (Ac)
	0.6	0.9	0.9	0.9	0.9	0.9	С
	0.186	0.864 0.756	0.594 0.405	0.999	0.549	0.576	CA
	0.186	0.864 0.756	0.594	0.999	0.549	0.576	ΣCA
	6.4	6.4	6.4	6.4	6.4	6.4	
	1.19	5.53 4.838	3.802 2.592	6.394 3.11	3.514	3.686	Q-Inter (CFS)
	0	1.614 0.904	0 0	0 2.197		1.094	Q Carry- Over (CFS)
	1.19 2.381 1.19	7.143 12.89 5.742	3.802 2.592	6.394 5.308	3.514		Qt Gutter Flow
	0.001 0.001 0.001	0.001 0.001 0.001	0.01	0.01 0.01	0.001	0.001	S Gutter Slope (ft/ft)
	0.02 0.02 0.02	0.02	0.02	0.02	0.02	0.02	Sx Cross Slope (ft/ft)
	10	12 12	10 8.7	12 11.5		·	T(Spread)
■ 1 1 1 1 1 1 1 1				5 N	12	2	
			2 2	2		2	W (ft)
			2 0.23	2 2 0.167 5 2 0.174		2	
			2 2	2		2	W (ft)
	0 Flow Approaching From 2 0.08 0 Flow Approaching From	Plow Approaching From 0.08 Flow Approaching From	2 0.2 0.08 4 2 0.23 0.08 4	2 0.167 0.08 4 2 0.174 0.08 4		2 Flow Approaching From	W (ft)  W/T  Sw (ft/ft)  Sw/Sx
			2 0.2 0.08 4 0.564 2 0.23 0.08 4 0.599	2 0.167 0.08 4 0.456 2 0.174 0.08 4 0.456		2 Flow Approaching From	W (ft)  W/T  Sw (ft/ft)  Sw/Sx  Eo(#10)
			2 0.2 0.08 4 2 0.23 0.08 4	2 0.167 0.08 4 2 0.174 0.08 4		2 Flow Approaching From	W (ft)  W/T  Sw (ft/ft)  Sw/Sx
			2 0.23 0.08 4 0.594 0.5 2 0.23 0.08 4 0.599 0.5	2 0.167 0.08 4 0.456 0.0 2 0.174 0.08 4 0.456 0.0		2 Flow Approaching From	W (ft)  W/T  Sw (ft/ft)  Sw/Sx  Eo(#10)
			2 0.2 0.08 4 0.564 0.015 2 3.44 2 0.23 0.08 4 0.599 0.015 2 3.44	2 0.167 0.08 4 0.456 0.015 2 3.44 2 0.174 0.08 4 0.456 0.015 2 3.44		2 Flow Approaching From	W (ft) W/T Sw (ft/ft) Sw/Sx Eo(#10) In Local Dep.
			2 0.2 0.08 4 0.564 0.015 2 3.44 0.143 2 0.23 0.08 4 0.599 0.015 2 3.44 0.143	2 0.167 0.08 4 0.456 0.015 2 3.44 0.143 2 0.174 0.08 4 0.456 0.015 2 3.44 0.143		2 Flow Approaching From	W (ft) W/T Sw (ft/ft) Sw/Sx Eo(#10) In Local Dep. a S'w =a/(12W)
			2 0.2 0.08 4 0.564 0.015 2 3.44 0.143 0.101 2 0.23 0.08 4 0.599 0.015 2 3.44 0.143 0.106	Z 0.167     0.08     4 0.456     0.015     2 3.44     0.143     0.085       Z 0.174     0.08     4 0.456     0.015     2 3.44     0.143     0.085		2 Flow Approaching From	W (ft) W/T Sw (ft/ft) Sw/Sx Ec(#10) In Local Dep. a S'w =a/(12W) Se (ft/ft) =Sx+SwEo
	Flow Approaching From 2 0.08 Flow Approaching From	Flow Approaching From 23.6 Flow Approaching From 23.6	2     0.2     0.08     4     0.564     0.015     2     3.44     0.143     0.101     13       2     0.23     0.08     4     0.599     0.015     2     3.44     0.143     0.106     10.75	Z 0.167     0.08     4 0.456     0.015     Z 3.44     0.143     0.085     17.88       Z 0.174     0.08     4 0.456     0.015     Z 3.44     0.143     0.085     16.53	Flow Approaching From	2 Flow Approaching From	W (ft) W/T Sw (ft/ft) Sw/Sx Eo(#10) In Local Dep. a S'w =a/(12W) Se (ft/ft) =Sx+SwEo Lt (ft) 15 P Effec L
		Flow Approaching From 0.08 Flow Approaching From Flow Approaching From	Z     0.2     0.08     4     0.564     0.015     2     3.44     0.143     0.101     13     0.515       Z     0.23     0.08     4     0.599     0.015     2     3.44     0.143     0.106     10.75     0.744	Z 0.167     0.08     4     0.456     0.015     Z     3.44     0.143     0.085     17.88     0.448       Z 0.174     0.08     4     0.456     0.015     Z     3.44     0.143     0.085     16.53     0.484	Flow Approaching From	2 Flow Approaching From	W (ft) W/T Sw (ft/ft) Sw/Sx Eo(#10) In Local Dep. a S'w =a/(12W) Se (ft/ft) =Sx+SwEo Lt (ft) 15 P Effec L L/Lt d (ft)
	Flow Approaching From 2 0.08 Flow Approaching From	Flow Approaching From 23.6 0.383 0.46 Flow Approaching From 23.6 0.383 0.46	2     0.2     0.08     4     0.564     0.015     2     3.44     0.143     0.101     13     0.815     0.821       2     0.23     0.08     4     0.599     0.015     2     3.44     0.143     0.106     10.75     0.744     0.914	Z 0.167     0.08     4     0.456     0.015     Z 3.44     0.143     0.085     17.88     0.448     0.656       2 0.174     0.08     4     0.456     0.015     2     3.44     0.143     0.085     16.53     0.484     0.696	Flow Approaching From	2 Flow Approaching From	W (ft) W/T Sw (ft/ft) Sw/Sx Eo(#10) In Local Dep. a S'w =a/(12W) Se (ft/ft) =Sx+SwEo Lt (ft) 15 P Effec L
	Flow Approaching From 2 0.08 Flow Approaching From	Flow Approaching From 23.6 0.383 0.46 0.833	Z     0.2     0.08     4     0.564     0.015     Z     3.44     0.143     0.101     13     0.615     0.821     3.121       Z     0.23     0.08     4     0.599     0.015     Z     3.44     0.143     0.106     10.75     0.744     0.914     2.369	Z 0.167     0.08     4     0.456     0.015     Z 3.44     0.143     0.085     17.88     0.448     0.656     4.196       Z 0.174     0.08     4     0.456     0.015     2     3.44     0.143     0.085     16.53     0.484     0.696     3.694	Flow Approaching From	2 Flow Approaching From 274 6 0 298 0 48 10 821	W (ft)  W/T  Sw (ft/ft)  Sw/Sx  Eo(#10)  n  Local Dep.  a a  S'w =a/(12W)  Se (ft/ft)  =Sx+SwEo  Lt (ft) 15  P Effec L  L/Lt d (ft)  E(#16) h  E(#16) h  E(#16) h
	Flow Approaching From 0.531	Flow Approaching From 23.6 0.383 0.46 0.833 19.17 Flow Approaching From 23.6 0.383 0.46 0.833 19.17	2     0.2     0.08     4     0.564     0.015     2     3.44     0.143     0.101     13     0.815     0.821       2     0.23     0.08     4     0.599     0.015     2     3.44     0.143     0.106     10.75     0.744     0.914	Z 0.167     0.08     4     0.456     0.015     Z 3.44     0.143     0.085     17.88     0.448     0.656       2 0.174     0.08     4     0.456     0.015     2     3.44     0.143     0.085     16.53     0.484     0.696	Flow Approaching From	2 Flow Approaching From 27.6 in 288 in 481 in 671	W (ft) W/T Sw (ft/ft) Sw/Sx Eo(#10) In Local Dep. a a S'w =a/(12W) Se (ft/ft) =Sx+SwEo Lt (ft) 15 P Effec L L/Lt d (ft) E (#16) h

Grate inlet from performance curve equation

# STORM WATER INLET COMPUTATIONS

5248 Olde Towne Road, Suite 1 Williamsburg, Virginia 23188 (757) 253-0040 Fax: (757) 220-8994

PROJECT
PROJECT NO.
SUBJECT
SHEET NO.
DATE
BY

Spread Calc's BWS

Remark

No. Lines: 5

Project file: stormsystem#2.stm

## Storm Sewer Tabulation

Page 1

Pro	(J)	4	ω	2	_		Line	Sta
ject Fil	4	N	2	_	End		o <u>T</u>	Station
e: ston	80.0	36.0	97.0	163.0	139.0	(ft)		Len
msyster	0.36	0.44	0.72	0.39	0.73	(ac)	Incr	Drng
Project File: stormsystem#2.stm	0.36	0.80	0.72	1.91	2.64	(ac)	Total	Drng Area
	0.90	0.90	0.90	0.90	0.90	Ĉ		Rnoff
	0.32	0.40	0.65	0.35	0.66		Incr	
	0.32	0.72	0.65	1.72	2.38		Total	Area x C
	5.0	5.0	5.0	5.0	5.0	(min)	Inlet	
	5.0	5.7	5.0	5.8	6.6	(min)	Syst	Tc
	7.0	6.8	7.0	6.8	6.6			Rain
	2.27	4.90	4.53	11.65	15.69	(in/hr) (cfs)		n Total
	5.46	18.17	5.20	5 20.19	21.75	(cfs)		Cap
	1.86	7   4.63	3.69	9 3.71	5 5.00	(ft/s)		Vel
	15	15	햐	24	24	(in)	Size	
	0.51	5.67	0.46	0.57	0.66	(%)	e Slope	Pipe
Z	82.00	81.59	80.00	79.55	78.62	( <del>f</del> )	up Up	_
Number of lines: 5								Invert Elev
lines: 5	81.59	79.55	79.55	78.62	77.70	<b>£</b>	Dn	ev
	83.19	82.48	82.63	81.97	81.23	( <del>†</del>	Пþ	HG
	83.12	82.29	82.29	81.66	80.75	( <del>‡</del> )	Dn	HGL Elev
<u>ي</u>	86.30	88.00	84.50	86.00	89.62		_	Grr
ın Date:						<b>∄</b>	₽ G	Grnd / Rim Elev
Run Date: 12-23-2003	88.00	86.00	86.00	89.62	79.70	( <del>‡</del> )	Dn	Elev
2003	2-5 to 2-6	2-4 to 2-5	2-3 to 2-4	2-2 to 2-3	2-1 to 2-2			Ē.
	2-6	2-5	2-4	2-3	2-2			Line ID
					<del></del> -			

NOTES: Intensity = 140.36 / (Inlet time + 19.80) ^ 0.93; Return period = 10 Yrs.



5248 Olde Towne Road, Suite 1 Williamsburg, Virginia 23188 (757) 253-0040 Fax: (757) 220-8994

toad, Suite 1 ginia 23188 0040 0-8994

PROJECT WINDSORMEADE MARKETPLACE
PROJECT NO. ####
SUBJECT Spread Calc's
SHEET NO. 1
DATE #####
BY BWS

# STORM WATER INLET COMPUTATIONS SHEET NO. 1 BY BY BWS BWS

	-	100	1.5	122	<del>-</del>	_
SS2-4	SS2-6	SS2-5	SS2-3	SS2-2	Number	
DI-28	DI-28	DI-28	DI-2B	DI-28	Туре	NLET
14		œ	8	œ	Length	
					Station	
0.72	0.32	0.44	0.39	0.73	Drainage Area (Ac)	
0.9	0.9	0.9	0.9	0.9	C .	
0.648	0.288	0.396	0.351	0.657	CA	
0.648	0.288	0.396	0.351	0.657	Σ CA	
6.4	6.4	6.4	6.4	6.4	t in/hr	
4.147	1.843	2.534	2.246	4.205	Q-Inter (CFS)	
0.7	0	0	0.951	a	Q Carry- Over (CFS	5)
4.847	1.843	2.534	3.197	4.205	Qt Gutter Flow	
0.01	0.01	0.01	0.01	0.01	S Gutter Slope (ft/ft	)
0.02	0.02	0.02	0.02	0.02	Sx Cross Slope (ft/ft	)
11.1	7.7	8.7	9.3	10.5	T(Spread)	
2	2	2	2	2	W (ft)	
0.18	0.26	0.23	0.215	0.19	W/T	
0.08	0.08	0.08	0.08	0.08	Sw (ft/ft)	
4	4	4	4	4	Sw/Sx	
0.51	0.634	0.599	0.564	0.51	Eo(#10)	
0.015	0.015	0.015	0.015	0.015	n	
2	2	2	2	2	Local Dep	٠.
3.44	3.44	3.44	3.44	3.44	а	
0.143	0.143	0.143	0.143	0.143	S'w =a/(12W)	
0.093	0.111	0.106	0.101	0.093	Se (ft/ft) =Sx+SwE	0
15.1	9.058	10.65	12.09	14.23	Lt (ft) 15 P Effec L	
0.927	0.883	0.751	0.662	0.562	L/Lt (ft)	d
0.991	0.979	0.918	0.858	0.774	E(#16) (ft)	h
4.803	1.805	2.327	2.743	3.254	Q Int CFS d/h	
0.044	0.039	0.207	0.454	0.951	Q Carryov Spread	/er
					Remark	

### **Storm Sewer Tabulation**

Page 1

ыd	_		Line	Sta
oject Fi	End	LIDE	To	Station
le: stori	50.0	€		Len
msyster	1.13	(ac)	Incr	Drng Area
Project File: stormsystem#3.stm	1.13	(ac)	Total	Area
-	0.90	Ĉ	COEII	Rnoff
	1.02		Incr	
	1.02		Total	Area x C
	5.0	(min)	Inlet	
	5.0	(min)	Syst	Tc
	7.0	(in/hr)		Rain
	7.11	(cfs)		Total
	21.18	(cfs)	<u> </u>	Cap
	6.08	(ft/s)		V <sub>el</sub>
	15	(Ē	Size	_
	7.70	(%)	Slope	Pipe
Num	81.55	<b>a</b>	Up	lnv
Number of lines: 1	77.70	(ft)	Dn	Invert Elev
nes: 1				
	82.62	₹	цр	HGL Elev
	80.72	∄	Dn	Elev
Run	89.55	( <del>2</del>	ę	Grnd
Date: 1	78.95	(f	Dn	Grnd / Rim Elev
Run Date: 12-22-2003	35	(₹)	3	lev
03				Line ID
				Ð
-	v * avev			

NOTES: Intensity = 140.36 / (Inlet time + 19.80) ^ 0.93; Return period = 10 Yrs.



### James City County Environmental Division Stormwater Management / BMP Inspection Report Detention and Retention Pond Facilities

SP-150-03

lame of Facility:	n 450 V 11/8	140 11/91/11/	MACE BY	MP No.: 1 of 1 Date: 9/22/16
ocation:				
lame of Owner:				
lame of Inspector:		· .		
ype of Facility:	Wef EX	TEXT	Powo	
Veather Conditions: 🏂	my way	Type: XI	Final Inspection	County BMP Inspection Program
f an inspection item is n		/	•	
Routine - The item cl	hecked requires hecked requires	attention, but does n immediate attention	not present an immed n to keep the BMP op	•
Facility Item	0.K.	Routine	Urgent	Comments
Embankments and Sid	e Slopes:	-arthly n	n, 8-20 m	ide; 24:1V
Grass Height				Very LIH/+ 91035
Vegetation Condition				Bare Soil on down
Tree Growth				None, Landscoping pre
Erosion	V/			Surface erusion
Trash & Debris				,
Seepage				Locksok.
E : D 1				
Fencing or Benches	Dlantad Amana	None Cons	tructed Wetland/Shallo	ow Marsh
<del></del>	rianteu Areas:	/		<u>,</u>
<del></del>	Tainted Areas:			
Interior Landscaping/l	Areas:			Needs stabilized.
Interior Landscaping/I Vegetated Conditions Trash & Debris	A laneu Areas:			Needs stabilized.
Interior Landscaping/l Vegetated Conditions Trash & Debris	A laneu Areas:			Needs stabilized.
Interior Landscaping/I Vegetated Conditions Trash & Debris Floating Material	A laneu Areas:			Needs stabilized.
Interior Landscaping/I Vegetated Conditions Trash & Debris Floating Material Erosion	A least			
Interior Landscaping/I Vegetated Conditions Trash & Debris Floating Material Erosion Sediment	A laneu Areas:			Looks of Coese

Facility Item	0.K.	Routine	Urgent	Comments
Water Pools:	rmanent Poo	(Retention Basin) S	hallow Marsh (De	etention Basin)
Shoreline Erosion				
Algae				Some
Trash & Debris		$\sim$		Remove frash in NW CAIM
Sediment				;
Aesthetics				
Other			1 4 1	"
Inflows (Describe Types	/Locations)	1)ABI CPP WES	F, 2/36	5W Corner #3) SMALL 121
Condition of Structure	1		,	
Erosion	V			,
Trash and Debris	,			Clean aftall Pipe #2
Sediment			V	From veg obstruction.
Outlet Protection	1/			
Other				
Principal Flow Control	Structure -	Riser, Intake, etc. (Descr	ibe Type):	48' RCP W/ CMP CAP; 36" outrall
Condition of Structure				NAPO
Corrosion				locah
Trash and Debris			V	Clean debris/around riser
Sediment				(FD.
Vegetation				,
Other	<i>V</i>			LIEAN CONTION, BAHON
Principal Outlet Structu	ra - Rarral	, Conduit, etc. : 36	RCP, E	S-/
Condition of Structure	- Barrer	Conduit, etc.: 36	KCP, C	.3-/
Settlement	V			Character // house of 16
Trash & Debris			1./	Clean outto// of veg, rock + de
Erosion/Sediment	· · · · ·			Kemine (atai)
Outlet Protection		- 12		12×25 classI, foreboy 1
Other	<u> </u>		1	1 2/ 100.4
Emergency Spillway (O	verflow):	Concrete, 10	W Z:1	; z'deep
Vegetation	- V			
Lining	\ <u>\</u>	-		Concrete
Erosion	V			
Trash & Debris	<u> </u>			
Other				Fence obstructs E.S.

Facility Item	O.K.	Routine	Urgent	Comments
Nuisance Type Condition	ons:			
Mosquito Breeding				
Animal Burrows				
Graffiti				
Other			• • • •	1
Surrounding Perimeter	Conditions:	Fence q	NorthWoo	13, South BUDG, EAST, WEST
Land Uses	V			
Vegetation		·		
Trash & Debris		<b>V</b>		BAGS of concrete sw corner.
Aesthetics				
Access /Maintenance Roads or Paths				Access Road incomplete GNIOP RAI/ MISSINS
Other			V	Gude KAI
Overall Environmental	locks of conerct	(Z	fer fence from infry	(Luopan/5) H1-2
Signature:	AK J	Umun Engmeer		Date: 9 77/00

SWMProg\BMP\CoInspProg\InspForms\DetRet.wpd

Reinspected 11-5-07 Jason Beek Okay

### **Scott Thomas**

From: Scott Thomas

Sent: Wednesday, October 11, 2006 5:24 PM

To: 'rhett@ashlandconstruction.com'

Cc: 'Arch Marston'; 'MGalli'; Joan Etchberger

Subject: Wet Pond BMP at WindsorMeade Marketplace

Rhett – As you a fighting a bond renewal deadline, I am emailing you this correspondence by email rather than my usual method by letterhead through the mail.

Date: October 11, 2006

To: Mr. Rhett Moody

Ashland Construction

Re: WindsorMeade Marketplace

County Plan No. SP-150-03 (Amends SP-2-05)

County BMP ID Code: PC 203

### Dear Moody:

The Environmental Divisions has received a record drawing (asbuilt) and construction certification for the stormwater management facility for the above referenced project. The record drawing provides as-built information for a wet extended detention pond in the back, northwest corner of the site. Based on our review of the project and a concurrent field inspection as performed on September 22, 2006 the following items must be addressed prior to release of the developer's surety instrument for the stormwater management/BMP facility at the site and to proceed with closing out the project:

### **Record Drawing:**

1. The record drawing set dated March 1, 2006 is **satisfactory**. Please forward one additional blue/black line and one reproducible of the record drawing set to our office.

### **Construction Certification:**

2. The construction certification dated May 3, 2006 is satisfactory.

### Construction - Related Items:

- 3. Stabilize all bare soil and erosion areas present on the dam and within the interior graded sideslopes. Most of the top of dam and downstream embankment and the south interior graded pond slope were not in an acceptable stabilized condition.
- 4. Clean and remove all debris, trash and minor sediments from around the low flow orifice pipe on the principal spillway device. This would be at the end of the 6-inch pipe which extends out from the riser.
- 5. Remove trash and debris in the northwest corner of the basin, approximately 50 ft. west of the basin.
- 6. Clean and remove sediment accumulations, debris, trash and vegetation within 10 feet of the outfall end of the 36-inch storm drain pipe which enters the basin at the southeast corner. This is the pipe between storm drainage structure SS # 2-2 and SS # 2-1 on the approved plan. Flow into the basin shall not be obstructed by debris, trash, sediment or vegetation.

- 7. Clean and remove all debris and obstruction at the outfall of the 36-inch barrel through the dam, especially obstructions within the flared end section.
- 8. The chain link fence around the perimeter of the facility is across and blocking the concrete emergency spillway. During high flow conditions, the fence will tend to trap debris which could raise the water surface elevation of the pond above that intended which could result in overtopping. Based on design information, depth of flow in the emergency spillway for the 100-year event would be at least 0.70 feet deep in the spillway; therefore, the fence should be cut about 1 foot.
- 9. Clean and remove debris (unused bags of concrete) in the southwest corner of the site.
- 10. The access road for BMP maintenance, as proposed in the southwest corner of the site, is incomplete and not installed per the approved design plan.
- 11. Guard rail, as proposed along the back service road between the road and the BMP area, was not installed per the approved plan.
- 12. The principal spillway device (riser) had no entry, access hatch or lid. It is impossible to inspect or maintain the riser without proper access.
- 13. To prevent unauthorized access, padlocks should be added to the two gate structures on the perimeter fence around the BMP area. Provide an extra set of keys or combination for the locks to the Environmental Division office.

Once this work is satisfactorily completed, contact our office appropriately for a re-inspection. We can then proceed with final release of the surety and/or closing out the project. Please contact me at 757-253-6639 or the assigned Environmental Division inspector, Mr. Jason Beck 757-259-4026 if you have any further comments or questions.

Scott J. Thomas, P.E. Chief Engineer - Stormwater James City County Environmental Division

cc: Arch Marson - via email
Mike Galli - via email

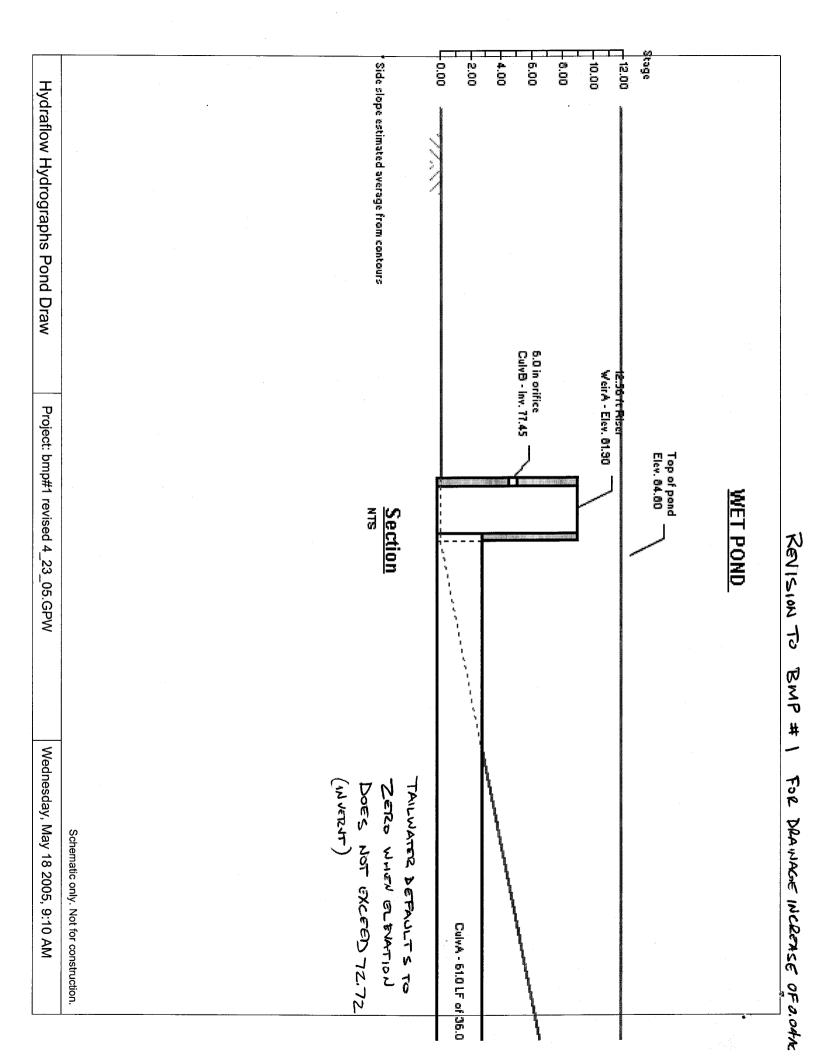


### James City County Environmental Division Stormwater Management/BMP Record Drawing & Construction Certification Review Tracking Form

10/ 1 - 0/
Project Name: WINDSUR N/64DE N/ARKETPUN CE
County Plan No.: 5P-150-03 (AMEND 5P-2-05)
Stormwater Management Facility: WET EXT DET POWO
BMP Phase #: DI DII TAIII  ** Information Package Received, Date/By: JVLY 21 700 AES
2 Intermediation / desired Notes Color Co. Detectory 1
Completeness Check:  Pecord Drawing  Date/By:
Record Drawing Date/by.
Construction Certification Date/By: <u>EC\$ 5/3/0U</u>
RD/CC Standard Forms (Required for all BMPs after Feb 1st 2001Only) Insp/Maint Agreement # / Date: # 040021396 Avg 23 Zov 4
BMP Maintenance Plan Location: Sincet 14 Record Mawing  Other:
Standard E&SC Note on Approved Plan Requiring RD/CC or County comment in plan review
Yes No Location: 5 heet 12
Assign County BMP ID Code #: Code: PC Z 0 3
Preliminary Input/Log into Division's "As-Built Tracking Log"
Add Location to GIS Map. Obtain basic site information (GPIN, Owner, Address, etc.)
Preliminary Log into Access Database (BMP ID #, Plan No., GPIN, Project Name, etc.)
Active Project File Review (correspondence, H&H, design computations, etc.).
1 Initial As-Built File setup (File label, folder, copy plan/details/design information, etc.).
inspector Check of RD/CC (forward to Inspector using transmittal for cursory review).
Pre-Inspection Drawing Review of Approved Plan (Quick look prior to Field Inspection).
K Final Inspection (FI) Performed Date: 912 06
K Record Drawing (RD) Review Date: 91206
Construction Certification (CC) Review Date: <u>1/2 2 (itc</u>
Actions:
□ No comments.
Comments. Letter Forwarded. Date:
Record Drawing (RD)
<ul> <li>Construction Certification (CC)</li> </ul>
Construction-Related (CR)
□ Site Issues (SI)
Dother:
Second Submission: Na
Reinspection (if necessary):
Acceptable for SWM Purposes (RD/CC/CR/Other). Ok to proceed with bond release.
Complete "Surety Request Form".
Check/Clean active file of any remaining material and finish "As-Built" file.
Add to County BMP Inventory/Inspection schedule (Phase I, II or III).
Copy Final Inspection Report into County BMP Inspection Program file.
Obtain Digital Photographs of BMP and save into County BMP Inventory.
Request mylar/reproducible from As-Built plan preparer.
Complete "As-built Tracking Log".
Last check of BMP Access Database (County BMP Inventory).
Add BMP to JCC Hydrology & Hydraulic database (optional).
Add BMP to Municipal BMP list (if a County owned facility)
Add BMP to PRIDE BMP ratings database. problem with program
Final Sign-Off

Plan Reviewer: Date: 11,7/07

\*\*\* See separate checklist, if needed.



### **Pond Report**

Hydraflow Hydrographs by Intelisolve

Wednesday, May 18 2005, 9:17 AM

### Pond No. 2 - WET POND

**Pond Data** 

Pond storage is based on known contour areas. Average end area method used.

### Stage / Storage Table

Stage (ft) Elevation (ft)		Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	73.00	6,701	0	0
1.00	74.00	12,612	9,657	9,657
2.00	75.00	13,689	13,151	22,807
3.00	76.00	14,799	14,244	37,051
4.00	77.00	15,942	15,371	52,422
5.00	78.00	22,057	19,000	71,421
6.00	79.00	27,489	24,773	96,194
7.00	80.00	29,673	28,581	124,775
8.00	81.00	31,917	30,795	155,570
9.00	82.00	34,224	33,071	188,641
10.00	83.00	36,580	35,402	224,043
11.00	84.00	38,898	37,739	261,782
11.80	84.80	40,842	31,896	293,678

Cul	vert /	Orifice	Struct	ures

W	<i>l</i> eir	Stri	uctu	res

	[A]	[B]	[C]	[D]		[A]	[B]	[C]	[D]
		L- J	F-1	1-1		2-3	L-J	r-1	r-1
Rise (in)	= 36.00	6.00	0.00	0.00	Crest Len (ft)	= 12.56	10.00	0.00	0.00
Span (in)	= 36.00	6.00	0.00	0.00	Crest El. (ft)	= 81.90	82.90	0.00	0.00
No. Barrels	= 1	1	0	0	Weir Coeff.	= 3.33	3.33	0.00	0.00
Invert El. (ft)	= 72.72	77.45	0.00	0.00	Weir Type	= Riser	Ciplti		
Length (ft)	= 61.00	0.00	0.00	0.00	Multi-Stage	= Yes	No	No	No
Slope (%)	= 1.18	0.00	0.00	0.00					
N-Value	= .013	.013	.000	.000					
Orif. Coeff.	= 0.60	0.60	0.00	0.00					
Multi-Stage	= n/a	Yes	No	No	Exfiltration = 0	0.000 in/hr (Co	ntour) Tai	lwater Ele	ev. = 0.00 ft

Note: Culvert/Orifice outflows have been analyzed under inlet and outlet control.

Stage /	/ Storage /	Discharge	Table
---------	-------------	-----------	-------

Stage ft	Storage cuft	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	Clv D cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Total cfs
	ouit	••	013	013	013	013	UIS	CIS	CIS	CIŞ	013	CIS
0.00	0	73.00	0.00	0.00			0.00	0.00				0.00
1.00	9,657	74.00	0.62	0.00			0.00	0.00				0.00
2.00	22,807	75.00	0.62	0.00			0.00	0.00				0.00
3.00	37,051	76.00	0.62	0.00			0.00	0.00				0.00
4.00	52,422	77.00	0.62	0.00			0.00	0.00				0.00
5.00	71,421	78.00	0.62	0.52			0.00	0.00				0.52
6.00	96,194	79.00	1.13	1.08			0.00	0.00				1.08
7.00	124,775	80.00	1.43	1.43			0.00	0.00				1.43
8.00	155,570	81.00	1.76	1.72			0.00	0.00				1.72
9.00	188,641	82.00	3.30	1.96			1.32	0.00				3.28
10.00	224,043	83.00	50.43	2.18			48.25	1.05				51.48
11.00	261,782	84.00	101.65	0.88			100.77	38.42				140.07
11.80	293,678	84.80	108.73	0.58			108.15	87.21				195.93

### **Hydrograph Return Period Recap**

Proj. file: bmp#1 revised 4\_23\_05.GPW

	Inflow Hyd(s)	}			Hydrograph					
No. type (origin)		1-Yr	2-Yr	3-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr	description
SCS Runoff		7.11	12.21			31.96	37.56		52.98	PRE-DEVELOPMENt
SCS Runoff		43.73	57.82			103.74	115.60		147.05	9069POST-DEVELOPMENT
Reservoir	2	1.75	3.81			62.45	80.42		121.09	wet pond
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									-	
	:									
	(origin) SCS Runoff SCS Runoff	(origin)  SCS Runoff SCS Runoff Reservoir 2	(origin)         1-Yr           SCS Runoff          7.11           SCS Runoff          43.73           Reservoir         2         1.75	(origin)         1-Yr         2-Yr           SCS Runoff          7.11         12.21           SCS Runoff          43.73         57.82           Reservoir         2         1.75         3.81	(origin)         1-Yr         2-Yr         3-Yr           SCS Runoff         7.11         12.21            SCS Runoff         43.73         57.82            Reservoir         2         1.75         3.81	(origin)         1-Yr         2-Yr         3-Yr         5-Yr           SCS Runoff	(origin)         1-Yr         2-Yr         3-Yr         5-Yr         10-Yr           SCS Runoff          7.11         12.21          31.96           SCS Runoff          43.73         57.82          103.74           Reservoir         2         1.75         3.81          62.45	(origin)         1-Yr         2-Yr         3-Yr         5-Yr         10-Yr         25-Yr           SCS Runoff          7.11         12.21          31.96         37.56           SCS Runoff          43.73         57.82          103.74         115.60           Reservoir         2         1.75         3.81          62.45         80.42	Corigin   1-Yr   2-Yr   3-Yr   5-Yr   10-Yr   25-Yr   50-Yr	(origin)         1-Vr         2-Vr         3-Vr         5-Vr         10-Vr         25-Yr         50-Vr         100-Vr           SCS Runoff          7.11         12.21           31.96         37.56          52.98           SCS Runoff          43.73         57.82           103.74         115.60          147.05           Reservoir         2         1.75         3.81          62.45         80.42          121.09

Hydraflow Hydrographs by Intelisolve

Wednesday, May 18 2005, 9:08 AM

# **Hydrograph Summary Report**

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Maximum storage (cuft)	Hydrograph description
1	SCS Runoff	7.11	2	736	36,768				PRE-DEVELOPMENt
2	SCS Runoff	43.73	2	726	152,637				9069POST-DEVELOPMENT
5	Reservoir	1.75	2	902	151,398	2	81.12	159,576	wet pond
						·	PREVIOUSLY		
							81.11		
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L					L			<u> </u>	Hydraflow Hydrographs by Intelisoly

Hydraflow Hydrographs by Intelisolve

Wednesday, May 18 2005, 9:32 AM

# Hyd. No. 2

### 9069POST-DEVELOPMENT

Hydrograph type = SCS Runoff

Storm frequency = 1 yrs

Drainage area = 20.94 ac

Basin Slope = 2.0 % Tc method = USER

Total precip. = 2.80 in Storm duration = 24 hrs Peak discharge = 43.73 cfs

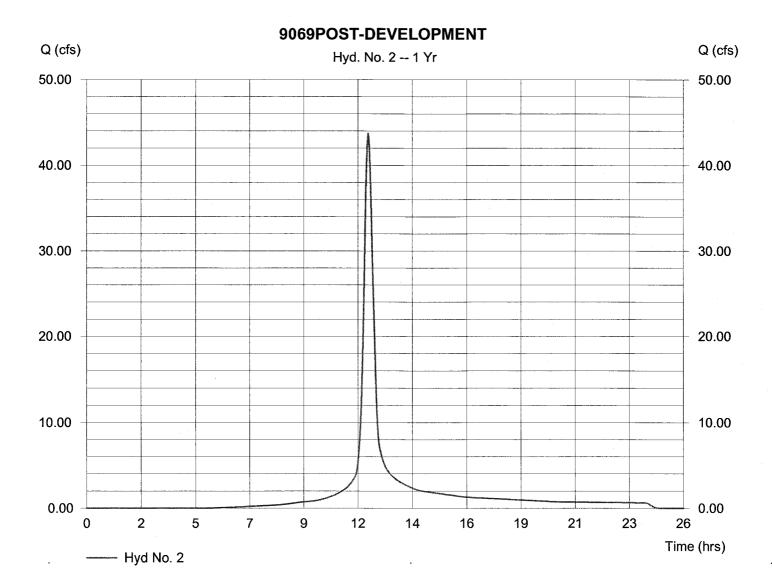
Time interval = 2 min

Curve number = 92 Hydraulic length = 3000 ft

Time of conc. (Tc) = 21 min

Distribution = Type II Shape factor = 484

Hydrograph Volume = 152,637 cuft



PREVIOUSLY 22,9

Hydraflow Hydrographs by Intelisolve

Wednesday, May 18 2005, 9:28 AM

## Hyd. No. 5

wet pond

Hydrograph type = Reservoir Storm frequency = 1 yrs

Inflow hyd. No. =

Reservoir name

= 2

= WET POND

Peak discharge

= 1.75 cfs

Time interval

= 2 min

Max. Elevation

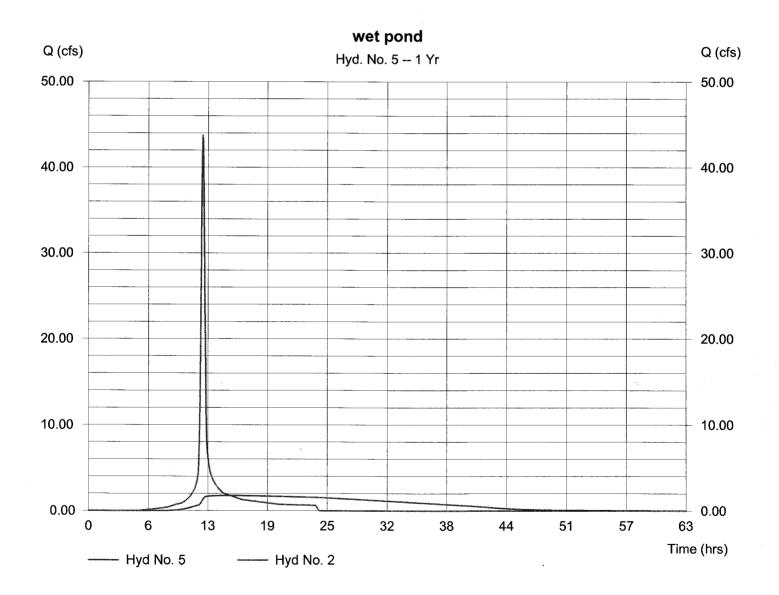
= 81.12 ft

Max. Storage

= 159,576 cuft

Storage Indication method used. Wet pond routing start elevation = 77.40 ft.

Hydrograph Volume = 151,398 cuft



# **Hydrograph Summary Report**

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Maximum storage (cuft)	Hydrograph description
1	SCS Runoff	12.21	2	736	58,844				PRE-DEVELOPMENt
2	SCS Runoff	57.82	2	726	204,004		<del></del>		9069POST-DEVELOPMENT
5	Reservoir	3.81	2	812	202,670	2	82.02	189,404	wet pond
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Hydraflow Hydrographs by Intelisolve

Wednesday, May 18 2005, 9:32 AM

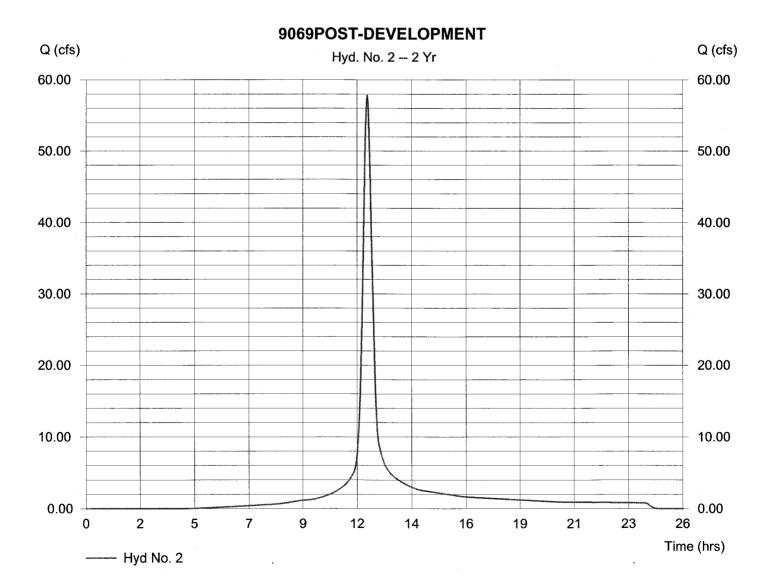
# Hyd. No. 2

## 9069POST-DEVELOPMENT

Hydrograph type = SCS Runoff
Storm frequency = 2 yrs
Drainage area = 20.94 ac
Basin Slope = 2.0 %
Tc method = USER
Total precip. = 3.50 in
Storm duration = 24 hrs

Peak discharge = 57.82 cfs
Time interval = 2 min
Curve number = 92
Hydraulic length = 3000 ft
Time of conc. (Tc) = 21 min
Distribution = Type II
Shape factor = 484

Hydrograph Volume = 204,004 cuft



Hydraflow Hydrographs by Intelisolve

Wednesday, May 18 2005, 9:28 AM

# Hyd. No. 5

wet pond

Hydrograph type = Reservoir

Storm frequency = 2 yrs

Inflow hyd. No.

= 2

Reservoir name = WET POND Peak discharge

= 3.81 cfs

Time interval

= 2 min

Max. Elevation

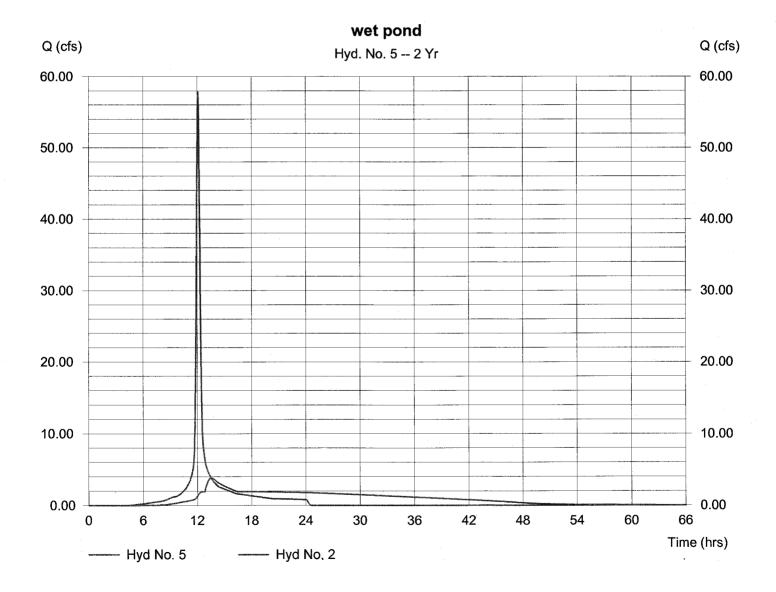
= 82.02 ft

Max. Storage

= 189,404 cuft

Storage Indication method used. Wet pond routing start elevation = 77.40 ft.

Hydrograph Volume = 202,670 cuft



# **Hydrograph Summary Report**

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Maximum storage (cuft)	Hydrograph description
1	SCS Runoff	31.96	2	736	145,833	<del></del>			PRE-DEVELOPMENt
2	SCS Runoff	103.74	2	726	377,016				9069POST-DEVELOPMENT
5	Reservoir	62.45	2	738	375,631	2	83.12 No CHARGÉ	228,727	wet pond
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			05.05		<b>.</b>		2.14		
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Hydraflow Hydrographs by Intelisolve

Wednesday, May 18 2005, 9:32 AM

# Hyd. No. 2

Storm duration

# 9069POST-DEVELOPMENT

Hydrograph type = SCS Runoff
Storm frequency = 10 yrs
Drainage area = 20.94 ac
Basin Slope = 2.0 %
Tc method = USER
Total precip. = 5.80 in

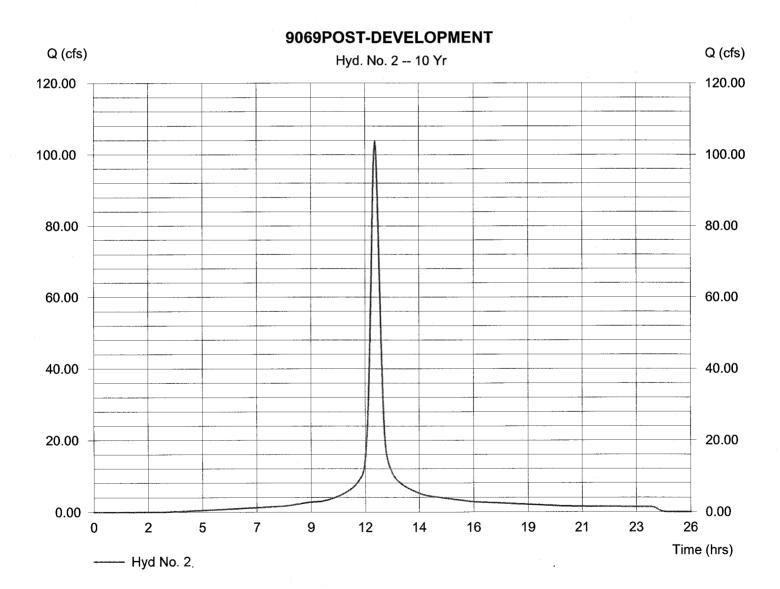
= 24 hrs

Peak discharge = 103.74 cfs
Time interval = 2 min
Curve number = 92
Hydraulic length = 3000 ft
Time of conc. (Tc) = 21 min
Distribution = Type II

Shape factor

Hydrograph Volume = 377,016 cuft

= 484



Hydraflow Hydrographs by Intelisolve

Wednesday, May 18 2005, 9:28 AM

# Hyd. No. 5

wet pond

Hydrograph type = Reservoir Storm frequency = 10 yrs

Inflow hyd. No.

= WET POND Reservoir name

= 2

Peak discharge

= 62.45 cfs

Time interval

= 2 min

Max. Elevation

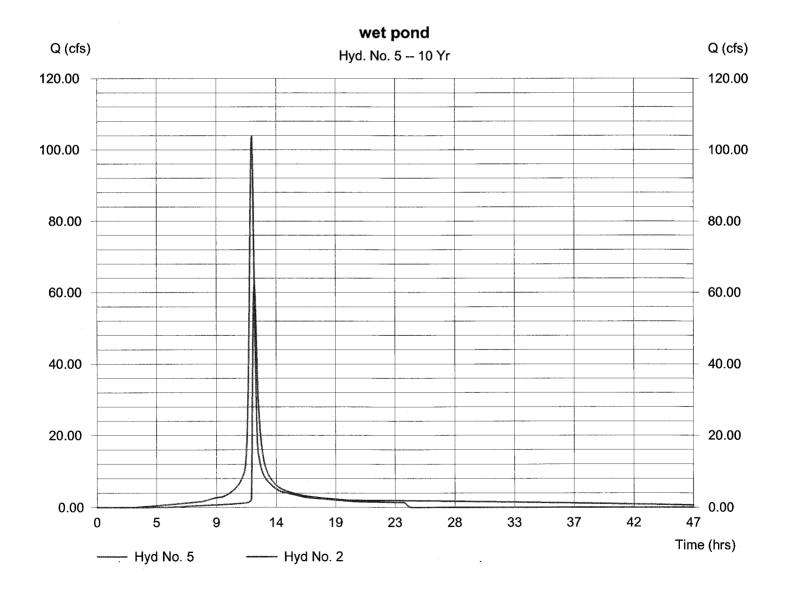
 $= 83.12 \, ft$ 

Max. Storage

= 228,727 cuft

Storage Indication method used. Wet pond routing start elevation = 77.40 ft.

Hydrograph Volume = 375,631 cuft



# **Hydrograph Summary Report**

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Maximum storage (cuft)	Hydrograph description
1	SCS Runoff	37.56	2	734	170,769				PRE-DEVELOPMENt
2	SCS Runoff	115.60	2	726	422,677			<del></del> .	9069POST-DEVELOPMENT
5	Reservoir	80.42	2	736	421,283	2	83.31	235,601	wet pond
							PRNIOUSLY 83.3°		-
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Hydraflow Hydrographs by Intelisolve

Wednesday, May 18 2005, 9:32 AM

# Hyd. No. 2

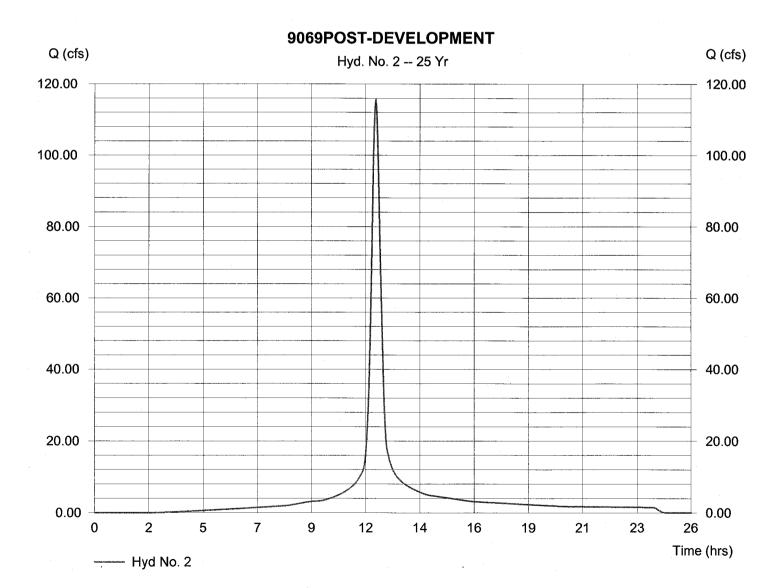
### 9069POST-DEVELOPMENT

Hydrograph type = SCS Runoff
Storm frequency = 25 yrs
Drainage area = 20.94 ac
Basin Slope = 2.0 %
Tc method = USER
Total precip. = 6.40 in
Storm duration = 24 hrs

Peak discharge = 115.60 cfs
Time interval = 2 min
Curve number = 92
Hydraulic length = 3000 ft
Time of conc. (Tc) = 21 min

Distribution = Type II Shape factor = 484

Hydrograph Volume = 422,677 cuft



Hydraflow Hydrographs by Intelisolve

Wednesday, May 18 2005, 9:28 AM

# Hyd. No. 5

wet pond

Hydrograph type = Reservoir Storm frequency = 25 yrs

Inflow hyd. No.

= 2

Reservoir name = WET POND

Peak discharge

= 80.42 cfs

Time interval

= 2 min

Max. Elevation

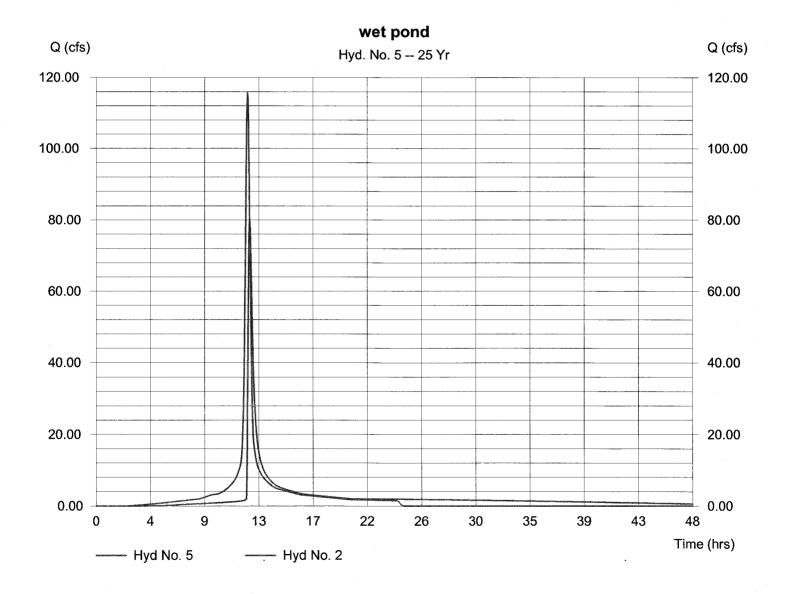
 $= 83.31 \, \text{ft}$ 

Max. Storage

= 235,601 cuft

Storage Indication method used. Wet pond routing start elevation = 77.40 ft.

Hydrograph Volume = 421,283 cuft



# **Hydrograph Summary Report**

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Maximum storage (cuft)	Hydrograph description
1	SCS Runoff	52.98	2	734	239,937				PRE-DEVELOPMENt
2	SCS Runoff	147.05	2	726	544,951				9069POST-DEVELOPMENT
5	Reservoir	121.09	2	732	543,542	2	83.70	250,592	wet pond
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Hydraflow Hydrographs by Intelisolve

Wednesday, May 18 2005, 9:32 AM

# Hyd. No. 2

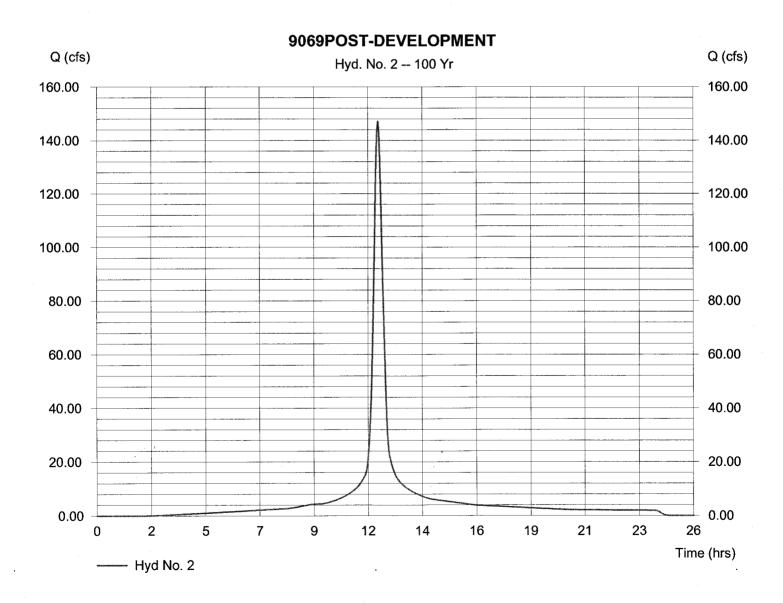
# 9069POST-DEVELOPMENT

Hydrograph type = SCS Runoff
Storm frequency = 100 yrs
Drainage area = 20.94 ac
Basin Slope = 2.0 %
Tc method = USER
Total precip. = 8.00 in
Storm duration = 24 hrs

Peak discharge = 147.05 cfs
Time interval = 2 min
Curve number = 92
Hydraulic length = 3000 ft
Time of conc. (Tc) = 21 min

Distribution = Type II Shape factor = 484

Hydrograph Volume = 544,951 cuft



Hydraflow Hydrographs by Intelisolve

Wednesday, May 18 2005, 9:28 AM

# Hyd. No. 5

wet pond

Hydrograph type = Reservoir Storm frequency = 100 yrs

Inflow hyd. No.

= 2

Reservoir name = WET POND

Peak discharge

= 121.09 cfs

Time interval

= 2 min

Max. Elevation

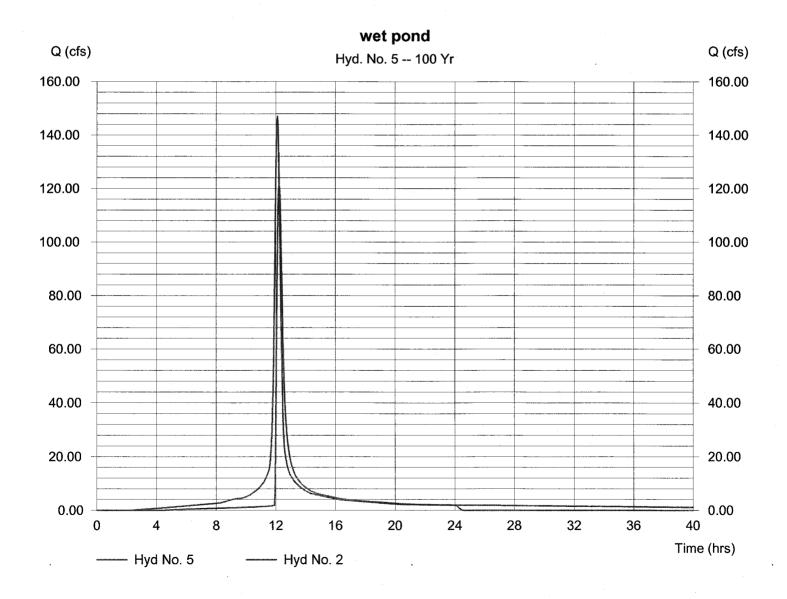
= 83.70 ft

Max. Storage

= 250,592 cuft

Storage Indication method used. Wet pond routing start elevation = 77.40 ft.

Hydrograph Volume = 543,542 cuft



## **TRANSMITTAL**

DATE:

September 16, 2004

TO:

**Environmental** 

JCSA (2)

FROM:

Christopher Johnson, Senior Planner

SUBJECT:

SP-150-03. WindsorMeade Marketplace

ITEMS ATTACHED:

**Revised Site Plans** 

**Engineering Calculations & Computations** 

**INSTRUCTIONS:** 

Please review and comment.

**RETURN BY:** 

October 1, 2004

**AGENCY COMMENTS:** 

RECEIVED SET 3 9 2004

RECEIVED

SEP 2 2004

ENVIRONMENTAL DIVISION

DUE OCT 11

Approved 10/4/04 DEC

Is this development served by Newport News Waterworks? \_\_\_\_(JCSA please check if yes)

If checked, planner will fax a copy of preliminary approval letter with Fire Department comments, and the JCSA completed water data sheet to Newport News Waterworks as soon as all three are available.

## TRANSMITTAL

DATE:

July 21, 2004

TO:

**Environmental** 

JCSA (2) VDOT

FROM:

Christopher Johnson, Senior Planner

SUBJECT:

SP-150-03. WindsorMeade Marketplace

ITEMS ATTACHED:

**Revised Site Plans** 

Water Distribution System Analysis (JCSA) Water & Sanitary Sewer Data Sheets (JCSA)

**INSTRUCTIONS:** 

Please review and comment.

**RETURN BY:** 

August 4, 2004

**AGENCY COMMENTS:** 

RECEIVED IN 26 2004

Approved. Specific vecommendations for BMP construction as ovtlined in the geotechnical report by ECS Ltd. (7/20/04; 07:6958) need to be considered during construction of the wet pond BMP.

Ant Them for DEC

Is this development served by Newport News Waterworks? \_\_\_\_(JCSA please check if yes)

If checked, planner will fax a copy of preliminary approval letter with Fire Department comments, and the JCSA completed water data sheet to Newport News Waterworks as soon as all three are available.



# Windsormeade Marketplace James City County Environmental

September 13, 2004

2 COPIES OF COMPUTATIONS

SP-150-03 FIWAL WAM ISSION

Prepared by:



**AES Consulting Engineers** 5248 Olde Towne Road. Suite 1 Williamsburg, VA 23188 (757) 253-0040 Fax: (757) 220-8994

## 5248 Olde Towne Road • Suite 1 Williamsburg, VA 23188 (757) 253-0040 • Fax (757) 220-8994



614 Moorefield Park Drive Richmond, VA 23236 (804) 330-8040 • Fax (804) 330-9840

September 13, 2004

Mr. Christopher Johnson Senior Planner James City County 101-E Mounts Bay Road Williamsburg, Virginia 23187-8784

RE: Case No. SP-150-03. Windsor Meade Marketplace AES Job No. 9069-02

Dear Mr. Johnson:

This letter is a response to the requested changes or revisions to the above referenced site plans. Changes or revisions were made to these documents to address the items provided in your letter of August 9, 2004. We are very hopeful this re-submittal will satisfy your comments and lead to a final approval.

### Planning:

1. Revised landscaping plans have not been submitted for review. Staff is aware that the landscape plans are being prepared by Higgins & Gerstenmaier.

It is our understanding that the landscape drawings have been submitted under separate cover by Higgins and Gerstenmaier.

### JCSA:

James City Service Authority has reviewed these plans for general compliance with the JCSA Standards and Specifications, Water Distribution and Sanitary Sewer Systems and have the following comments. Quality control and back checking of the plans and calculations for discrepancies, errors, omissions, and conflicts is the sole responsibility of the professional engineer and/or surveyor who has signed, sealed, and dated the plans and calculations. It is the responsibility of the engineer or surveyor to ensure the plans and calculations comply with all governing regulations, standards, and specifications. Before the JCSA can approve these plans for general compliance with the JCSA Standards and Specifications, the following comments must be addressed. We may have additional

comments when a revised plan incorporating these comments is submitted.

### General Comments:

1. The Applicant shall provide landscape drawings which address JCSA comments previously issued on May 6, 2004.

It is our understanding that the landscape drawings have been submitted under separate cover by Higgins and Gerstenmaier.

2. Per previous comment and prior to JCSA acceptance of the utilities, the Owner/Developer shall provide a formal instrument which emulates the Urban Easement requirement established for other phases of the New Town development.

This has been provided to JCSA (Larry Foster) by the developer on July 9, 2004. A copy of this submitted agreement is included in your package.

3. Calculations substantiating proposed meter sizes were not provided with the site plan submittal. As previously requested, the Applicant shall provide water demand calculations for verification that the proposed water meters are adequately sized. Calculations shall be provided for each "unit" of buildings and be based on the International Plumbing Code. If data is not available at this time in relation to the type of tenant and fixtures required, then the Applicant shall show and label the meter locations as future (w/o size annotated). A stub/valve can be provided at the location for future installation.

This information is now provided with this submittal package.

### Sheet 6:

1. The Applicant shall either indicate the check valve type required at the fire service connection or remove the note referencing JCSA. This is part of the proposed private fire supply line and the responsibility of the Owner/Developer. JCSA=s responsibility terminates with the detector check valve assembly proposed prior to the fire supply pump. Revise call-out accordingly.

Per our conversation of August 19, 2004, the note referring JCSA at the fire service connection has been removed.

Case No. SP-150-03. Windsor Meade Marketplace September 13, 2004 Page 3

### Sheet 13:

- 1. WL "A" Profile:
  - A. Sta 16+10 (+/-): The graphical location of the 10" HDPE pipe contradicts design data provided on Sheet 9. It appears that the proposed storm sewer will actually conflict with the proposed 12" waterline. Verify and revise accordingly. A minimum vertical clearance of 18-inches shall be provided between the waterline and the storm sewer crossing.

The HDPE pipe inverts have been modified. There is no conflict with the proposed 12" waterline. A minimum cover of 18" was maintained at the crossing of the HDPE pipe and the waterline.

- 2. Ex San MH #7 to San MH #3:
  - A. Sta 16+10 (+/-): The graphical location of the 10" HDPE pipe contradicts design data provided on Sheet 9. A minimum vertical clearance of 18-inches shall be provided between the sanitary sewer and the storm sewer crossing.

The HDPE pipe inverts have been modified. A minimum cover of 18" was maintained at the crossing of the HDPE pipe and the gravity sewer line.

### Sheet 15:

1. WL "B" & "C" Profiles: Pipe material from the tee to the hydrant shall be DIP. Revise plan and profile accordingly.

Waterlines "B" and "C" servicing the fire hydrants have now been modified to be ductile iron pipe. The water data sheets have also been modified to reflect this revision.

### Water Data Sheet:

1. Section 5b: The Applicant shall revise the line item to provide the "Average Day Domestic Demand" in gpm for the development (refer to JCSA standards Section 2.9A). Reference to any fire flows or pressures should not be included as part of this line item. Verify and revise accordingly.

The average day domestic demand in section 5b represents the total from the water meter sizing calculations divided by 4 and multiplied by 1.7. This should give you the "Average Day Domestic Demand."

Case No. SP-150-03. Windsor Meade Marketplace September 13, 2004 Page 4

- 2. Section 6:
  - 1. Verify where the 8-inch PVC pipeline is used on this project. If not, remove from tabulation block.

This 8" PVC is no longer used for the waterline. This has been removed from the tabulation block.

2. Revise callout for "6" fire line to DDC vault" to read "8" fire line to Detector Check Valve".

This callout now reads "8" fire line to Detector Check Valve" to coincide with the plan.

3. Per previous comment, fire hydrant pipe material shall be DIP.

The service lines "B" and "C" are now all ductile iron.

3. Section 7: Refer to General Comments Note 3 above concerning meter sizing. The Water Data Sheet references four 1-inch meters when five are shown on the plan. Verify and revise accordingly.

The water data sheet has been revised to accurately reflect the water meters depicted on the plans.

### Sanitary Sewer Data Sheet:

1. Section 6: The 8" PVC pipe length listed does not correspond with profiled information on the plan (appears to be 1116 lf). Verify and revise accordingly.

The 866 lf of 8" PVC listed in section 6 is correct. Per previous comment, we had removed the 250 lf of PVC pipe designated as "private" from the sanitary sewer data sheet.

Water Distribution Hydraulic Analysis:

1. Provide a professional engineer's seal, signed and dated, on the cover of the hydraulic analysis report.

The hydraulic analysis has been sealed and signed.

Case No. SP-150-03. Windsor Meade Marketplace September 13, 2004 Page 5

- 2. Nodal Demand Summary Table:
  - A. Fire Flow + Max Day + Irrigation column Flows listed for nodes J-2, J-4M and J-8M appear to be incorrect as they do not include the proposed irrigation flows. Verify and revise accordingly.

The hydraulic analysis nodal summary table has been updated.

3. It appears the flows associated with Node J-4M was omitted from each scenario analysis. Verify and revise accordingly.

The hydraulic analysis has been updated so that node J-4M has the correct flows associated with the node.

### Environmental:

Base upon resubmitted plans and computations, all comments relating to the site erosion and sediment control plan and major issues associated with the site stormwater management plan have been adequately addressed; therefore, the plan is approved for land-disturbing permit purposes. The following two comments, which pertain to final site plan approval for the project, are still outstanding. Final site plan approval for the project cannot be granted by our Division until the following two issues are resolved.

1. Geotechnical. Previous comment #11 was not addressed. Response indicates that a geotechnical report is forthcoming to show that existing soils beneath the wet pond are adequate to sustain a permanent pool as intended for a County type A-3 BMP. Final site plan approval cannot be issued by our Division until it is determined the BMP will function as a wet pond per the BMP point calculation (County type A-3 BMP).

The geotechnical report has been submitted. Per your discussion with Arch Marston it was determined that no liner would be required for this BMP.

2. Landscaping. Previous comment #12 was not addressed. Response indicates that the landscaping comment will be addressed on forthcoming landscape plans. The landscaping plan must show pond perimeter and bench landscaping and plantings, consistent with the requirements of the County BMP manual and Minimum Standard & Spec. 3.05 of the Virginia Stormwater Management Handbook and to remain consistent with the approved pond bench waiver request.

It is our understanding that the landscape drawings have been submitted under separate cover by Higgins and Gerstenmaier.

3. Per telephone message you requested a modification to the emergency spillway and design calculations in relationship to the 100 yr storm event.

The emergency spillway has been modified per your request and the design information has been provided per your request.

Please note we have made minor changes to storm sewer system #1 and storm sewer system #3 for ease of construction. New computations have been provided for the changes. The revisions to these systems are listed below:

### Sheet 8

- SS#1-13 was changed from a manhole to a drop inlet. This reduces the drainage area serviced by SS#1-17 from 2.15 Ac. to 1.94 Ac.
- SS#1-13 now outfalls to structure SS#1-11 (it previously outfalled to SS#1-5 which made the constructability of that inlet difficult.) The inverts have been adjusted between SS#1-11 and SS#1-16A.
- Inlet SS#1-16A was added. The drainage area previously served by SS#1-16 is now split between SS#1-16 and SS#1-16A.

### Sheet 9

- SS#3-2 was deepened to avoid conflicts with the utilities.

I would like to thank you and the other agencies involved for their assistance in the review of this project. Should any further questions arise, please feel free to contact us.

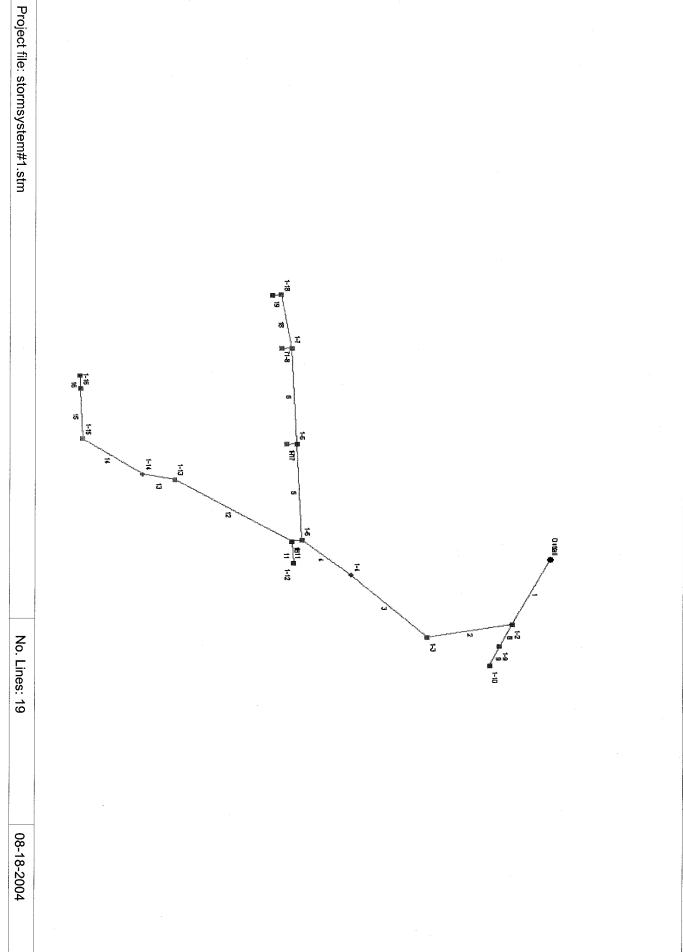
Sincerely,

**AES Consulting Engineers** 

Bryan Stevenson, P.E.

Project Manager

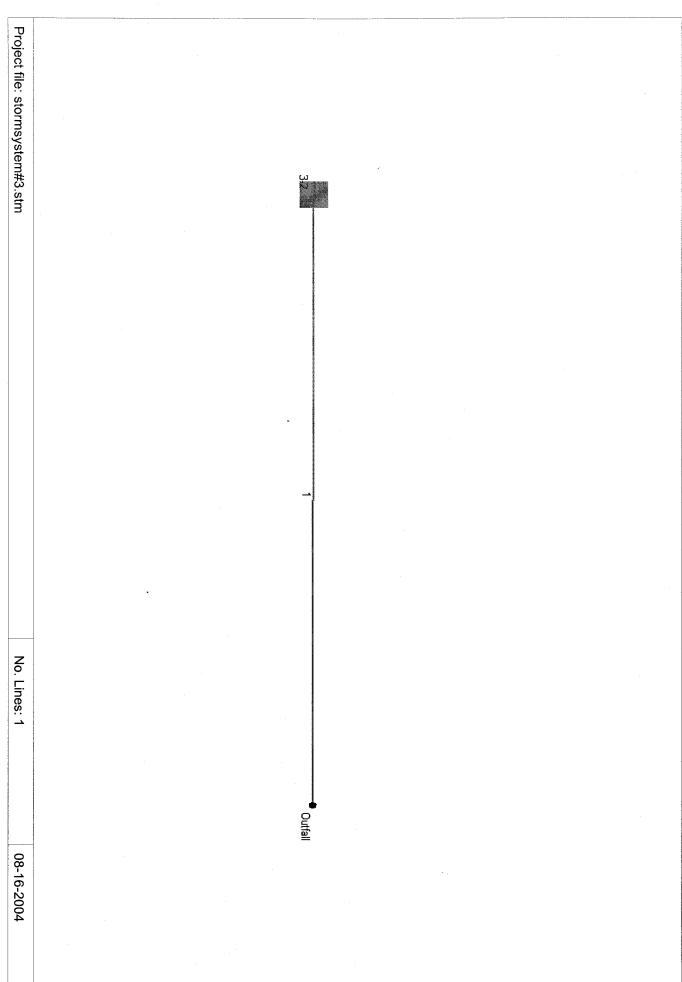
# **Hydraflow Plan View**



# **Storm Sewer Tabulation**

Number of lines: 19	Number of lines: 19	Numbe	-												stormsvstem#1.stm	nsyster		Proiect File:
													ARENS		LNEH DENIM AGE	L NEH		
87.49	87.51	85.00	85.30	1.36	5	1.44	7.54	1.76	7.0	5.0	5.0	0.25	0.25	0.70	0.36	0.36	22.0	18
87.04	87.35	82.72	85.00	1.61	15	2.45	8.18	3.01	6.9	5.3	5.0	0.43	0.18	0.70	0.62	0.26	142.0	တ
86.69	86.76	81.46	82.18	3.00	24	3.93	39.18	12.34	7.0	5.0	5.0	1.76	1.76	0.90	1.96	1.96	24.0	Οī
89.65	89.67	84.36	84.50	0.41	24	1.44	14.51	4.53	7.0	5.0	5.0	0.65	0.65	0.90	0.72	0.72	34.0	15
89.43	89.60	83.73	84.36	0.48	24	2.59	15.63	8.13	6.9	5.4	5.0	1.18	0.53	0.90	1.31	0.59	132.0	14
88.36	89.03	82.91	83.73	0.48	24	4.52	15.71	14.19	6.7	6.2	5.0	2.12	0.94	0.90	2.36	1.05	170.0	13
87.94	88.23	82.53	82.91	0.49	24	4.42	15.89	13.88	6.5	6.9	0.0	2.12	0.00	0.90	2.36	0.00	77.0	12
86.31	87.69	80.97	82.53	0.49	24	4.73	15.77	14.85	6.5	7.2	5.0	2.30	0.17	0.90	2.55	0.19	321.0	10
86.31	86.40	80.97	83.40	4.19	15	2.11	13.22	2.59	4.7	18.0	18.0	0.55	0.55	0.90	0.61	0.61	58.0	10
85.36	85.52	80.20	80.97	3.21	24	5.82	40.51	18.28	4.6	19.0	19.0	3.97	1.13	0.90	4.41	1.25	24.0	4
84.29	84.38	79.00	80.00	1.79	15	2.08	8.63	2.55	6.3	8.0	8.0	0.41	0.41	0.90	0.45	0.45	56.0	<b>∞</b>
84.00	84.18	77.15	79.00	2.89	24	3.80	38.45	11.93	5.9	10.0	10.0	2.03	1.62	0.90	2.25	1.80	64.0	_
87.04	87.08	82.72	83.42	2.92	24	2.93	38.63	9.19	7.0	5.0	5.0	1.31	1.31	0.90	1.46	1.46	24.0	တ
86.69	86.88	81.46	82.72	0.50	36	2.63	47.16	18.55	6.7	6.2	5.0	2.77	1.03	0.90	3.22	1.14	252.0	Çī
85.36	86.09	80.20	81.46	0.50	36	5.07	47.16	35.82	6.3	7.8	5.0	5.66	1.13	0.90	6.43	1.25	252.0	4
84.89	85.08	79.45	80.20	0.50	48	4.06	101.9	51.03	4.6	19.1	17.0	11.10	1.47	0.90	12.47	1.63	149.0	ω
84.56	84.85	78.23	79.45	0.50	48	4.00	101.8	50.29	4.5	19.7	0.0	11.10	0.00	0.90	12.47	0.00	243.0	2
84.00	84.27	77.15	78.23	0.53	48	4.12	104.8	51.75	4.4	20.7	12.0	11.69	0.59	0.90	13.13	0.66	203.0	
83.12	83.50	76.10	77.15	0.55	48	5.09	106.2	63.92	4 3	21.5	5.0	14.72	1.00	0.90	16.49	<u></u> - <u>-</u> 1	192.0	End
	Æ	( <del>t</del> )	( <del>†</del>	(%)	(in)	(ft/s)	(cfs)	(cfs)	(in/hr)	(min)	(min)			<u>(C)</u>	(ac)	(ac)	<b>(£)</b>	
- 1	ρ	P	ę	Slope	Size		<u> </u>		=======================================	Syst	Inlet	Total	Incr	COG	Total	Incr		- - - -
ш	HGL Elev	Invert Elev	Inve	Pipe		9	<u>ء</u> ج	10121		,	-	2 4 4	_	Knon	4	Dring Area	Len	Station

NOTES: Intensity = 140.36 / (Inlet time + 19.80) ^ 0.93; Return period = 10 Yrs.



# **Storm Sewer Tabulation**

Page 1

Pro	-	٠		Line	Sta
Project File:		Π Σ		ij J	Station
e: stori		n 0	<b>(</b>		Len
stormsystem#3.stm	<u>-</u>	3	(ac)	Incr	Drng
n#3.stm		3	(ac)	Total	Drng Area
	C. Y.	3	<u>(C)</u>		Rnoff
		3		Incr	
		3		Total	Area x C
	g.	n >	(min)	Inlet	
	· · · · · · · · · · · · · · · · · · ·	יו ס	) (min)	Syst	Tc
		7	) (in/hr)		Rain
		1	r) (cfs)		n Total
	, <u>, , , , , , , , , , , , , , , , , , </u>		) (cfs)		Cap
			) (ft/s)		Vel
	ő		(in)	Size	
	2.52	)	(%)	ze Slope	Pipe
Z					
ımber o			∄	ф	Invert Elev
Number of lines: 1	1 0 1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	,	€	Dn	Elev
_	WITH UTILITIES	}	<b>(</b>	υþ	ĭ
	<b>D</b> g			Dn	HGL Elev
_			<b>∄</b>		
Run Dat	90.55 <b>2</b>		<b>(#</b>	윤	irnd / R
Run Date: 08-16-2004	φ		(ft)	Dn	Grnd / Rim Elev
-2004	ू रू			ŀ	_
	and the second s				Line ID



5248 Olde Towne Road, Suite 1 Williamsburg, Virginia 23188 (757) 253-0040 Fax: (757) 220-8994

S S P P

PROJECT WINDS
PROJECT NO.
SUBJECT Spread
SHEET NO. 1
DATE ####
BY BWS

WINDSORMEADE MARKETPLACE 9069 Spread Calc's

# STORM WATER INLET COMPUTATIONS

		7	•		
SS1-7	<u>881-8</u>	SS1-16A	881-16	SS1-15	Number
	DI-2C	DI-2B	DI-2B	DI-2B	Type Z
20	20	6	6	8	Length
					Station
0.51 0.63	0.71	0.24 0.48	0.27	0.66	Drainage Area (Ac)
0.9	0.9	0.9	0.9	0.9	С
0.46 0.57	0.64 0.67	0.22 0.43	0.24	0.59	CA
0.46 0.57	0.64 0.67	0.22	0.24	0.59	Σ CA
6.4	6.4 6.4	6.4	6.4	6.4	l in/hr
2.94 3.63	4.09 4.26	1.38 2.76	1.56 1.84	3.8 2.25	Q-Inter (CFS)
0 0					Q Carry- Over (CFS)
2.94 6.57 3.63	4.09 8.35 4.26	1.38 4.15 2.76	1.56 3.4 1.84	3.8 6.05 2.25	Qt Gutter Flow
0 0 0	000	000	0 0 0	000	S Gutter Slope (ft/ft)
0.02 0.02 0.02	0.02 0.02 0.02	0.02 0.02 0.02	0.02 0.02 0.02	0.02 0.02 0.02	Sx Cross Slope (ft/ft)
12 12			11.3	12 12	T(Spread)
Flow Approaching From 2 0.08 Flow Approaching From Flow Approaching From 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Flow Approaching From 0.08 12 Flow Approaching From 12 Flow Approaching	10.7 Flow Approaching From 2 1 0.08 12 Flow Approaching From 12 Flow Approaching From 12 Flow Approaching From 15 Flow Approaching From 16 Flow Approaching From 15 Flow Ap	Flow Approaching From 2 0.08 Flow Approaching From	Flow Approaching From 2 0.08 Flow Approaching From	W (ft)
Flow Approaching From 2 0.08 Flow Approaching From Flow Approaching From 1 0.00 Flow Approaching From 1 0.00 Flow Approaching From 1 0.00 Flow Approaching Flow Flow Flow Flow Flow Flow Flow Flow	hproac	hpproac	hpproac	Flow Approaching From 2 0.08 Flow Approaching From	W/T
hing Fr 0.08 hing Fr	thing Fu 0.08 thing Fr	thing Fi 0.08 thing Fi	hing Fr 0.08 hing Fr	hing Fr	Sw (ft/ft)
rom	rom	rom	rom	rom	Sw/Sx
					Eo(#10)
					n
	A III				Local Dep.
					а
					S'w =a/(12W)
					Se (ft/ft) =Sx+SwEo
23.6	23.6	9.6	9.6	11.6	Lt (ft) 15 P Effec L
0.24	0.29	0.33	0.29	0.37	L/Lt d (ft)
0.46	0.46	0.46	0.46	0.46	E(#16) h (ft)
0.53	0.62	0.71	0.62	0.81	Q Int CFS d/h
12.2	14.4	16.4	14.4	18.6	Q Carryover Spread
					Remark

- NEW INJETS

SS1-5	SS1-6	SS1-13	Number	
DI-2C	DI-2C	DI-2A	Type Z	
20	20	2.5	Length	
			Station	STO
0.26 1.37	0.74	0.19 0.81 1.15	Drainage Area (Ac)	STORM WATER INLET COMPUTATIONS
0.9	0.9	0.9	С	P ≥
0.23	0.67	0.17 0.73 1.04	CA	罗思
0.23	0.67	0.17 0.73 1.04	Σ CA	NE NE
6.4	6.4	6.4	l in/hr	REVISED
1.5	4.26	1.09 4.67 6.62	Q-Inter (CFS)	₽Š
0	0	0.51	Q Carry- Over (CFS)	PUT
1.5 6.43 4.93	4.26 7.14 2.88	1.09 5.17 11.8 6.62	Qt Gutter Flow	ITA.
000	0	0.02 0 0	S Gutter Slope (ft/ft)	NO NO
0.02 0.02 0.02 0.02	0.02 0.02 0.02	0.02 0.02 0.02 0.02	Sx Cross Slope (ft/ft)	S
11.1	12 12	5.3 12 12	T(Spread)	
Flow Approaching From 2 0.08 Flow Approaching From	Flow Approaching From 2 0.08 Flow Approaching From	2 0.38 0.08 Flow Approaching From 2 0.08 Flow Approaching From 5	W (ft)	
pproac	pproac	0.38 pproac	W/T	
hing Fr 0.08 hing Fr	hing Fr 0.08 hing Fr	0.08 hing Fr 0.08 hing Fr	Sw (ft/ft)	
om	Om	om om	Sw/Sx	
		0.82	Eo(#10)	
		0.02	n	
		2	Local Dep.	
		3.44	а	
		0.14	S'w =a/(12W)	
		0.14	Se (ft/ft) =Sx+SwEo	
23.6	23.6	7.22 23.6	Lt (ft) 15 P Effec L	
0.24	0.26	0.35	L/Lt d (ft)	
0.46	0.46	0.53 0.46	E(#16) h (ft)	
0.52	0.56	0.59	Q Int CFS d/h	
12.1	12.9	0.51	Q Carryover Spread	
			Remark	

CONSULTING ENGINEERS

5248 Olde Towne Road, Suite 1 Williamsburg, Virginia 23188 (757) 253-0040 Fax: (757) 220-8994

PROJECT NO.
SUBJECT SHEET NO.
DATE
BY

BWS

Spread Calc's



5248 Olde Towne Road, Suite 1 Williamsburg, Virginia 23188 (757) 253-0040 Fax: (757) 220-8994

PROJECT
PROJECT NO.
SUBJECT
SHEET NO.
DATE
BY

Spread Calc's

BWS

# STORM WATER INLET COMPUTATIONS

																									Station	
							0.0		0.31			0.84		0.96	9	0.45	0.66	0.54		1 11	0.61		0.64	0.01	Drainage Are (Ac)	ea
							0.0	3	0.6			0.9		0.9		0	0.9	0.9	6.0	0 9	0.9		0.9	6.0	С	
							0.19	5	0.19	3		0.76		0.86	9.4	2	0.59	0.49		_	0.55		0.58	0.00	CA	
							0.18		0.19	,		0.76		0.86	4	0 41	0.59	0.49		_	0.55		0.58	0.00	Σ <b>CA</b>	
							0.4	2	6.4	)		6.4		6.4		2	6.4	6.4	9	6.4	6.4		6.4	6.4	l in/hr	
							1.19		1.19			4.84		5.53	2.00	3 70	3.8	3.11	0.00	6.3G	3.51		3.69	3.5	Q-Inter (CFS	5)
									0			0.9		1.61			0	2.2		0			1.09	_	Q Carry- Ove (CFS)	er
							1.19	2.38	1.19			5.74	12.9	7.14	60.3	3 50	3.8	5.31	0.00	6 30	3.51	8.29	4.78	3.51	Qt Gutter Flo	ow
							0	0	0			0	0	0	0.0	2	0.01	0.01		0.01	0	0	0	0.01	S Gutter Slope (ft/ft)	
							0.02	0.02	0.02			0.02	0.02	0.02	0.02	2	0.02	0.02	0.01	0 00	0.02	0.02	0.02	0.02	Sx Cross Slope (ft/ft)	
							10	;	10	i		12		12	0.	0 7	10	11.5	ī	1 3	12		12	9.7	T(Spread)	
							- low A	2	Flow A			Flow A	2	Flow /	1	3	2	2		J	Flow A	2	Flow A	2	W (ft)	
							Flow Approaching From		Flow Approaching From			Flow Approaching From		Flow Approaching From	0.2.0	0 00	0.2	0.17		0.47	Flow Approaching From	2 0.08	pproac	0.21	W/T	
							ning Fr	0.08	hing Fr			hing Fr	0.08	hing Fi	0.00	000	0.08	0.08	0.00	80.0	hing F	0.08	hing Fr	0.08	Sw (ft/ft)	
							ğ		m Om			mo		OM	4		4	4		,	mo		om	4	Sw/Sx	
															0.0	) )	0.56	0.46	5.	0 46				0.56	Eo(#10)	
															0.02	3	0.02	0.02	0.02	0 03				0.02	n	
											determine to an				_	<b>3</b>	2	2	^	J		Ì		2	Local Dep.	
															3.44	2	3.44	3.44	. <del>1</del>	3				3.44	а	
															0.14		0.14	0.14	Ç.	0 1 1				0.14	S'w =a/(12W)	)
															0.11		0.1	0.09	0.08	000				0.1	Se (ft/ft) =Sx+SwEo	
													23.6		7.01		13	16.5	17.8	470		23.6		12.6	Lt (ft) 15 F Effec L	•
								0.53					0.38		0.74	2	0.62	0.48	0.40	27.0		0.29		0.48	L/Lt d (ft)	
													0.46		1.6.0		0.82	0.7	0.00	0 00		0.46		69.0	E(#16) h (ft)	
													0.83		2.3/		3.12	3.69	4.2			0.62		2.42	Q Int CFS d/h	
													19.2		0.22		0.68	1.61	2.2	3		14.3		1.09	Q Carryover Spread	
						curve equation	from performance	Grate inlet																	Remark	

SS1-10 SS1-3 SS1-2 SS1-11

Type

\_ength

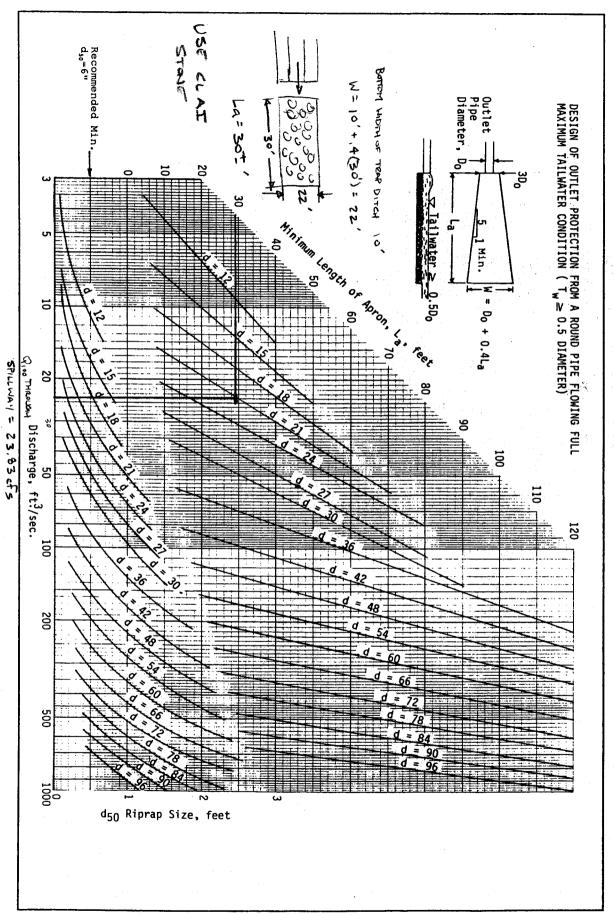
SS3-2

DI-2B DI-2B

SS1-9

SS1-18

DI-7



# **Pond Report**

Hydraflow Hydrographs by Intelisolve

Tuesday, Aug 17 2004, 4:15 PM

## Pond No. 2 - WET POND

### **Pond Data**

Pond storage is based on known contour areas. Average end area method used.

### Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	73.00	6,701	0	0
1.00	74.00	12,612	9,657	9,657
2.00	75.00	13,689	13,151	22,807
3.00	76.00	14,799	14,244	37,051
4.00	77.00	15,942	15,371	52,422
5.00	78.00	22,057	19,000	71,421
6.00	79.00	27,489	24,773	96,194
7.00	80.00	29,673	28,581	124,775
8.00	81.00	31,917	30,795	155,570
9.00	82.00	34,224	33,071	188,641
10.00	83.00	36,580	35,402	224,043
11.00	84.00	38,898	37,739	261,782
11.80	84.80	40,842	31,896	293,678

### **Culvert / Orifice Structures**

### **Weir Structures**

	[A]	[B]	[C]	[D]		[A]	[B]	[C]	[D]
Rise (in)	= 36.00	6.00	0.00	0.00	Crest Len (ft)	= 12.56	10.00	0.00	0.00
Span (in)	= 36.00	6.00	0.00	0.00	Crest El. (ft)	= 81.90	82.90	0.00	0.00
No. Barrels	= 1	1	0	0	Weir Coeff.	= 3.33	3.33	0.00	0.00
Invert El. (ft)	= 72.72	77.45	0.00	0.00	Weir Type	= Riser	CipIti		
Length (ft)	= 61.00	0.00	0.00	0.00	Multi-Stage	= Yes	No	No	No
Slope (%)	= 1.18	0.00	0.00	0.00	-				
N-Value	= .013	.013	.000	.000					
Orif. Coeff.	= 0.60	0.60	0.00	0.00					
Multi-Stage	= n/a	Yes	No	No	Exfiltration = 0	0.000 in/hr (Co	ontour) Tai	Iwater Ele	ev. = 0.00

Note: Culvert/Orifice outflows have been analyzed under inlet and outlet control.

Stage / Storage / Discharge Table												
Stage ft	Storage cuft	Elevation ft	Clv A cfs	CIv B cfs	Clv C cfs	CIv D cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Total cfs
0.00	0	73.00	0.00	0.00			0.00	0.00				0.00
0.10	966	73.10	0.62	0.00			0.00	0.00				0.00
0.20	1,931	73.20	0.62	0.00			0.00	0.00			·	0.00
0.30	2,897	73.30	0.62	0.00			0.00	0.00				0.00
0.40	3,863	73.40	0.62	0.00			0.00	0.00				0.00
0.50	4,828	73.50	0.62	0.00			0.00	0.00				0.00
0.60	5,794	73.60	0.62	0.00			0.00	0.00				0.00
0.70	6,760	73.70	0.62	0.00			0.00	0.00				0.00
0.80	7,725	73.80	0.62	0.00			0.00	0.00				0.00
0.90	8,691	73.90	0.62	0.00			0.00	0.00				0.00
1.00	9,657	74.00	0.62	0.00			0.00	0.00				0.00
1.10	10,972	74.10	0.62	0.00			0.00	0.00				0.00
1.20	12,287	74.20	0.62	0.00			0.00	0.00			·	0.00
1.30	13,602	74.30	0.62	0.00			0.00	0.00				0.00
1.40	14,917	74.40	0.62	0.00			0.00	0.00				0.00
1.50	16,232	74.50	0.62	0.00			0.00	0.00				0.00
1.60	17,547	74.60	0.62	0.00			0.00	0.00				0.00
1.70	18,862	74.70	0.62	0.00			0.00	0.00				0.00
1.80	20,177	74.80	0.62	0.00			0.00	0.00				0.00
1.90	21,492	74.90	0.62	0.00			0.00	0.00				0.00
2.00	22,807	75.00	0.62	0.00			0.00	0.00				0.00
2.10	24,231	75.10	0.62	0.00			0.00	0.00				0.00
2.20	25,656	75.20	0.62	0.00			0.00	0.00				0.00
2.30	27,080	75.30	0.62	0.00			0.00	0.00				0.00
2.40	28,505	75.40	0.62	0.00			0.00	0.00				0.00

Continues on next page...

# WET POND Stage / Storage / Discharge Table

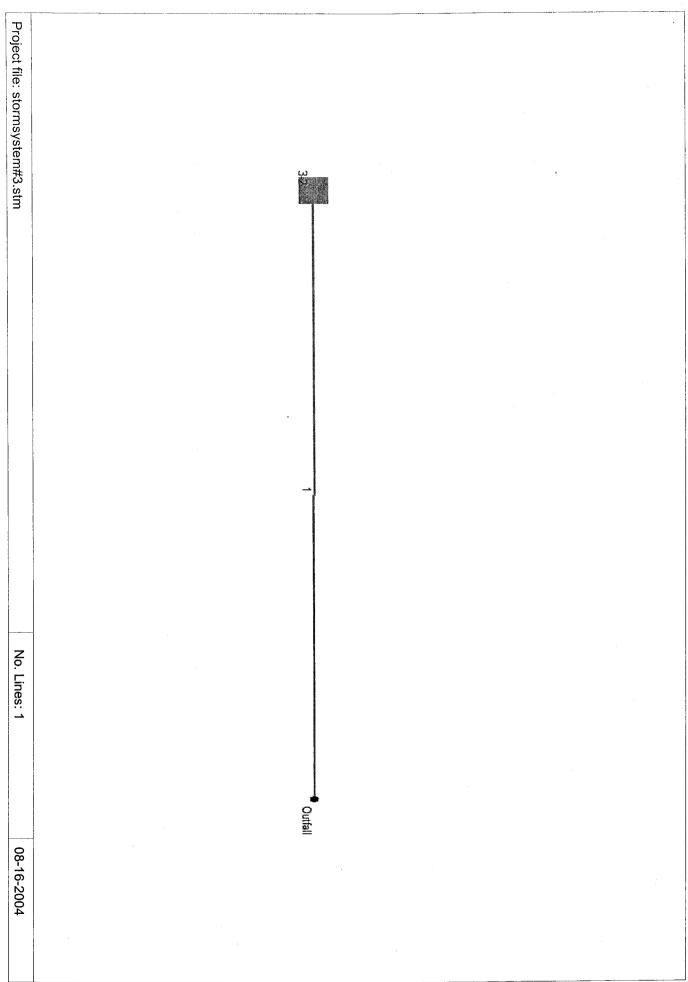
Stage	/ Storage /	Discharge	e rabie									
Stage ft	Storage cuft	Elevation ft	CIV A cfs	CIv B cfs	Clv C cfs	Clv D cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Total cfs
2.50	29,929	75.50	0.62	0.00			0.00	0.00				0.00
2.60	31,353	75.60	0.62	0.00			0.00	0.00				0.00
2.70	32,778	75.70	0.62	0.00			0.00	0.00				0.00
2.80	34,202	75.80	0.62	0.00			0.00	0.00				0.00
2.90	35,627	75.90	0.62	0.00			0.00	0.00				0.00
3.00 3.10	37,051	76.00	0.62	0.00			0.00	0.00				0.00
3.10	38,588 40,125	76.10 76.20	0.62 0.62	0.00			0.00	0.00				0.00
3.30	41,662	76.20	0.62	0.00 0.00			0.00	0.00				0.00
3.40	43,199	76.40	0.62	0.00			0.00 0.00	0.00 0.00				0.00
3.50	44,736	76.50	0.62	0.00			0.00	0.00				0.00
3.60	46,273	76.60	0.62	0.00			0.00	0.00				0.00 0.00
3.70	47,810	76.70	0.62	0.00			0.00	0.00				0.00
3.80	49,347	76.80	0.62	0.00			0.00	0.00				0.00
3.90	50,884	76.90	0.62	0.00			0.00	0.00				0.00
4.00	52,422	77.00	0.62	0.00			0.00	0.00				0.00
4.10	54,321	77.10	0.62	0.00			0.00	0.00				0.00
4.20 4.30	56,221	77.20	0.62	0.00			0.00	0.00				0.00
4.40	58,121 60,021	77.30 77.40	0.62 0.62	0.00 0.00			0.00	0.00				0.00
4.50	61,921	77.50	0.62	0.00			0.00	0.00				0.00
4.60	63,821	77.60	0.62	0.07			0.00 0.00	0.00 0.00				0.01
4.70	65,721	77.70	0.62	0.17			0.00	0.00				0.07 0.17
4.80	67,621	77.80	0.62	0.30			0.00	0.00				0.17
4.90	69,521	77.90	0.62	0.43			0.00	0.00				0.43
5.00	71,421	78.00	0.62	0.52			0.00	0.00				0.52
5.10	73,898	78.10	0.62	0.60			0.00	0.00				0.60
5.20	76,376	78.20	0.67	0.67			0.00	0.00				0.67
5.30 5.40	78,853 81,330	78.30 78.40	0.74	0.73			0.00	0.00				0.73
5.50	83,807	78.40 78.50	0.81 0.88	0.79 0.85			0.00	0.00				0.79
5.60	86,285	78.60	0.88	0.83			0.00 0.00	0.00 0.00				0.85
5.70	88,762	78.70	0.96	0.95			0.00	0.00				0.90
5.80	91,239	78.80	1.04	0.99			0.00	0.00				0.95 0.99
5.90	93,717	78.90	1.04	1.04			0.00	0.00				1.04
6.00	96,194	79.00	1.13	1.08			0.00	0.00				1.08
6.10	99,052	79.10	1.13	1.12			0.00	0.00				1.12
6.20	101,910	79.20	1.22	1.16			0.00	0.00				1.16
6.30	104,768 107,626	79.30	1.22	1.20			0.00	0.00				1.20
6.40 6.50	107,626	79.40 79.50	1.23 1.32	1.23			0.00	0.00				1.23
6.60	113,343	79.50 79.60	1.32	1.27 1.30			0.00	0.00	***			1.27
6.70	116,201	79.70	1.34	1.34			0.00 0.00	0.00				1.30
6.80	119,059	79.80	1.42	1.37			0.00	0.00 0.00				1.34
6.90	121,917	79.90	1.42	1.40			0.00	0.00				1.37 1.40
7.00	124,775	80.00	1.43	1.43			0.00	0.00				1.43
7.10	127,855	80.10	1.53	1.46			0.00	0.00				1.46
7.20	130,934	80.20	1.53	1.49			0.00	0.00				1.49
7.30	134,014	80.30	1.53	1.52			0.00	0.00				1.52
7.40	137,093	80.40	1.55	1.55			0.00	0.00				1.55
7.50 7.60	140,173 143,252	80.50 80.60	1.64 1.64	1.58			0.00	0.00				1.58
7.70	146,332	80.70	1.64	1.61 1.64			0.00	0.00				1.61
7.80	149,411	80.80	1.66	1.66			0.00 0.00	0.00 0.00				1.64
7.90	152,491	80.90	1.76	1.69			0.00	0.00				1.66 1.69
8.00	155,570	81.00	1.76	1.72			0.00	0.00				1.72
8.10	158,877	81.10	1.76	1.74			0.00	0.00				1.74
8.20	162,184	81.20	1.77	1.77			0.00	0.00				1.77
8.30	165,491	81.30	1.79	1.79			0.00	0.00				1.79
8.40	168,798	81.40	1.89	1.82			0.00	0.00				1.82
8.50	172,105	81.50	1.89	1.84			0.00	0.00				1.84
8.60 8.70	175,412 178,710	81.60	1.89	1.87			0.00	0.00				1.87
8.80	178,719 182,026	81.70 81.80	1.89	1.89			0.00	0.00				1.89
8.90	185,333	81.80	1.91 2.02	1.91 1.94			0.00	0.00				1.91
9.00	188,641	82.00	3.30	1.94			0.00	0.00				1.94
9.10	192,181	82.10	5.74	1.98			1.32 3.74	0.00 0.00				3.28
9.20	195,721	82.20	9.01	2.01			5.74 6.87	0.00				5.72 8.88
9.30	199,261	82.30	12.63	2.03			10.58	0.00				0.00 12.61
9.40	202,801	82.40	17.14	2.05			14.79	0.00				16.84
							🕶					10.07

WET POND

Stage / St	torage /	Discharge	Table
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Stage ft	Storage cuft	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	Clv D cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Total cfs
,,,	cuit	11	CIS	CIS	CIS	CIS	CIS	CIS	CIS	CIS	Cis	CIS
9.50	206,342	82.50	21.51	2.07			19.44	0.00				21.51
9.60	209,882	82.60	26.71	2.09			24.49	0.00				26.59
9.70	213,422	82.70	32.09	2.11			29.93	0.00				32.04
9.80	216,962	82.80	37.84	2.13			35.71	0.00				37.84
9.90	220,502	82.90	43.98	2.16			41.82	0.00				43.98
10.00	224,043	83.00	50.43	2.18			48.25	1.05				51.48
10.10	227,816	83.10	57.18	2.20			54.98	2.98				60.16
10.20	231,590	83.20	64.19	2.20			61.99	5.47				69.67
10.30	235,364	83.30	71.33	2.05			69.28	8.42				79.75
10.40	239,138	83.40	78.69	1.85			76.84	11.77				90.46
10.50	242,912	83.50	86.25	1.60			84.65	15.48				101.72
10.60	246,686	83.60	93.96	1.25			92.70	19.50				113.46
10.70	250,460	[83.70]	97.04	1.10			95.94	23.83				120.86
10.80	254,234	83.80	98.87	1.01			97.86	28.43				127.30
10.90	258,008	83.90	100.37	0.94			99.43	33.30				133.66
11.00	261,782	84.00	101.65	0.88			100.77	38.42				140.07
11.08	264,971	84.08	102.57	0.83			101.73	42.68				145.25
11.16	268,161	84.16	103.42	0.79			102.62	47.10				150.51
11.24	271,350	84.24	104.20	0.76			103.44	51.65				155.85
11.32	274,540	84.32	104.95	0.73			104.22	56.35				161.29
11.40	277,730	84.40	105.65	0.70			104.95	61.18				166.82
11.48	280,919	84.48	106.31	0.67			105.64	66.14				172.44
11.56	284,109	84.56	106.95	0.64			106.30	71.22				178.17
11.64	287,298	84.64	107.56	0.62			106.94	76.43			-	183.99
11.72	290,488	84.72	108.15	0.60			107.55	81.76				189.91
11.80	293,678	84.80	108.73	0.58			108.15	87.21				195.93

...End



## **Storm Sewer Tabulation**

Number of lines: 1
WITH UTILITIE
7.0 7.11 12.11 5.80 15 2.52 78.96 77.70 83.55
(min) (in/hr) (cfs) (cfs) (ft/s) (in) (%) (ft) (ft) (ft)
Rain Total Cap Vel Pipe Invert Elev HGL Elev



5248 Olde Towne Road, Suite 1 Williamsburg, Virginia 23188 (757) 253-0040 Fax: (757) 220-8994

STORM WATER INLET COMPUTATIONS

PROJECT
PROJECT NO.
SUBJECT
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DATE
BY

Spread Calc's

BWS

###

		1-7			51-8			S1-16A				S1-16			\$1-15		Number	z
		DI-2C			DI-2C			DI-2B				DI-2B			DI-2B		Туре	NLET
		20			20			6				6			8		Length	
																	Station	
	0.63	0.51	1	0.74		0.71	0.48	5	0.24		0.32	0.27		0.39		0.66	Drainage A (Ac)	rea
L	0.9	0.9	M	0.9		0.9	0.9		0.9		0.9	0.9		0.9		0.9	С	
L	0.57	0.46		0.67		0.64	0.43		0.22		0.29	0.24		0.35		0.59	CA	
L	0.57	0.46		0.67		0.64	0.43		0.22		0.29	0.24		0.35		0.59	Σ CA	
L	6.4	6.4		6.4		6.4	6.4		6.4		6.4	6.4		6.4		6.4	l in/hr	
	3.63	2.94		4.26		4.09	2.76		1.38		1.84	1.56		2.25		3.8	Q-Inter (CF	
L	0	0															Q Carry- Ov (CFS)	/er
L	3.63	2.94 6.57		4.26	8.35	4.09	2.76	4.15	1.38		1.84	1.56 3.4		2.25	6.05	3.8	Qt Gutter Fl	low
L	0	00		0	0	0	0	0	0		0	90		0	0	0	S Gutter Slope (ft/ft)	
L	0.02	0.02		0.02	0.02	0.02	0.02	0.02	0.02		0.02	0.02		0.02	0.02	0.02	Sx Cross Slope (ft/ft)	
L	12	12		12		12	12		10.7	ı	12	11.3		12		12	T(Spread)	
	Flow A	Flow A		Flow A	2	Flow A	Flow A	2	Flow A		Flow A	Flow A		Flow A	2	Flow A	W (ft)	
	pproa	pproa		pproac		pproa	pproac		pproac		pproac	pproac		pproac		pproac	W/T	
	— ত:	- 인	-			<u>Ω</u>							_		1			
L	ching Fro	ching Fro		ning Fr	0.08	ching Fr	hing Fr	0.08	ning Fr	an.	ing Fn	o.og Fr		hing Fr	0.08	hing Fr	Sw (ft/ft)	
	Flow Approaching From	Flow Approaching From 2 0.08		Flow Approaching From	0.08	Flow Approaching From	Flow Approaching From	0.08	Flow Approaching From	i i	Flow Approaching From	Flow Approaching From 0.08		Flow Approaching From	0.08	Flow Approaching From	Sw (ft/ft) Sw/Sx	
	ching From	ching From 0.08		ing From	0.08	ching From	hing From	0.08	ning From		ing From	ning From 0.08		hing From	0.08	ching From		
	ching From	ching From 0.08		ing From	0.08	ching From	hing From	0.08	ning From		ing From	ning From 0.08		hing From	0.08	ching From	Sw/Sx	
	ching From	ching From 0.08		ning From	0.08	ching From	hing From	0.08	ning From		ing From	ning From 0.08		hing From	0.08	ching From	Sw/Sx Eo(#10)	
	ching From	ching From		ing From	0.08	ching From	hing From	0.08	ning From		ing From	ning From		hing From	0.08	ching From	Sw/Sx Eo(#10)	
	ching From	ching From		ing From	0.08	ching From	hing From	0.08	ning From		ing From	ning From 0.08		hing From	0.08	ching From	Sw/Sx Eo(#10) n Local Dep. a S'w =a/(12V)	(\$
	ching From	ching From		ing From	0.08	ching From	hing From	0.08	ning From		ing From	ning From 0.08		hing From	0.08	ching From	Sw/Sx  Eo(#10)  n  Local Dep.  a  S'w =a/(12W)  Se (ft/ft) =Sx+SwEo	
		ching From		ing From	0.08 23.6	ching From	hing From	0.08 9.6	ning From			0.08 9.6		hing From	0.08	ching From	Sw/Sx  Eo(#10)  n  Local Dep.  a  S'w =a/(12W)  Se (ft/ft) =Sx+SwEo  Lt (ft) 15  Effec L	V)
				ing From		ching From	hing From		ning From							ching From	Sw/Sx  Eo(#10)  n  Local Dep.  a  S'w =a/(12W)  Se (ft/ft) =Sx+SwEo  Lt (ft) 15  Effec L  L/Lt d (ft)	P
		23.6		ing From	23.6	ching From	hing From	9.6	ning From			9.6			11.6	ching From	Sw/Sx  Eo(#10)  n  Local Dep.  a  S'w =a/(12V)  Se (ft/ft) =Sx+SwEo  Lt (ft) 15 Effec L  L/Lt d (ft)  E(#16) h (ft)	P
		23.6 0.24		ing From	23.6 0.29	ching From	hing From	9.6 0.33	ling From			9.6 0.29			11.6 0.37	shing From	Sw/Sx  Eo(#10)  n  Local Dep.  a  S'w =a/(12V)  Se (ft/ft) =Sx+SwEo  Lt (ft) 15 Effec L  L/Lt d (ft)  E(#16) h (ft)  Q Int CFS d/h	P
		23.6 0.24 0.46		ing From	23.6 0.29 0.46	ching From	hing From	9.6 0.33 0.46	ling From			9.6 0.29 0.46			11.6 0.37 0.46	thing From	Sw/Sx  Eo(#10)  n  Local Dep.  a  S'w =a/(12V)  Se (ft/ft) =Sx+SwEo  Lt (ft) 15 Effec L  L/Lt d (ft)  E(#16) h (ft)  Q Int CFS	P

Remark

SS1-16A

SS1-16

SS1-15

- NEW INJET'S

SS1-5	SS1-6	SS1-13 SS1-17	Number	
DI-2C	DI-2C	DI-2A DI-3C	Type Z	
20	C 20	A 2.5	Length	
			Station	STO
0.26 1.37	0.74	0.19 0.81 1.15	Drainage Area (Ac)	STORM WATER INLET COMPUTATIONS
7 0.9	0.9	0.9	С	K A
0.23	0.67	0.17 0.73 1.04	CA	TER II
0.23	0.67	0.17 0.73 1.04	Σ CA	NLE NLE
6.4	6.4	6.4	l in/hr	REVISES
1.5 4.93	4.26	1.09 4.67 6.62	Q-Inter (CFS)  Q Carry- Over	
0	0	0.51	(CFS)	TU'
1.5 6.43 4.93	4.26 7.14 2.88	1.09 C 5.17 11.8 6.62	Qt Gutter Flow S Gutter	
000	000	0.02	Slope (ft/ft) Sx Cross	SN
0.02	0.02 0.02 0.02	0.02	Slope (ft/ft) T(Spread)	
11.1 Flor	12 Flo	5.3 12 Flov 12 Flov	W (ft)	
w Appro 2 W Appro	w Appro	2 0.38 w Approac 2 w Approac	w/T	
Flow Approaching From 2 0.08 Flow Approaching From	12 Flow Approaching From 2 0.08 12 Flow Approaching From	2 0.38 0.08 Flow Approaching From 2 0.08 Flow Approaching From 2	Sw (ft/ft)	
From From	From		Sw/Sx	
		4 0.82	Eo(#10)	
		0.02	n	
		2	Local Dep.	
		3.44	а	
		0.14	S'w =a/(12W)	
		0.14	Se (ft/ft) =Sx+SwEo	
23.6	23.6	7.22	Lt (ft) 15 P Effec L	
0.24	0.26	0.36	L/Lt d (ft) E(#16) h	
0.46	0.46	0.53	(ft) R Q Int CFS	
0.52	0.56	0.59 (	d/h Q Carryover	
12.1	12.9	0.51	Spread	
			Remark	

CONSULTING ENGINEERS

5248 Olde Towne Road, Suite 1 Williamsburg, Virginia 23188 (757) 253-0040 Fax: (757) 220-8994

PROJECT NO.
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Spread Calc's



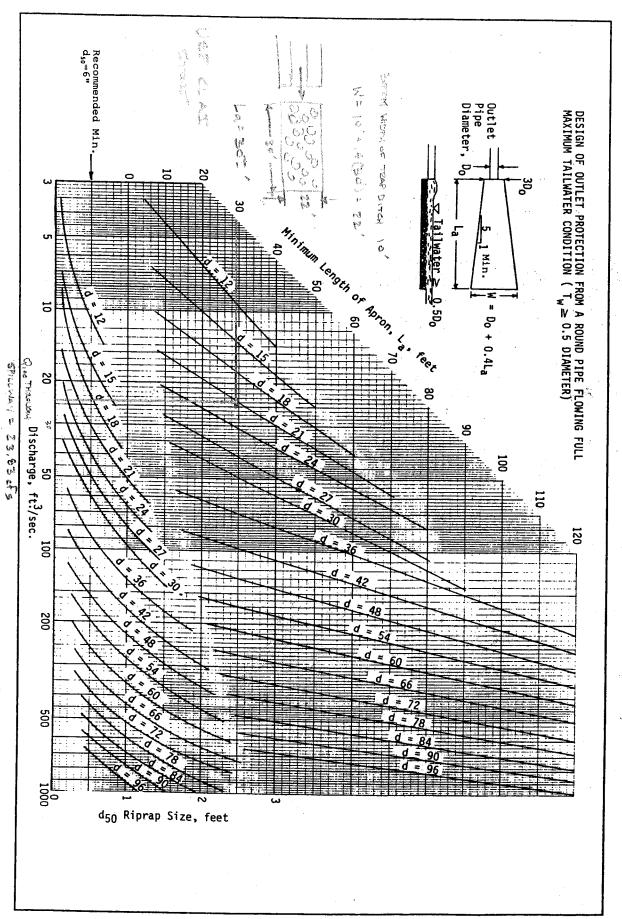
5248 Olde Towne Road, Suite 1 Williamsburg, Virginia 23188 (757) 253-0040 Fax: (757) 220-8994

PROJECT
PROJECT NO.
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SHEET NO.
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Spread Calc's 1 BWS

# STORM WATER INLET COMPUTATIONS

		Ī										SS1-18				851-9	×		SS1-10	SS1-3	SS1-2		SS3-2			SS1-11		0	SS1-17	Maria
																														Number Z
	_	_		_		-	-					DI-7				טו-20			DI-2B	DI-2B	DI-2B		DI-2B			DI-2C		7	H H H	Type □
	-				_			L	_			2.5				20		,	∞	00			<u></u>			20				Length
																														Station
	_										0.31		0.31		0.84		0.96	0.10	0.45	0.66	0.54		1.11		0.61		0.64	0.0	0 81	Drainage Area (Ac)
											0.6		0.6		9.0		0.9	100	0.9	0.9	0.9		0.9		0.9		0.9	c.	9	С
											0.19		0.19		0.76	1	0.86	9	0 41	0.59	0.49		_		0.55		0.58	0.00	7.5	CA
ı											0.19		0.19		0.76		0.86		0 41	0.59	0.49		_		0.55		0.58	0.00	7,5	Σ CA
											6.4		6.4		6.4		6.4	9	6.4	6.4	6.4		6.4		6.4		6.4	ç	5,	l in/hr
											1.19		1.19		4.84		5.53	1.00	2 59	3.8	3.11		6.39		3.51		3.69	0.01	, ,	Q-Inter (CFS)
													0		0.9		1.61		0	o	2.2		o				1.09		ı	Q Carry- Over (CFS)
											1.19	2.38	1.19		5.74	12.9	7.14	1.00	2 50	3.8	5.31		6.39		3.51	8 29	4.78	0.0	, , ,	Qt Gutter Flow
											0	0	0		0	0	0	6.6	0.01	0.01	0.01		0.01		0	0	0	0.0		S Gutter Slope (ft/ft)
ļ											0.02	0.02	0.02		0.02	0.02	0.02	0.02	0 03	0.02	0.02		0.02		0.02	0.02	0.02	0.02		Sx Cross Slope (ft/ft)
											10		10		12	;	12	9	8 7	10	11.5		73		12		12	9.7	4	T(Spread)
l											Flow Approaching From	2	Flow Approaching From		Flow Approaching From	2	Flow Approaching From		<b>3</b>	2	2		2		Flow Approaching From	2 0.08	Flow A	_		W (ft)
l				 							pproac		pproac		pproac		pproac	0.2.0	0 23	0.2	0.17		0.17		pproac		pproac	0.21	,	W/T
											hing Fr	0.08	hing Fr		hing Fr	0.08	hing Fr	0.00	008	0.08	0.08	91	0.08	٥	hina Fr	80.0	hina Fr	0.00	7 1	Sw (ft/ft)
											om		a :		om		mo		4	4	4		4		S		S	4		Sw/Sx
																		ć	O 6	0.56	0.46	:	0.46					0.00	32	Eo(#10)
																		0.02	0 00	0.02	0.02		0.02					0.02		n
																			J	2	2		2					7		Local Dep.
																		-	۱ ۱	3.44	3.44	9	3.44					J.44		а
																			0 14	0.14	0.14	9	0.14					0.14		S'w =a/(12W)
																		9	0 11	0.1	0.09	9	0.09					Ç.	1	Se (ft/ft) =Sx+SwEo
																23.6			17.7	13	16.5		17.9		20:0	23 <b>6</b>		12.0		Lt (ft) 15 P Effec L
												0.53				0.38			7.7 N	0.62	0.48	9	0.45		0.1.0	0 29		0.48		L/Lt d (ft)
																0.46			001	0.82	0.7	0.00	0.66		9	0.46		0.69		E(#16) h (ft)
																0.83		1.0.7	2 27	3.12	3.69	i	4.2		0.01	0 62		2.42		Q Int CFS d/h
																19.2		77.0	0 00	0.68	1.61	!	2.2			143		60.1		Q Carryover Spread
										curve equation	from performance	Grate inlet																		Remark



### **Pond Report**

Hydraflow Hydrographs by Intelisolve

Tuesday, Aug 17 2004, 4:15 PM

### Pond No. 2 - WET POND

### **Pond Data**

Pond storage is based on known contour areas. Average end area method used.

### Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	73.00	6,701	0	0
1.00	74.00	12,612	9,657	9,657
2.00	75.00	13,689	13,151	22,807
3.00	76.00	14,799	14,244	37,051
4.00	77.00	15,942	15,371	52,422
5.00	78.00	22,057	19,000	71,421
6.00	79.00	27,489	24,773	96.194
7.00	80.00	29,673	28,581	124,775
8.00	81.00	31,917	30,795	155,570
9.00	82.00	34,224	33,071	188,641
10.00	83.00	36,580	35,402	224,043
11.00	84.00	38,898	37,739	261,782
11.80	84.80	40,842	31,896	293,678

Culvert	1	Orific	a Str	ucturas
Guiveil	•		e Jui	uctures

Weir Structur	res	
---------------	-----	--

	[A]	[B]	[C]	[D]		[A]	[B]	[C]	[D]
Rise (in)	= 36.00	6.00	0.00	0.00	Crest Len (ft)	= 12.56	10.00	0.00	0.00
Span (in)	= 36.00	6.00	0.00	0.00	Crest El. (ft)	= 81.90	82.90	0.00	0.00
No. Barrels	= 1	1	0	0	Weir Coeff.	= 3.33	3.33	0.00	0.00
Invert El. (ft)	= 72.72	77.45	0.00	0.00	Weir Type	= Riser	Ciplti		
Length (ft)	= 61.00	0.00	0.00	0.00	Multi-Stage	= Yes	No.	No	No
Slope (%)	= 1.18	0.00	0.00	0.00	_				
N-Value	= .013	.013	.000	.000					
Orif. Coeff.	= 0.60	0.60	0.00	0.00					
Multi-Stage	= n/a	Yes	No	No	Exfiltration = 0	0.000 in/hr (Co	ontour) Tai	lwater Ele	ev. = 0.00 ft

Note: Culvert/Orifice outflows have been analyzed under inlet and outlet control.

Stage /	Storage /	Discharge	Table				Note: Cun	vert/Oritice ou	τιows nave b	een analyzed	under inlet and	outlet control.
Stage ft	Storage cuft	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	Clv D cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Total cfs
0.00	0	73.00	0.00	0.00			0.00	0.00				0.00
0.10	966	73.10	0.62	0.00			0.00	0.00				0.00
0.20	1,931	73.20	0.62	0.00			0.00	0.00				0.00
0.30	2,897	73.30	0.62	0.00			0.00	0.00				0.00
0.40	3,863	73.40	0.62	0.00			0.00	0.00				0.00
0.50	4,828	73.50	0.62	0.00			0.00	0.00				0.00
0.60	5,794	73.60	0.62	0.00			0.00	0.00				0.00
0.70	6,760	73.70	0.62	0.00			0.00	0.00				0.00
0.80	7,725	73.80	0.62	0.00			0.00	0.00				0.00
0.90	8,691	73.90	0.62	0.00			0.00	0.00				0.00
1.00	9,657	74.00	0.62	0.00			0.00	0.00				0.00
1.10	10,972	74.10	0.62	0.00			0.00	0.00				0.00
1.20	12,287	74.20	0.62	0.00			0.00	0.00				0.00
1.30	13,602	74.30	0.62	0.00			0.00	0.00				0.00
1.40	14,917	74.40	0.62	0.00			0.00	0.00				0.00
1.50	16,232	74.50	0.62	0.00			0.00	0.00				0.00
1.60	17,547	74.60	0.62	0.00			0.00	0.00				0.00
1.70	18,862	74.70	0.62	0.00			0.00	0.00				0.00
1.80	20,177	74.80	0.62	0.00			0.00	0.00				0.00
1.90	21,492	74.90	0.62	0.00			0.00	0.00				0.00
2.00	22,807	75.00	0.62	0.00			0.00	0.00				0.00
2.10	24,231	75.10	0.62	0.00			0.00	0.00				0.00
2.20	25,656	75.20	0.62	0.00			0.00	0.00				0.00
2.30	27,080	75.30	0.62	0.00			0.00	0.00				0.00
2.40	28,505	75.40	0.62	0.00			0.00	0.00				0.00

Continues on next page...

WET POND Stage / Storage / Discharge Table

Stage /	Storage /	Discharge	apie									
Stage ft	Storage cuft	Elevation ft	CIv A cfs	Clv B cfs	Clv C cfs	CIV D	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Total cfs
2.50	29,929	75.50	0.62	0.00			0.00	0.00				0.00
2.60	31,353	75.60	0.62	0.00			0.00	0.00				0.00
2.70	32,778	75.70	0.62	0.00			0.00	0.00				0.00
2.80	34,202	75.80	0.62	0.00			0.00	0.00				0.00
2.90	35,627	75.90	0.62	0.00			0.00	0.00				0.00
3.00	37,051	76.00	0.62	0.00			0.00	0.00				0.00
3.10	38,588	76.10	0.62	0.00			0.00	0.00				0.00
3.20	40,125	76.20 76.30	0.62 0.62	0.00 0.00			0.00 0.00	0.00 0.00				0.00 0.00
3.30 3.40	41,662 43,199	76.30 76.40	0.62	0.00			0.00	0.00				0.00
3.50	44,736	76.50	0.62	0.00			0.00	0.00				0.00
3.60	46,273	76.60	0.62	0.00			0.00	0.00				0.00
3.70	47,810	76.70	0.62	0.00			0.00	0.00				0.00
3.80	49,347	76.80	0.62	0.00			0.00	0.00	-			0.00
3.90	50,884	76.90	0.62	0.00			0.00	0.00				0.00
4.00	52,422	77.00	0.62	0.00			0.00	0.00				0.00
4.10 4.20	54,321 56,221	77.10 77.20	0.62 0.62	0.00 0.00			0.00 0.00	0.00 0.00				0.00 0.00
4.20	58,121	77.30	0.62	0.00			0.00	0.00				0.00
4.40	60,021	77.40	0.62	0.00			0.00	0.00				0.00
4.50	61,921	77.50	0.62	0.01			0.00	0.00				0.01
4.60	63,821	77.60	0.62	0.07			0.00	0.00				0.07
4.70	65,721	77.70	0.62	0.17			0.00	0.00				0.17
4.80	67,621	77.80	0.62	0.30			0.00	0.00				0.30
4.90	69,521	77.90	0.62 0.62	0.43 0.52			0.00 0.00	0.00 0.00				0.43 0.52
5.00 5.10	71,421 73,898	78.00 78.10	0.62	0.60			0.00	0.00				0.60
5.20	76,376	78.20	0.67	0.67			0.00	0.00				0.67
5.30	78,853	78.30	0.74	0.73			0.00	0.00				0.73
5.40	81,330	78.40	0.81	0.79			0.00	0.00				0.79
5.50	83,807	78.50	0.88	0.85			0.00	0.00				0.85
5.60	86,285	78.60	0.90	0.90			0.00	0.00				0.90
5.70	88,762	78.70	0.96	0.95			0.00	0.00 0.00				0.95 0.99
5.80 5.90	91,239 93,717	78.80 78.90	1.04 1.04	0.99 1.04			0.00 0.00	0.00				1.04
6.00	96,194	79.00	1.13	1.08			0.00	0.00				1.08
6.10	99,052	79.10	1.13	1.12			0.00	0.00				1.12
6.20	101,910	79.20	1.22	1.16			0.00	0.00				1.16
6.30	104,768	79.30	1.22	1.20			0.00	0.00				1.20
6.40	107,626	79.40	1.23	1.23			0.00	0.00				1.23
6.50	110,485	79.50	1.32	1.27			0.00	0.00				1.27
6.60 6.70	113,343 116,201	79.60 79.70	1.32 1.34	1.30 1.34			0.00 0.00	0.00 0.00				1.30 1.34
6.80	119,059	79.70 79.80	1.42	1.37			0.00	0.00				1.37
6.90	121,917	79.90	1.42	1.40			0.00	0.00				1.40
7.00	124,775	80.00	1.43	1.43			0.00	0.00				1.43
7.10	127,855	80.10	1.53	1.46			0.00	0.00				1.46
7.20	130,934	80.20	1.53	1.49			0.00	0.00				1.49
7.30	134,014	80.30	1.53	1.52			0.00	0.00				1.52
7.40	137,093	80.40	1.55 1.64	1.55 1.58			0.00 0.00	0.00 0.00				1.55 1.58
7.50 7.60	140,173 143,252	80.50 80.60	1.64	1.61			0.00	0.00				1.61
7.70	146,332	80.70	1.64	1.64			0.00	0.00				1.64
7.80	149,411	80.80	1.66	1.66			0.00	0.00				1.66
7.90	152,491	80.90	1.76	1.69			0.00	0.00				1.69
8.00	155,570	81.00	1.76	1.72			0.00	0.00				1.72
8.10	158,877	81.10	1.76	1.74			0.00	0.00				1.74
8.20	162,184	81.20	1.77	1.77			0.00	0.00				1.77
8.30	165,491	81.30	1.79	1.79			0.00 0.00	0.00 0.00				1.79 1.82
8.40 8.50	168,798 172,105	81.40 81.50	1.89 1.89	1.82 1.84			0.00	0.00				1.84
8.60	172,103	81.60	1.89	1.87			0.00	0.00				1.87
8.70	173,412	81.70	1.89	1.89			0.00	0.00				1.89
8.80	182,026	81.80	1.91	1.91			0.00	0.00				1.91
8.90	185,333	81.90	2.02	1.94			0.00	0.00				1.94
9.00	188,641	82.00	3.30	1.96			1.32	0.00				3.28
9.10	192,181	82.10	5.74	1.98			3.74	0.00				5.72
9.20	195,721	82.20	9.01	2.01			6.87	0.00				8.88
9.30	199,261	82.30	12.63	2.03 2.05			10.58 14.79	0.00 0.00				12.61 16.84
9.40	202,801	82.40	17.14	∠.∪5			14.79	0.00				10.04

### WET POND Stage / Storage / Discharge Table

Stage ft	Storage cuft	Elevation ft	CIv A cfs	Clv B cfs	Clv C cfs	Clv D cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Total cfs
									0.0	0.0	0,0	0.5
9.50	206,342	82.50	21.51	2.07			19.44	0.00				21.51
9.60	209,882	82.60	26.71	2.09			24.49	0.00				26.59
9.70	213,422	82.70	32.09	2.11			29.93	0.00				32.04
9.80	216,962	82.80	37.84	2.13			35.71	0.00				37.84
9.90	220,502	82.90	43.98	2.16			41.82	0.00				43.98
10.00	224,043	83.00	50.43	2.18			48.25	1.05				51.48
10.10	227,816	83.10	57.18	2.20			54.98	2.98				60.16
10.20	231,590	83.20	64.19	2.20			61.99	5.47				69.67
10.30	235,364	83.30	71.33	2.05			69.28	8.42				79.75
10.40	239,138	83.40	78.69	1.85			76.84	11.77				90.46
10.50	242,912	83.50	86.25	1.60			84.65	15.48				101.72
10.60	246,686	83.60	93.96	1.25			92.70	19.50				113.46
10.70	250,460	83.70	97.04	1.10			95.94	23.83)				120.86
10.80	254,234	83.80	98.87	1.01			97.86	28.43				127.30
10.90	258,008	83.90	100.37	0.94			99.43	33.30				133.66
11.00	261,782	84.00	101.65	0.88			100.77	38.42				140.07
11.08	264,971	84.08	102.57	0.83			101.73	42.68				145.25
11.16	268,161	84.16	103.42	0.79			102.62	47.10				150.51
11.24	271,350	84.24	104.20	0.76			103.44	51.65				155.85
11.32	274,540	84.32	104.95	0.73			104.22	56.35				161.29
11.40	277,730	84.40	105.65	0.70			104.95	61.18				166.82
11.48	280,919	84.48	106.31	0.67			105.64	66.14				172.44
11.56	284,109	84.56	106.95	0.64			106.30	71.22				178.17
11.64	287,298	84.64	107.56	0.62			106.94	76.43				183.99
11.72	290,488	84.72	108.15	0.60			107.55	81.76				189.91
11.80	293,678	84.80	108.73	0.58			108.15	87.21				195.93

...End

## Project file: stormsystem#1.stm No. Lines: 19 · 08-18-2004

NOTE	Proj		19	18	17	16	5	14	ವ	12	1	10	9	00	7	0	O1	4	ω	2	->		Line	Station
S: Inte	Project File:		18	<u></u> თ	Ŋ	5	4	13	12	75	10	4	<b>∞</b>	_	<u>ნ</u>	<u>ტ</u>	4	ω	2	_	End		- - - - -	ion
NOTES: Intensity = 140.36 / (Inlet time + 19.80) ^ 0.93;			22.0	142.0	24.0	34.0	132.0	170.0	77.0	321.0	58.0	24.0	56.0	64.0	24.0	252.0	252.0	149.0	243.0	203.0	192.0	æ		Len
140.36 /	stormsystem#1.stm	r3k1	0.36	0.26	1.96	0.72	0.59	1.05	0.00	0.19	0.61	1.25	0.45	1.80	1.46	1.14	1.25	1.63	0.00	0.66	1.1	(ac)	Incr	Drng Area
(Inlet ti	#1.stm	JEAN L	0.36	0.62	1.96	0.72	1.31	2.36	2.36	2.55	0.61	4.41	0.45	2.25	1.46	3.22	6.43	12.47	12.47	13.13	16.49	(ac)	Total	Area
me + 19		Sec >	0.70	0.70	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0	000	Rnoff
9.80) ^ 0		AREAS	0.25	0.18	1.76	0.65	0.53	0.94	0.00	0.17	0.55	1.13	0.41	1.62	1.31	1.03	1.13	1.47	0.00	0.59	1.00		Incr	Are
į .			0.25	0.43	1.76	0.65	1.18	2.12	2.12	2.30	0.55	3.97	0.41	2.03	1.31	2.77	5.66	11.10	11.10	11.69	14.72		Total	Area x C
Return period =			5.0	5.0	5.0	5.0	5.0	5.0	0.0	5.0	18.0	19.0	8.0	10.0	5.0	5.0	5.0	17.0	0.0	12.0	5.0	(min)	Inlet	_
1			5.0	5.3	5.0	5.0	5.4	6.2	6.9	7.2	18.0	19.0	8.0	10.0	5.0	6.2	7.8	19.1	19.7	20.7	21.5	(min)	Syst	Тс
10 Yrs.			7.0	6.9	7.0	7.0	6.9	6.7	6.5	6.5	4.7	4.6	6.3	5.9	7.0	6.7	6.3	4.6	4.5	4.4	4.3	(in/hr)	3	Rain
			1.76	3.01	12.34	4.53	8.13	14.19	13.88	14.85	2.59	18.28	2.55	11.93	9.19	18.55	35.82	51.03	50.29	51.75	63.92	(cfs)		Total
			7.54	8.18	39.18	14.51	15.63	15.71	15.89	15.77	13.22	40.51	8.63	38.45	38.63	47.16	47.16	101.9	101.8	104.8	106.2	(cfs)	<u> </u>	Cap
			1.44	2.45	3.93	1.44	2.59	4.52	4.42	4.73	2.11	5.82	2.08	3.80	2.93	2.63	5.07	4.06	4.00	4.12	5.09	(ft/s)		V <sub>el</sub>
			15	35	24	24	24	24	24	24	15	24	15	24	24	36	36	48	48	48	48	(in)	Size	7
			1.36	1.61	3.00	0.41	0.48	0.48	0.49	0.49	4.19	3.21	1.79	2.89	2.92	0.50	0.50	0.50	0.50	0.53	0.55	(%)	Slope	Pipe
	Numt		85.30	85.00	82.18	84.50	84.36	83.73	82.91	82.53	83.40	80.97	80.00	79.00	83.42	82.72	81.46	80.20	79.45	78.23	77.15	( <del>‡</del>	ď	lnv
	Number of lines: 19		85.00	82.72	81.46	84.36	83.73	82.91	82.53	80.97	80.97	80.20	79.00	77.15	82.72	81.46	80.20	79.45	78.23	77.15	76.10	( <del>I</del>	뫄	Invert Elev
	s: 19		87.51		86.76	6 89.67	3 89.60	1 89.03	3   88.23						2 87.08	6 86.88	0 86.09	5 85.08	3 84.85	5 84.27	83.50			
										87.69	86.40	85.52	84.38	84.18								(ft)	두	HGL Elev
			87.49	87.04	86.69	89.65	89.43	88.36	87.94	86.31	86.31	85.36	84.29	84.00	87.04	86.69	85.36	84.89	84.56	84.00	83.12	( <del>‡</del>	Dn	lev
	Run D		89.00	89.00	87.80	89.90	89.90	90.75	93.50	91.53	89.70	88.29	86.33	85.50	88.10	87.80	87.80	88.29	91.00	89.30	86.50	(ft)	Пр	Grnd /
	Run Date: 08-18-2004		89.00	87.80	87.80	89.90	90.75	93.50	91.53	88.29	88.29	88.29	85.50	86.50	87.80	87.80	88.29	91.00	89.30	86.50	0.00	(ŧ)	Dn	Grnd / Rim Elev
	18-200-																				<u></u>			ζ
	+		1-19 to 1-18	1-18 to 1-7	1-17 to 1-6	1-16A to 1-16	1-16 to 1-15	1-15 to 1-14	1-14 to 1-13	1-13 to 1-11	1-12 to 1-11	1-11 to 1-5	1-10 to 1-9	1-9 to 1-2	1-7 to 1-8	1-6 to 1-7	1-5 to 1-6	1-4 to 1-5	1-3 to 1-4	1-2 to 1-3	1-1 to 1-2			Line ID
						6			_	$\sim$														
									, v	in the second	Ĕ													

ENVIRONMENTAL DIVISION PROJECT REVIEW and COMMENTS - TRACKING SUP
Plan Type:   (Concept Plan)   M (Master Plan)   Other, Special:  (Site Plan)   SUP (Special Use Permit)    (Subdivision)   Z (Rezoning)
O EXPEDITED REVIEW STATUS (TOP PRIORITY) O DRC Case REVIEW STATUS
Project Information: Case No.:  Project Name:  Project Name:  WINDSARVEACE MARKETPURCE - OTHARCELS 9, 10 111  Planner:  MATT ARCIER   Extension: 6876  (1° Submission, 1° Plan Review)
Cardised Plan 1 (2 <sup>rd</sup> Submission, 2 <sup>rd</sup> Plan Review)   Slip-Sheet to Env. Div.     Revised Plan 2 (3 <sup>rd</sup> Submission, 3 <sup>rd</sup> Plan Review)   Amendment to Prev. Approved Plan     Revised Plan 3 (4 <sup>rd</sup> Submission, 4 <sup>rd</sup> Plan Review)
Date Tracking: Transmittal Date:  Received Environmental Division: Due / Return Date (Planning):  21 days from Transmittal Date: Erosion & Sediment Control Plan Review Complete: Stormwater Management/Drainage Review Complete: Environmental Division Completion Date:  Date  MAY 20 05 (from Planning)  // NAY 3 05 (Planning Remark)  // NAY 3 05 (EASC Review Complete)  // NAY 6 05 (SWM Review Complete)  /// 6 05 (All Personnel)
Forwarded to Planning  ☐ Email ☐ Fax to Professional  Environmental Review Computer File Setup:
Old Files (Previous Reviews, Old files) File:  Old Files (1" Submission, 1" Review) File:  Revised Plan 1 (2" Submission, 2" Review) File:  Revised Plan 2 (3" Submission, 3rd Review) File:  Revised Plan 3 (4" Submission, 4" Review) File:  3
Erosion & Sediment Control Plan Review (William A. Caim / Mike D. Woolson)  Date Received:  MAY 20 05 (Received for E&SC Plan Review)  Review Complete:  MAY 23 05 (E&SC Plan Review Complete)
Stormwater Management / Drainage Plan Review (Scott J. Thomas)  Date Received:  Review Complete:  MANIZY NOT (Received for SWM Plan Review)  (SWM Plan Review Complete)
Comments: NO LOMMENTS.
77-00-05
Nott.

### **TRANSMITTAL**

DATE:

May 20, 2005

TO:

Environmental\*

Fire JCSA\*

Wayland Bass

VDOT

Scott Whyte Real Estate Police

FROM:

Matthew Arcieri, Senior Planner

**SUBJECT:** 

SP-67-05, WindsorMeade Marketplace - Outparcels 9, 10 & 11

**ITEMS** 

ATTACHED: Plan

Calculations\*

**ACTION:** 

Please review and return comments by June 3, 2005.

Approved DEC 7/11/05

RECEIVED MAY 2 4 2005 Due June 10

**RECEIVED** 

MAY 2 0 2005

ENVIRONMENTAL

DIVISION



### WindsorMeade Marketplace Outparcels 9, 10 and 11

### James City County Environmental

May 18, 2005

5P-67-05

Prepared by:



AES Consulting Engineers
5248 Olde Towne Road. Suite 1
Williamsburg, VA 23188
(757) 253-0040 Fax: (757) 220-8994
http://www.aesva.com



### James City County, Virginia Environmental Division

## **Erosion and Sediment Control and Stormwater Management Design Plan Checklists**

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Issue Date
March 1, 2001

### JAMES CITY COUNTY, VIRGINIA ENVIRONMENTAL DIVISION

### EROSION AND SEDIMENT CONTROL PLAN CHECKLIST

I.		<u>GENERAL</u>	$\underline{L}$ :
Yes	No	N/A	FAMILIARITY with current versions of Chapter 8, Erosion and Sedimentation Control and Chapter 23, Chesapeake Bay Preservation ordinances of the Code of James City County, Virginia and the Virginia Erosion and Sediment Control Handbook (VESCH).
$\boxtimes$			LAND DISTURBING PERMIT AND SILTATION AGREEMENT with surety are required for the project.
			VARIANCE if necessary, requested in writing, for the plan approving authority to waive or modify any of the minimum standards and specifications of the VESCH deemed inappropriate based on site conditions specific to this review case only. Variances which are approved shall be properly documented in the plan and become part of the approved erosion and sediment control plan for the site.
II.		SITE PLA	<u>N</u> :
Yes	No	N/A	VICINITY MAP locating the site in relation to the surrounding area. Include any major landmarks which might assist in physically locating the site.
$\boxtimes$			INDICATE NORTH direction in relation to the site.
$\boxtimes$			LIMITS OF CLEARING AND GRADING for the site including that required for implementation of erosion and sediment controls, stockpile areas and utilities.
$\boxtimes$			DISTURBED AREA ESTIMATES in acres or square feet for the project.
$\boxtimes$			EXISTING TOPOGRAPHY or contours for the site at no more than 5 foot contour interval.
$\boxtimes$			FINAL TOPOGRAPHY, contours or proposed site grading in accordance with the design plan which indicates changes to existing topography and drainage patterns at no more than 2 foot contour interval (or 1 foot contours where required).
$\boxtimes$			EXISTING AND PROPOSED SPOT ELEVATIONS to supplement existing and proposed contours, topography or site grading information. Spot elevations may replace final contours in some instances, especially if terrain is in a low lying area or relatively flat.
		$\boxtimes$	EXISTING VEGETATION including existing tree lines, grassed or unique vegetation areas

Yes	No	N/A 	EXISTING SITE FEATURES including roads, buildings, homes, utilities, streams, fences, structures and other important surface features of the site.
			SOILS MAP with soil symbols, boundaries and legend in accordance with the current Soil Survey of James City and York Counties and the City of Williamsburg, Virginia.
$\boxtimes$			<i>ENVIRONMENTAL INVENTORY</i> in accordance with Section 23-10(2) of the Chesapeake Bay Preservation Ordinance of James City County. Inventory generally includes: tidal shores and wetlands, non-tidal wetlands, resource protection area, hydric soils and slopes steeper than 25 percent. For wetlands, provide a copy of issued permits or satisfactory evidence that appropriate permits are being pursued for the entire project.
			100-YEAR FLOODPLAIN LIMITS or any special flood hazard areas or flood zones based on appropriate Federal Management Agency Flood Insurance Rate Maps (FIRMs) or Flood Hazard Boundary Maps (FHBMs) of James City County, Virginia.
$\boxtimes$			DRAINAGE AREAS for offsite and onsite areas, existing or proposed as applicable. Include drainage divides and directional labels for all subareas at points of interest and size (in acres), weighted runoff coefficient or curve number and times of concentration for each subarea.
		$\boxtimes$	CRITICAL EROSION AREAS which require special consideration or unique erosion and sediment control measures. Refer to the VESCH, Chapter 6 for criteria.
$\boxtimes$			DEVELOPMENT PLAN for the site showing all improvements such as buildings, structures, parking areas, access roadways, above and below ground utilities, stormwater management and drainage facilities, trails or sidewalks, proposed vegetation and landscaping, amenities, etc.
$\boxtimes$			LOCATION OF PRACTICES proposed for erosion and sediment control, tree protection and temporary stormwater management due to land disturbance activities at the site. Use standard abbreviations, labels and symbols consistent for plan views based on minimum standards and specifications in Chapter 3 of the VESCH.
		$\boxtimes$	TEMPORARY STOCKPILE AREAS or staging and equipment storage areas as required for onsite or offsite construction activities or indicate that none are anticipated for this project.
			OFFSITE LAND DISTURBING AREAS including borrow sites, waste areas, utility extensions, etc. and required erosion and sediment controls. If none are anticipated for the project, then indicate on the plans by general or erosion and sediment control notes.
			DETAILS or alternately, appropriate reference to current minimum standards and specifications of the VESCH for each measure proposed for the project. Non-modified, standard duplicated details (silt fence, diversion dikes, etc.) may be referenced to the current version of the VESCH. Specific dimensional or modified standards (basins, traps, outlet protections, check dams, etc.) require presentation on detail sheets. Schedules or tables may be used for multiple site measures such as sediment traps, basins, channels, slope drains, etc. Any modification to standard details should be clearly defined, explained and illustrated.

			MAINTENANCE PLAN or alternately, appropriate reference to current minimum standards and specifications of the VESCH, outlining the inspection frequency and maintenance requirements for all erosion and sediment control measures proposed for the project.
		$\boxtimes$	TRENCH DEWATERING methods and erosion and sediment controls, if anticipated for the project.
$\boxtimes$			CONSTRUCTION SEQUENCE outlining the anticipated sequence for installation of erosion and sediment controls and site, grading and utility work to be performed for the project by the site contractor.
$\boxtimes$			PHASING PLAN if required for larger project sites that are to be developed in stages or phases.
$\boxtimes$			STANDARD COUNTY NOTES are required to be placed on the erosion and sediment control plan. Refer to the standard James City County Erosion and Sediment Control Notes dated May 5, 1999.
$\boxtimes$			PROFESSIONAL SEAL AND SIGNATURE required on final and complete approved plans drawings, technical reports and specifications.
m.		<u>NARRATI</u>	<u>VE</u> :
Yes ⊠	No	N/A	PROJECT DESCRIPTION briefly describing the nature and purpose of the land disturbing activity and the acreage to be disturbed.
C 7	No	<b>N/A</b> □	
	No	N/A	activity and the acreage to be disturbed.  EXISTING SITE CONDITIONS description of existing topography, land use, cover and
	No	N/A □  □  □	activity and the acreage to be disturbed.  EXISTING SITE CONDITIONS description of existing topography, land use, cover and drainage patterns at the site.  ADJACENT AREA descriptions of neighboring onsite or offsite areas such as streams, lakes, property, roads, etc. and potential impacts due to concentrated flow or runoff from
	No □ □ □ □ □		activity and the acreage to be disturbed.  EXISTING SITE CONDITIONS description of existing topography, land use, cover and drainage patterns at the site.  ADJACENT AREA descriptions of neighboring onsite or offsite areas such as streams, lakes, property, roads, etc. and potential impacts due to concentrated flow or runoff from the land disturbing activity.  OFFSITE DISTURBED AREA descriptions of proposed borrow sites, water or surplus

Yes No ⊠ □	N/A	PROPOSED EROSION & SEDIMENT CONTROL MEASURES inclusive to the specific erosion and sediment control plan as proposed for the land disturbing activity. Measures should be consistent with those proposed on the site drawings. Address general use, installation, limitations, sequencing and maintenance requirements for each control measure.
		STABILIZATION MEASURES required for the site, either temporary or permanent, and during and following construction including temporary and permanent seeding and mulching, paving, stone, soil stabilization blankets and matting, sodding, landscaping or special stabilization techniques to be utilized at the site.
		STORMWATER MANAGEMENT CONSIDERATIONS for the site, either of temporary or permanent nature, and strategies, sequences and measures required for control. May reference the stormwater management plan for the site, if prepared, for permanent stormwater management facilities and control of drainage once the site is stabilized.
IV.	<u>CALCULA</u>	ATIONS:
Yes No	N/A ⊠	CALCULATIONS AND COMPUTATIONS associated with hydrology, hydraulics and design of proposed temporary and permanent erosion and sediment control measures including: sediment traps and basins, diversions, stormwater conveyance channels, culverts, slope drains, outlet protections, etc. Computations are not required on the construction plan and may be attached in a supplemental erosion and sediment control plan design report, if presented in a clear and organized format.
		TEMPORARY SEDIMENT BASIN DESIGN DATA SHEET submitted for each basin along with schematic or sketch cross-section showing applicable design and construction data, storage volumes (wet-dry), dimensions and elevations. Peak design runoff to be based on the 2- or 25-year design storm event based on maximum disturbed site conditions (existing, interim or proposed conditions) in accordance with Minimum Standard 3.14 of the VESCH.

### JAMES CITY COUNTY, VIRGINIA ENVIRONMENTAL DIVISION

### STORMWATER MANAGEMENT DESIGN PLAN CHECKLIST

I.	<u>GENERA.</u>	<u>L</u> :
Yes No	• N/A │ □	FAMILIARITY with current versions of the James City County Guidelines for Design and Construction of Stormwater Management BMPs manual; Chapter 8, Erosion and Sediment Control and Chapter 23, Chesapeake Bay Preservation ordinances of the Code of James City County, Virginia; the Virginia Erosion and Sediment Control Handbook (VESCH); and the Virginia Stormwater Management Handbook (VSMH).
		WAIVER OR EXCEPTION if necessary, requested in writing, for the plan approving authority to waive or except the requirements of Chapter 23, Chesapeake Bay Preservation ordinance in accordance with procedure established in Sections 23-14 through 23-17 of the ordinance. Applies to the review case only.
		VARIANCE REQUEST if necessary, requested in writing for the plan approving authority to waive or modify any of the minimum standards and specifications of the VESCH deemed inappropriate based on site conditions specific to this review case only. Variances which are approved shall be properly documented in the plan and become part of the approved erosion and sediment control plan for the site.
		PROFESSIONAL SEAL AND SIGNATURE required on final and complete approved stormwater management plans, drawings, technical reports and specifications.
		WORKSHEET FOR BMP POINT SYSTEM to ensure the stormwater management plan for the project attains at least 10 BMP points (New Development) or traditional pollutant load reduction computations per the Chesapeake Bay Local Assistance Manual (Redevelopment Only)
		PROPOSED CONSERVATION EASEMENT AREAS for any natural open space points claimed in the BMP worksheet.
		INSPECTION/MAINTENANCE AGREEMENT is required to be prepared and executed with the County for the project.
		FEMA FIRM PANEL reference with designated special flood hazard areas or zone designations associated with the site, as applicable.
		DRAINAGE AREA MAP at a maximum scale of 1"=200' scale showing drainage area boundaries for pre- and postdevelopment conditions and associated time of concentration flow paths. Labels to include drainage area size, runoff coefficient or curve number and time of concentration for each subarea shown on the map.

I es No N/A  □ □	SOILS MAP with soil symbols, boundaries and legend in accordance with the current Soil Survey of James City and York Counties and the City of Williamsburg, Virginia with approximate locations of the project site, BMPs and applicable drainage basins.
	STORMWATER MANAGEMENT NARRATIVE in a brief and simple format which describes the project; location; site and drainage basin soil characteristics; receiving water or drainage facility; existing site and drainage basin conditions (topography, land use, cover, slopes, etc.); proposed site development; proposed stormwater management and drainage plan including County BMP type selected; summary of hydrology and hydraulics; maintenance program; and any special assumptions utilized for development of the stormwater management and drainage design plan or computations.
	TEMPORARY STORMWATER MANAGEMENT (if applicable) for control of stormwater runoff encountered during construction activities in addition to measures provided in the erosion and sediment control plan or stormwater management/drainage plan for the site. Adequate protection measures or sequencing provided.
	MODIFICATION PLAN clearly defined for temporary sediment control structures which will be converted to permanent SWM/BMP structures. Includes appropriate hydrologic and hydraulic computations, conversions, sequencing and cleanout information or details. Normally related to primary control structures associated with dry detention or wet retention ponds. Normally not permitted for Group C or D categories such as bioretention, infiltration and filtering system facilities.
	STORMWATER MANAGEMENT and DRAINAGE DESIGN REPORT in a bound 8-1/2 x 11 inch size format. Report shall generally include a title sheet, date, project identification, owner and preparer information, table of contents, narrative, summaries and computations as required. Computations may include: backwater, closed conduit, headwater, hydraulic, hydraulic grade line, hydrology, inlet, open channel, storm sewer, water quality, extended detention or stream channel protection and multi-stage storm routing calculations, as applicable, for the project. Computation data may include hand or computer generated computations, maps or schematics. All information should be presented in a clear, easy to follow format and should closely match construction plan information.
	PLAN VIEW at 1 inch = 50 ft. scale or less (1" = 40', 1" = 30', etc.)  North arrow and plan legend.  Property lines.  Adjacent property information.  Existing site features and existing impervious cover areas.  Impervious cover tabulations.  Existing drainage facilities (natural or manmade)  Existing environmentally sensitive areas (RPA, wetlands, floodplain, steep slopes, critical soils, buffers, etc.)  Existing and proposed contours (1' or 2' contour interval) and spot elevations as necessary to define high and low topography.  Existing and proposed easement locations.

	CTO DAG	Yes No N/A	Proposed site improvements and proposed impervious cover areas.  Proposed stormwater conveyance, drainage and management facilities with appropriate labeled construction data and information.  Proposed landscaping and seeding plans (disturbed areas, pond interior, etc.)  Proposed slope stabilization areas (riprap, blankets, mattings, walls, etc.)  Delineation of permanent pools and the 1-, 2-, 10- and 100-year Design Water Surface Elevations.  Delineation of ponding, headwater, surcharge or backwater areas which may affect adjacent existing or proposed buildings, structures or upstream adjacent properties.  Test boring locations with reference surface elevations (if known).  Risers, barrels, underdrains, overflows and outlet protections.  Emergency spillway level section and outlet channel.  Existing and proposed site utilities and protection measures.  Erosion and sediment control measures (for site or BMP).  Maintenance or access corridors to permanent stormwater management, BMP or drainage facilities.
п.	STORMW.	<u>ATER CONVEYA</u>	NCE SYSTEMS:
Yes No ⊠ □	N/A	PLAN VIEWS  □ □ □ □ □ □ □	Storm drain lengths, sizes, types, classes and slopes for all segments. Label directly on plan or use structure/pipe schedule.  Access structure (inlets, manholes, junctions, etc.) rim elevations, inverts, type and required grate or top unit and lengths labeled.  All structure numbers labeled.  Adequate horizontal clearance from other site utilities or structures.
		provided, ensure a	ally are not required but are encouraged to expedite review. If not all pipe segments have adequate minimum cover, do not exceed of cover for the type/class of pipe specified and do not conflict with other eavation areas.
			Typical storm drain bedding details or reference note.  Standard details or reference note for all proposed access structure types (inlets, manholes, junctions, etc.).  Inlet shaping detail or applicable reference note.  Step detail or applicable reference note (if depth 4 ft. or more).  Typical open channel details with designation, location, shape, type, bottom width, top width, lining, slope, length, side slope, and installation depth required for construction. Channel design data as necessary may also be included.  Outlet protections at all pipe outfalls.

Yes No ⊠ □	N/A	STORMWATER C	Storm Sewer Design computations based on 10-year design event. Hydraulic Grade Line computations based on 10-year design event. Inlet computations based on current VDOT procedure for spread, ponding depth and grate size required.  Culvert Headwater computations. Design based on 10-year design storm event and check only for 100-year storm event.  Open Channel computations based on 2-year design event for velocity and 10-year design event for capacity.  Standard outlet protection or special energy dissipators.  Pipe thickness design computations, as required, for selected pipe type (live load, minimum cover, maximum height of cover, etc.).  Adequate channel computations for receiving channels (based on field measured channel section data).
III.	<u>STORMW.</u>	ATER MANAGEM	MENT/BMP FACILITIES:
Yes No	N/A	management/BMP Under 20 acres, of critical storm are a	an SCS based methodology is required for the design of stormwater facilities with watersheds exceeding 20 acres.  The generally accepted methodologies such as the modified rational, allowable. Refer to Chapter 5 of the VESCH or Chapter 5 of the VSMH.
			Runoff Curve Number or Coefficient determinations: predeveloped and ultimate development land use scenarios.  Time of concentration: predeveloped and ultimate development indicating overland, shallow concentrated, and channel flow components (200 ft. maximum length for overland flow).  Hydrograph generation (tabular or graphical): pre- and postdevelopment conditions for the 1-, 2-, 10- and 100-year design storm events.
		FACILITY CONFI	GURATION and MINIMUM SEPARATIONS  Screening and layout consistent with Section 24-98(d) of the Chapter 24 Zoning ordinance (landscaping, screening, visibility, etc.).  Basic considerations for safety and unauthorized entry.  Proper length to width ratio (Typically 2H:1V).  Facilities with deep pools (4 feet or more in depth) provided with two benches. Fifteen (15) ft. safety bench outward from normal pool at maximum 6 percent slope and aquatic bench inward from normal
			shoreline below normal pool. Narrower widths may be considered on a case-by-case basis.  Pond buffer minimum 25 feet outward from maximum design WSEL. Additional setbacks may be required to permanent structures.  No trees, shrubs or woody plants within 15 feet of embankment toe or 25 feet from principal spillway structure.  Infiltration and filtering system facilities generally located at least 100 feet horizontally from any water supply well; 100 feet from any downslope building; and 25 feet from any upslope buildings, unless site specific investigation allows for reduced separation.

HYDRAULIC COL	Elevation- or Stage-Storage curve and/or tabular data.  Weir / Orifice Control – Extended Detention.  Weir / Orifice Control – riser 1-year control for channel protection.  Weir / Orifice Control – riser 2-year control for quantity (if required).  Weir / Orifice Control – riser 10-year control for quantity (if required).  Inlet / Outlet (barrel) control – (All Storms).  Check for barrel control prior to riser orifice flow to prevent slug flowwater hammer conditions.  Emergency spillway capacity and depth of flow.  Elevation – Discharge (Outlet Rating) curve and/or table. Provide all supporting calculations and/or design assumptions.  Adequate channel computations for receiving channel. May be waived if facility is designed based on current Stream Channel Protection criteria.
POND or RESERV	Storage-Indication Routing of postdeveloped inflow hydrographs for the 1-, 2-, 10-, and 100-year design storms. Preference is for structure to discharge up to the 10-year storm through the principal spillway and pass the 100-year storm with a minimum 1 foot of freeboard through a combination principal and emergency spillways. If no emergency spillway is provided, riser must be large enough to pass the design high water flow and trash without overtopping the facility, have 3 square fee or more of cross-sectional area, contain a hood type inlet and have a minimum freeboard of 2 feet. Token spillways with minimum 8 ft. width are also recommended at or above the design 100-year storm elevation.  Downstream hydrographs at established study points, if conditions warrant (i.e. facility discharge combined with uncontrolled bypass).
MISCELLANEOU  MI	Water quality volume for permanent pool based on selected BMP treatment volume (WQv).  Water quality volume for extended detention base on selected BMP treatment volume (WQv) with drawdown computations.  Drawdown computations for the 1-year, 24 hour detention for stream channel protection criteria.  Pond drain computations (within 24 hours).  Anti-seep collar design (concrete preferred) or match material type.  Filter diaphragm design (or alternative method of controlling seepage).  Riser / base structure flotation analyses. FS = 1.25 minimum.  Downstream danger reach study and/or emergency action plan (if conditions warrant).  Upstream backwater analyses onto offsite adjacent property (if conditions warrant).

Yes No N/A □ □ ⊠	GEOTECHNICAL	REQUIREMENTS Geotechnical Report with recommendations specific to BMP facility type selected. Report prepared by a registered professional engineer.
		Requires submission, review and approval prior to issuance of Land Disturbance Permit.  Initial Feasibility Testing requirements satisfied as per Appendix E of the James City County Guidelines fro Design and Construction of Stormwater Management BMPs manual. (Infiltration, Bioretention and
		Filtering System BMP types only).  Concept Design Testing requirements satisfied as per Appendix E of the James City County Guidelines for Design and Construction of Stormwater Management BMPs manual (Infiltration, Bioretention
		and Filtering System BMP types only).  Minimum Boring locations: borrow area, pool area, principal control structure, top of facility near one abutment and emergency spillway if
		provided.  Boring logs with Unified Soil Classification (ASTM D2487), soils descriptions and depths to bedrock and the seasonal water table
		indicated. Standard County Record Drawing/Construction Certification note provided on plan. Note: It is understood that preparation of record drawings and construction certifications as required for project facilities may not necessarily be performed by the plan preparer. These components may be performed by others.
	PRINCIPAL SPIL	LWAY PROFILE AND ASSOCIATED DETAILS
		EXISTING GROUND AND PROPOSED GRADE

Yes No N/A	CORE TRENCH	Bottom width (4' recommendations) Side slopes (1:1 m	or Geotechnical Report). minimum or greater as dictated by Geotechnial Report). naximum steepness) m or greater as dictated by Geotechnical Report).
	PRINCIPAL CON REQUIRED FOR	ALL ITEMS) Durable, watertight Riser diameter is a All pertinent dime Control orifice or Trash rack – remo Anti-vortex device Riser base structur (concrete preferred Interior access (ste	re with dimensions and embedment specifications d). eps, ladders, etc.) for maintenance for structures over
		exterior access on	excessively high risers may need some form of top portion.  with trash rack device.
	PRINCIPAL CON  □ □	Material (ASTM 0	E OUTLET BARREL C-361 reinforced concrete pipe) with watertight joints. uired for all other pipe material (other RCP types,
		Support and beddi	ng requirements for barrel - concrete cradles, etc. or
		Pipe inverts, lengt	by the Geotechnical Report.  h, size, class and slope shown.  or endwall provided on barrel outlet.
	SEEPAGE CONT	Phreatic line show	n (4:1 slope measured from the intersection of the he principal spillway design high water).
		ANTI-SEEP COLL  Colors  Colors	ARS Anti-seep collar, concrete preferred. Size – 15 percent increase in length of saturation using outside pipe diameter. Spacing and location on barrel (located at least 2 feet from a pipe joint).
		FILTER DIAPHR.	AGMS  Design based on latest NRCS design methods and certified by a professional engineer.

Yes No N/A		
$\boxtimes$ $\square$ $\square$		ND DIMENSIONAL DESIGN DATA
		Top of facility – construction height and settled height (10 percent settlement).
		Crest of principal control structure spillway at least one (1) foot below crest of emergency spillway, if provided.
		Minimum freeboard of one (1) foot above the 100-year design high
		water elevation for facilities <u>with</u> an emergency spillway.  Minimum freeboard of two (2) feet above the 100-year design high
		water elevation for facilities <u>without</u> an emergency spillway or in accordance with the SCS National Engineering Handbook (prior approval required).
		Basin Sediment Clean-Out elevation (permanent mode). Typically 10 to 25 percent of water quality volume.
	CROSS SECTIO	ON THROUGH FACILITY
		Existing Ground.
	# H H	Proposed grade.  Top of facility – constructed and settled.
		Location of emergency spillway with side slopes labeled (emergency
		spillway in cut). Bottom of core trench (4' minimum).
	ППП	Location of each soil boring.
		Barrel location.
		Existing and proposed utility location/protection.
	EMERGENCY S	SPILLWAY PROFILE
		Existing ground.
	HHH	Inlet, level (control) and outlet sections per SCS.  Spillway and crest elevations.
		Spinway and crest elevations.
	pretreatment voito: sediment for	NT DEVICES of adequate depth and properly designed using required lumes for the selected County BMP facility type. Including, but not limited ebays, sediment basins, sumps, grass channels, gravel diaphragms, plunge
	pools, chamber	separators, manufactured systems or other acceptable methods.

X es No N/A	CONSTRUCTION	SPECIFICATIONS and NOTES
	$\boxtimes \square \square$	Anticipated sequence of construction for BMP (consistent with erosion
		and sediment control plan).
		Provisions to control base stream or storm flow conditions encountered
		during construction.
		Site and subgrade preparation requirements.
		Embankment, fill and backfill material soil and placement (lift) thickness requirements.
	$\boxtimes$ $\square$ $\square$	Compaction and soil moisture content requirements.
		Geosynthetics for drainage, filtration, moisture barrier, separation, and
		reinforcement purposes.
		Clay or synthetic (PVC or HDPE) pond liners.
	$\boxtimes$ $\square$ $\square$	Storm drain, underdrain and pipe conduit requirements.
		Minimum depth of pipe cover for temporary (construction) and final
		cover conditions.
	$\boxtimes$ $\square$ $\square$	Permanent shutoff valve and pond drain.
	$\boxtimes$ $\square$ $\square$	Concrete requirements for structural components.
	$\boxtimes$ $\square$ $\square$	Riprap and slope protection.
	$\boxtimes$ $\square$ $\square$	Access or maintenance road surface, base, subbase.
		Temporary and permanent stabilization measures.
		Temporary or permanent safety fencing.
		BMP Landscaping (deep, shallow, fringe, perimeter, etc.)
		Dust and traffic control (if warranted).
		Construction monitoring and certification by professional.
		Other:
		Other:
lacktriangled	<u>MAINTENANCE</u> I	
		Entity responsible for maintenance identified.
	$\boxtimes$ $\square$ $\square$	Maintenance Plan which outlines the long-term schedule for
		inspection/maintenance of the facility and forebays.
		Maintenance access from public right-of-way or publicly traveled road.
		Maintenance easement provided encompassing high water pool and
		buffer, principal and emergency spillways, outlet structures, forebays,
		embankment area and possible sediment-removal stockpile areas.
	$\boxtimes$ $\square$ $\square$	Minimum 6 foot wide public safety shelf (landing) or alternative
		fencing.

### IV. OUTLET PROTECTIONS:

Yes No N/A	
$oxed{oxed}$	Sized for maximum design release (generally 10-year storm).
$\boxtimes$ $\square$ $\square$	Flared end section or endwall.
	Dimensions.
$\boxtimes$ $\square$ $\square$	Rock or riprap size, quantity and placement thickness.
	Slope at 0 percent (Level Grade).
	Geotextiles (nonwoven).
	Special energy dissipators are required for design discharge velocities that
	exceed eighteen (18) feet per second; or if use of standard outlet protection
	would result in velocities exceeding permissible channel velocities; or if
	enace restricts or limits their use

### IV. ADDITIONAL COMMENTS OR INFORMATION SPECIFIC TO THE PLAN:

We provided new computations for the increase in drainage area (0.04 Ac) for the BMP#1 and revisions to Storm sewer system #1. The increase in drainage resulted in the 100 year storm in the basin to increase by a height of 0.01'.

Plan Preparer: <u>BWS</u> Date: <u>4/22/05</u>

Copy of JCC: SWMProg/BMP/Checklist/ChkList

## CALCULATION FOR SCS HYDROGRAPH GENERATION AND CHANNEL PROTECTION FOR SWMP POND #1 WINDSORMEADE MARKETPLACE AES Project No.:9069-02 December 20, 2003 REV: April 25, 2005

PRE-DEVELOPMENT CONDITIONS TO POINT OF CONCERN

A. Pre-Development Drainage Area to Point of Concern =
B. Pre-development Land Use, Soil Classification and Calculation of Composite Curve Number

13.90 Acres

34 minutes

	Soil Type	Soil Hydrologic Group	Post-Development Land Use	Area of Land Use (in Acres)	Curve Number for Land Use (CN)	Adjusted (CN)
1)	20-B	В	woods, good condition	0.21	58.0	12
3)	11-B, 11-C, 14-B, 14-C, 15-D, 15-E, 15-F, 29-A	С	woods, good condition	12.11	72.0	872
4)	11C, 20-B, 34-C	D	wwods, good condition	1.60	79	126
	Total Adjusted CN = Composite CN =			13.92		1,011 <b>73</b>
1)	elopment Time of Concentration Calculations Overland Flow (maximum 300 feet) Surface description (table 5-7) Manning's roughness coefficient., n (table 5-7) Length of overland flow, L 2-year 24-hour rainfall, P2 Average slope of overland flow, s Travel time, Tt = (0.007*(n*L)^0.8)/(P2^0.5*s^0.4)	-)				Woods, Good Cond. 0.4 250 Feet 3.5 inches 0.04 feet per fo 0.54 hours
2)	Shallow concentrated flow (maximum 300 feet) Surface description, paved or unpaved Length of shallow concentrated flow, L Average slope of shallow concentrated flow, s Average velocity, v Travel time, Tt = L/(3600*v)					Wooded, Good Cond 300 Feet 0.03 feet per fo 2.8 feet per se 0.03 hours
3)	Channel or Pipe Flow Length of channel flow, L Average velocity of channel flow, v Travel time, Tt = L/(3600*v)					0 Feet 2.5 feet per se 0.00 hours

20.94 Acres

120

POST-DEVELOPMENT CONDITIONS TO POINT OF CONCERN (for total site and Off-site Contributing Areas)

A. B.

1) 3)

4) 6) 7)

20-B

Post-Development Drainage Area to Point of Concern =
Post-development Land Use, Soil Classification and Calculation of Composite Curve Number

<u>Soil Type</u>	Soil Hydrologic Group	Post-Development Land Use	Area of Land Use (in Acres)	Curve Number for Land Use (CN)	Adjusted (CN)
20-B	С	woods, good condition	1.91	72.0	138
11-B, 11-C, 14-B, 14-C, 15-D, 15-E, 15-F, 29-A, 10-C	Α	commercial	1.28	89.0	114
11C, 20-B, 34-C	В	commercial	0.29	90	26
11-B, 11-C, 14-B, 14-C, 15-D, 15-E, 15-F, 29-A	С	commercial	16.20	94	1,523

commercial

1.26

95

Total Adjusted CN = Composite CN = 20.94 1,920 C.

D

Post-l	Development Time of Concentration Calculations	
1)	Overland Flow (maximum 300 feet)	
	Surface description (table 5-7)	Woods, good condition
	Manning's roughness coefficient., n (table 5-7)	0.4
	Length of overland flow, L	100 Feet
	2-year 24-hour rainfall, P2	3.5 inches
	Average slope of overland flow , s	0.03 feet per foot
	Travel time, $Tt = (0.007^*(n^*L)^0.8)/(P2^0.5^*s^0.4)$	0.29 hours
2)	Shallow concentrated flow (maximum 300 feet)	
	Surface description, paved or unpaved	paved
	Length of shallow concentrated flow, L	115 Feet
	Average slope of shallow concentrated flow, s	0.01 feet per foot
	Average velocity, v	2.00 feet per second
	Travel time, $Tt = L/(3600^*v)$	0.02 hours
3)	Channel or Pipe Flow	
-	Length of channel flow, L	812 Feet
	Average velocity of channel flow, v	5.6 feet per second
	Travel time, Tt = L/(3600*v)	0.04 hours

0.04 hours Total Time of Concentration = 0.35 hours or 21 minutes

### PROPOSED ESTIMATED POND(S) VOLUME

				Inc. Volume	Sum	Sum
		Area	Incremental Volume	(cu. yd.)	Volume	Volume
Elevation	<u>Depth</u>	(sq. ft.)	(cu. ft.)		(cu. ft.)	(cu. yd.)
<u>73</u>	<u>0</u>	<u>6701</u>	<u>o</u>	0	0	0
74	1	12,612	9,657	358	9,657	358
75	1	13,689	13,151	487	22,807	845
76	1	14,799	14,244	528	37,051	1,372
77	1	15,942	15,371	569	52,422	1,942
78	1	22,057	19,000	704	71,421	2,645
79	1	27,489	24,773	918	96,194	3,563
80	1	29,673	28,581	1,059	124,775	4,621
81	1	31,917	30,795	1,141	155,570	5,762
82	· 1	34,224	33,071	1,225	188,641	6,987
83	1	36,580	35,402	1,311	224,043	8,298
84	1	38,898	37,739	1,398	261,782	9,696
85	1	40,842	39,870	1,477	301,652	11,172

### IV. DETERMINING REQUIRED WATER QUALITY VOLUME

Diameter of Release Inlet =

Due to preliminary considerations, it is desired to provide this site extended detention wet pond to achieve a 10 point BMP rating for the facility. Under the James City County guide lines for storm water management BMPs, the extended detention wet pond may have one half of the water quality volume stored in the permanent pool and one half of the water quality volume released in a 24-hour period.

Percent Impervious of the BMP Watershed, Post-Development	76.0%	
Drainage Area of the BMP Watershed	20.94 acres	
Impervious Acres of BMP Watershed	15.92 acres	
Calculation for Water Quality Volume, WQ  WQ <sub>v</sub> = (2.0 inches per impervious acre) *( impervious acres of BMP watershed)  WQv = (2.0 inches) *( 1 ft / 12 inches) * (43560 sq. Ft per acre) * (impervious acres of BMP watershed)	ershed)	
$WQ_v = (2.0 \text{ inches})^* (1 \text{ ft / } 12 \text{ inches})^* (43560 \text{ sq. Ft per acre})^*$	16.80 =	121968 cu. Ft
$WQ_v =$	60984 cu. Ft 60984 cu. Ft	Required Volume for Permanent Pool Design Volume for Dry Storage (1" per Impervious Acre)
$WQ_v$ (provided)=	60984 cu. Ft 124350 cu. Ft 185334	Water Quality Volume Provided for Wet pool Water Quality Volume Provided for Dry pool Total Water quality volume
Elevation of total WQv =	81.9	
Elevation of release inlet for 1/2 water quality volume =	77.5	
Average head, in feet, on release inlet =	2.2	
Average release rate calculation 124,350.0 cubic feet	_	1.4 cfs
(24 hours x 60 minutes/hour x 60 seco	nds/ minute)	1.4 cis
Calculation of size of release inlet for 1/2 Water Quality Volume  Diameter of Release Inlet = 2 * ( Q / ((64.32 * (h / 2)) ^ (1/2) * 0.6 * 3.14))) ^ (1/2)  where, Q equals Average Release Rate, in cfs h equals Average Head, in feet		

Note: A design with an orifice size of 6" will be used for channel protection requirements

0.60

feet, or

8 inches

### AES Project No. 9069 Job Title BMP No. 1

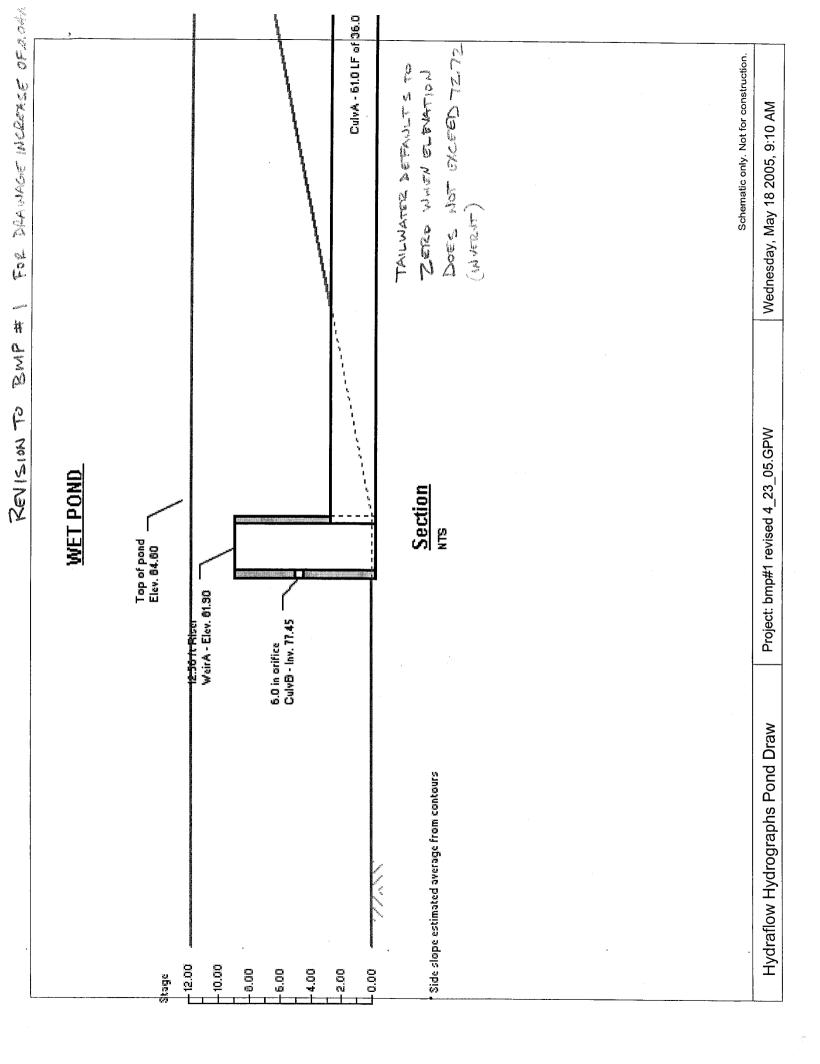
Area=	20.94 Acres	0.0327sq.mi.
CN=	91	
Tc=	0.350 hr.	
P=	2.8 in.	Rainfall depth for 1yr return period
la=	0.198	Initial abstraction is all losses before runoff begins. le surface depressions, water intercepted by vegitation, evaporatation(SeeTR55 Chapter 2, Equation 2-1)
Qu=	630.41 csm/in	Unit Peak Discharge - Peak discharge per square mile per inch of runoff (Units are "cubic square miles per ing
Direct Runoff=	1.9 in.	Runoff in inches (See TR55 Chapter 2, Equation 2-1)
Qi=	38.89 cfs	Peak Inflow Discharge
Qo/Qi=	0.028	Ratio of Peak Inflow Discharge to Peak Outflow Discharge (See TR55 Chapter 6)
Qo=	1.08 cfs	Peak Outflow Discharge (See TR55 Chapter 6) Taken from Maryland Dept. of Stormwater Management Appendix D.11, figured.11.2. The curve for 24hr detention used in Chart 1 was scaled and a curve was fit to the data points. The resulting equation, which appears on the chart yeilds a very good fit.
	0.644 2.117 Ac-Ft 92,232 cu.ft.	Ratio of Volume Stored to Volume Realeased (See TR55 Chapter 6). Value Computed using equation for Figure 6-1 as shown in Appendix F. Required Storage Volume

Average Flow Rate (Qo) 1.08 cfs Average head= 1.55 ft.

Area of orifice= 0.18 sq.ft.

Orifice diameter = 0.48 ft.
Orifice diameter = 5.8 in.

This offers a place to start. After routing the 1yr storm through the oriface check the out put to make sure that the Required Storage Volume is actually detaind for 24 hours. If not adjust the orifice size and recompute.



### **Pond Report**

Hydraflow Hydrographs by Intelisolve

Wednesday, May 18 2005, 9:17 AM

### Pond No. 2 - WET POND

**Pond Data** 

Pond storage is based on known contour areas. Average end area method used.

### Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	73.00	6,701	0	0
1.00	74.00	12,612	9,657	9,657
2.00	75.00	13,689	13,151	22,807
3.00	76.00	14,799	14,244	37,051
4.00	77.00	15,942	15,371	52,422
5.00	78.00	22,057	19,000	71,421
6.00	79.00	27,489	24,773	96,194
7.00	80.00	29,673	28,581	124,775
8.00	81.00	31,917	30,795	155,570
9.00	82.00	34,224	33,071	188,641
10.00	83.00	36,580	35,402	224,043
11.00	84.00	38,898	37,739	261,782
11.80	84.80	40,842	31,896	293,678

Coolerand	1	A-151	Structures
Cuiven	1	UTITICE	Structures

	[A]	[B]	[C]	[D]	
Rise (in)	= 36.00	6.00	0.00	0.00	Crest Len (ft
Span (in)	= 36.00	6.00	0.00	0.00	Crest El. (ft)
No. Barrels	= 1	1	0	0	Weir Coeff.
Invert El. (ft)	= 72.72	77.45	0.00	0.00	Weir Type
Length (ft)	= 61.00	0.00	0.00	0.00	Multi-Stage
Slope (%)	= 1.18	0.00	0.00	0.00	
N-Value	= .013	.013	.000	.000	
Orif. Coeff.	= 0.60	0.60	0.00	0.00	
Multi-Stage	= n/a	Yes	No	No	Exfiltration =

### **Weir Structures**

	[A]	[B]	[C]	[D]
Crest Len (ft)	= 12.56	10.00	0.00	0.00
Crest El. (ft)	= 81.90	82.90	0.00	0.00
Weir Coeff.	= 3.33	3.33	0.00	0.00
Weir Type	= Riser	Ciplti		***
Multi-Stage	= Yes	No	No	No

Exfiltration = 0.000 in/hr (Contour) Tailwater Elev. = 0.00 ft

Note: Culvert/Orifice outflows have been analyzed under inlet and outlet control.

Stage	Storage	/ Discharge	Table
Staue	Storage	Dischalue	Iable

Stage /	Storage /	Discharge	lable									
Stage ft	Storage cuft	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	CIV D cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Total cfs
0.00	0	73.00	0.00	0.00			0.00	0.00				0.00
1.00	9,657	74.00	0.62	0.00			0.00	0.00				0.00
2.00	22,807	75.00	0.62	0.00			0.00	0.00				0.00
3.00	37,051	76.00	0.62	0.00			0.00	0.00				0.00
4.00	52,422	77.00	0.62	0.00			0.00	0.00				0.00
5.00	71,421	78.00	0.62	0.52			0.00	0.00				0.52
6.00	96,194	79.00	1.13	1.08			0.00	0.00				1.08
7.00	124,775	80.00	1.43	1.43			0.00	0.00				1.43
8.00	155,570	81.00	1.76	1.72			0.00	0.00				1.72
9.00	188,641	82.00	3.30	1.96			1.32	0.00				3.28
10.00	224,043	83.00	50.43	2.18			48.25	1.05				51.48
11.00	261,782	84.00	101.65	0.88			100.77	38.42				140.07
11.80	293,678	84.80	108.73	0.58			108.15	87.21			~~~	195.93

### Hydrograph Return Period Recap

yd.	Hydrograph	Inflow		Peak Outflow (cfs)							Hydrograph		
0.	type (origin)	Hyd(s)	1-Yr	2-Yr	3-Yr	5-Yr	10-Yr	10-Yr 25-Yr	50-Yr	100-Yr	description		
	SCS Runoff		7.11	12.21			31.96	37.56		52.98	PRE-DEVELOPMENt		
	SCS Runoff		43.73	57.82			103.74	115.60		147.05	9069POST-DEVELOPMENT		
	Reservoir	2	1.75	3.81			62.45	80.42		121.09	wet pond		
										,			
roi	. file: bmp	#1 revis	sed 4 2	23 05.0	GPW	•	4 , , , ===	-	W	ednesd	lay, May 18 2005, 9:08 /		

### **Hydrograph Summary Report**

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Maximum storage (cuft)	Hydrograph description
1	SCS Runoff	7.11	2	736	36,768				PRE-DEVELOPMENt
2	SCS Runoff	43.73	2	726	152,637				9069POST-DEVELOPMENT
5	Reservoir	1.75	2	902	151,398	2	81.12	159,576	wet pond
							Prenously 81.11		
			·						
							·		
							·		
				-					
								Politica per	
									·
bmr	p#1 revised	d 4_23	_ _05.GP	W	Return	Period: 1	l Year	Wedneso	lay, May 18 2005, 9:08 AM
bmţ	o#1 revised	d 4_23_	_05.GP	W	Return	Period:	l Year	Wedneso	lay, May 18 2005, 9:08 A

Hydraflow Hydrographs by Intelisolve

Wednesday, May 18 2005, 9:32 AM

#### Hyd. No. 2

Storm duration

#### 9069POST-DEVELOPMENT

Hydrograph type = SCS Runoff

Storm frequency = 1 yrs

Drainage area = 20.94 acPREVIOUSLY 2019

= 24 hrs

Basin Slope = 2.0 % Tc method = USER Total precip.

= 2.80 in

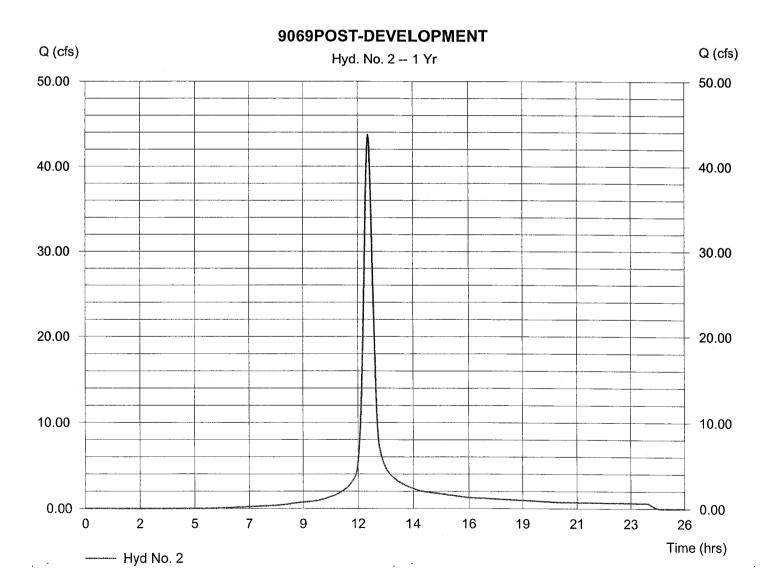
Peak discharge = 43.73 cfs

Time interval = 2 min Curve number = 92

Hydraulic length = 3000 ft Time of conc. (Tc) = 21 min

Distribution = Type II Shape factor = 484

Hydrograph Volume = 152,637 cuft



Hydraflow Hydrographs by Intelisolve

Wednesday, May 18 2005, 9:28 AM

#### Hyd. No. 5

wet pond

Hydrograph type = Reservoir Storm frequency = 1 yrs

Inflow hyd. No. = 2

Reservoir name

= WET POND

Peak discharge

= 1.75 cfs

Time interval

= 2 min

Max. Elevation

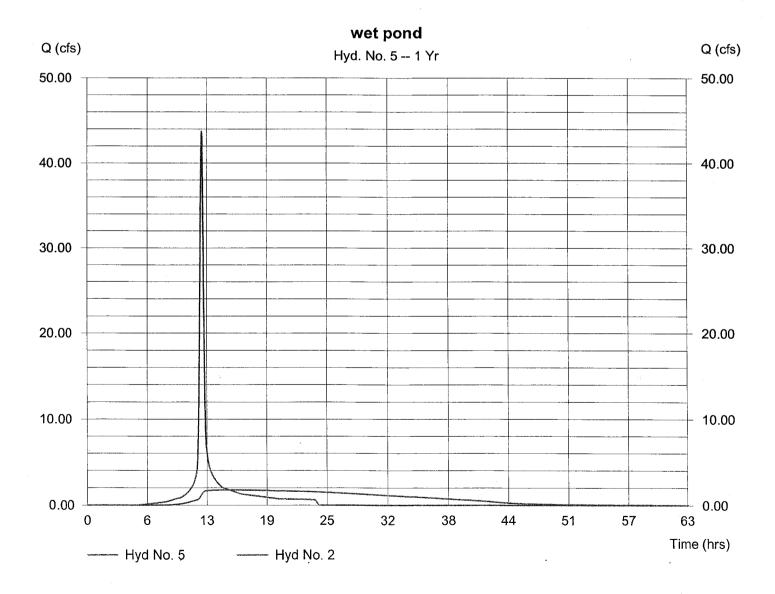
= 81.12 ft

Max. Storage

= 159,576 cuft

Storage Indication method used. Wet pond routing start elevation = 77.40 ft.

Hydrograph Volume = 151,398 cuft



# **Hydrograph Summary Report**

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Maximum storage (cuft)	Hydrograph description
1	SCS Runoff	12.21	2	736	58,844				PRE-DEVELOPMENt
2	SCS Runoff	57.82	2	726	204,004				9069POST-DEVELOPMENT
5	Reservoir	3.81	2	812	202,670	2	82.02	189,404	wet pond
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bmp	o#1 revised	4_23_	05.GP	W	Return	Period: 2	2 Year	Wednesd	ay, May 18 2005, 9:08 AM
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Hydraflow Hydrographs by Intelisolve

Wednesday, May 18 2005, 9:32 AM

#### Hyd. No. 2

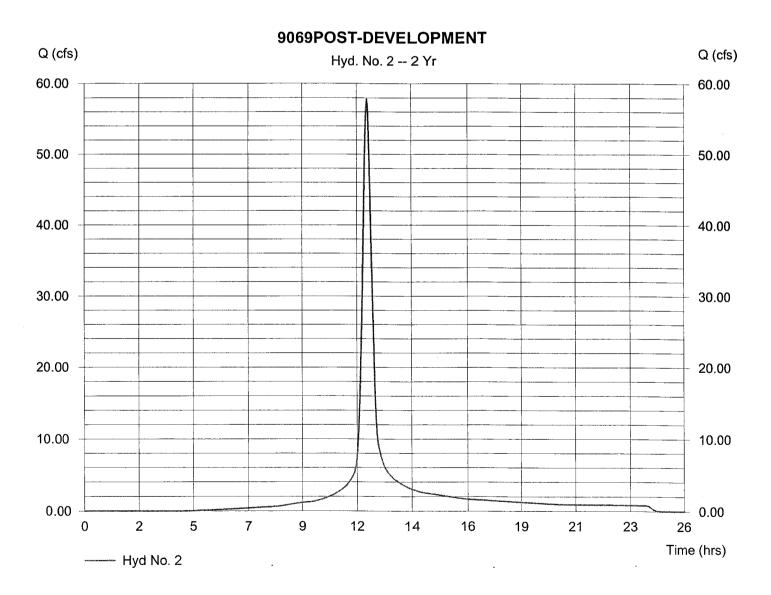
#### 9069POST-DEVELOPMENT

Hydrograph type = SCS Runoff Storm frequency = 2 yrsDrainage area = 20.94 acBasin Slope = 2.0 % Tc method = USER Total precip. = 3.50 inStorm duration

= 24 hrs

Peak discharge = 57.82 cfsTime interval = 2 min Curve number = 92 Hydraulic length = 3000 ftTime of conc. (Tc) = 21 minDistribution = Type II Shape factor = 484

Hydrograph Volume = 204,004 cuft



Hydraflow Hydrographs by Intelisolve

Wednesday, May 18 2005, 9:28 AM

#### Hyd. No. 5

wet pond

Hydrograph type = Reservoir

Storm frequency = 2 yrs Inflow hyd. No. = 2

Reservoir name = WET POND

Peak discharge =

= 3.81 cfs

Time interval

= 2 min

Max. Elevation

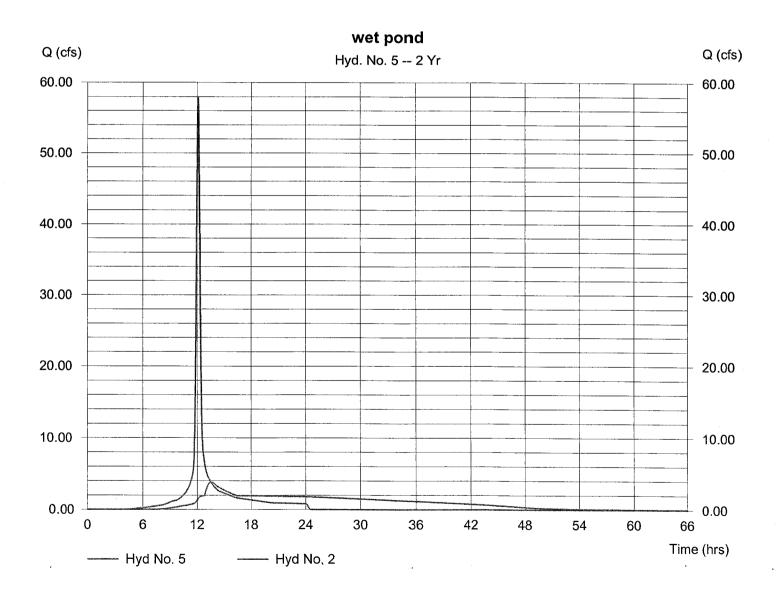
= 2 min = 82.02 ft

Max. Storage

= 189,404 cuft

Storage Indication method used. Wet pond routing start elevation = 77.40 ft.

Hydrograph Volume = 202,670 cuft



# **Hydrograph Summary Report**

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Maximum storage (cuft)	Hydrograph description
1	SCS Runoff	31.96	2	736	145,833				PRE-DEVELOPMENt
2	SCS Runoff	103.74	2	726	377,016				9069POST-DEVELOPMENT
5	Reservoir	62.45	2	738	375,631	2	83.12 No carres	228,727	wet pond
				*					
		•							
					,				
A rock	-								
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Hydraflow Hydrographs by Intelisolve

Wednesday, May 18 2005, 9:32 AM

#### Hyd. No. 2

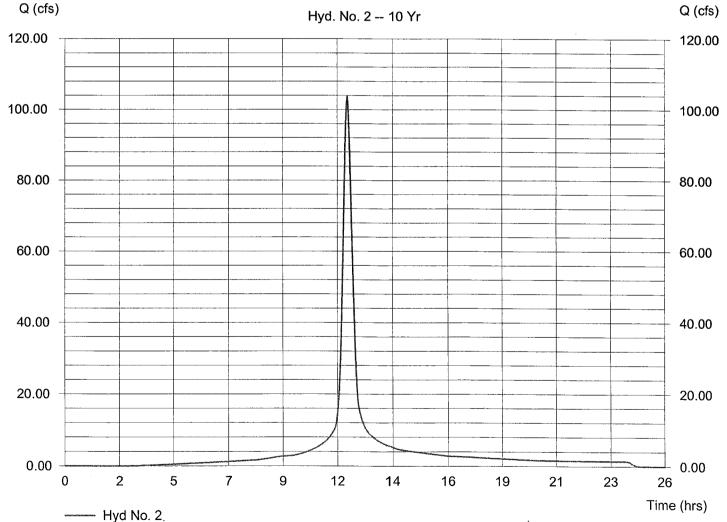
#### 9069POST-DEVELOPMENT

Hydrograph type = SCS Runoff
Storm frequency = 10 yrs
Drainage area = 20.94 ac
Basin Slope = 2.0 %
Tc method = USER
Total precip. = 5.80 in
Storm duration = 24 hrs

Peak discharge = 103.74 cfs
Time interval = 2 min
Curve number = 92
Hydraulic length = 3000 ft
Time of conc. (Tc) = 21 min
Distribution = Type II
Shape factor = 484

Hydrograph Volume = 377,016 cuft

#### 9069POST-DEVELOPMENT



Hydraflow Hydrographs by Intelisolve

Wednesday, May 18 2005, 9:28 AM

#### Hyd. No. 5

wet pond

Hydrograph type = Reservoir Storm frequency = 10 yrs

Inflow hyd. No.

= 2

Reservoir name = WET POND Peak discharge

= 62.45 cfs

Time interval

= 2 min

Max. Elevation

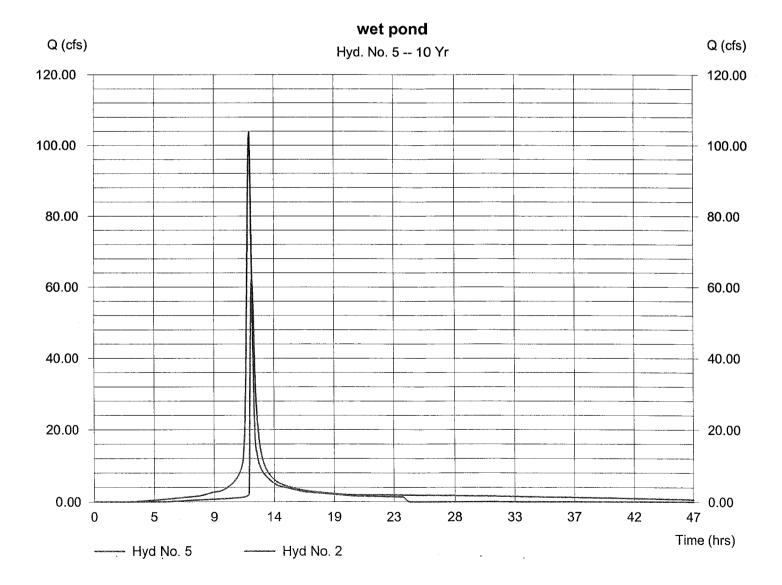
 $= 83.12 \, \mathrm{ft}$ 

Max. Storage

= 228,727 cuft

Storage Indication method used. Wet pond routing start elevation = 77.40 ft.

Hydrograph Volume = 375,631 cuft



# **Hydrograph Summary Report**

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Maximum storage (cuft)	Hydrograph description
1	SCS Runoff	37.56	2	734	170,769				PRE-DEVELOPMENt
2	SCS Runoff	115.60	2	726	422,677				9069POST-DEVELOPMENT
5	Reservoir	80.42	2	736	421,283	2	83.31 PENIOSEY 83,30	235,601	wet pond
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Hydraflow Hydrographs by Intelisolve

Wednesday, May 18 2005, 9:32 AM

#### Hyd. No. 2

#### 9069POST-DEVELOPMENT

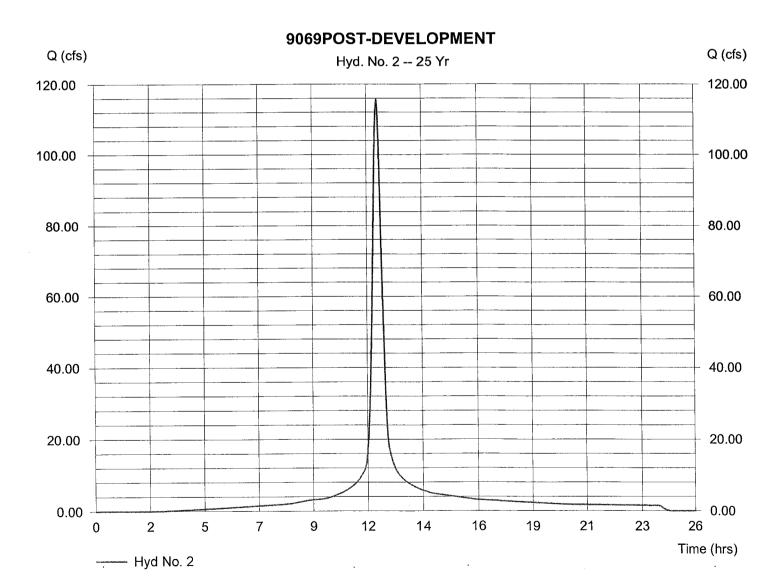
Hydrograph type = SCS Runoff Storm frequency = 25 yrs Drainage area = 20.94 ac Basin Slope = 2.0 % Tc method = USER Total precip. = 6.40 in

Storm duration = 6.40 if

Peak discharge = 115.60 cfs
Time interval = 2 min
Curve number = 92
Hydraulic length = 3000 ft

Time of conc. (Tc) = 21 min Distribution = Type II Shape factor = 484

Hydrograph Volume = 422,677 cuft



Hydraflow Hydrographs by Intelisolve

Wednesday, May 18 2005, 9:28 AM

#### Hyd. No. 5

wet pond

Hydrograph type = Reservoir Storm frequency = 25 yrs

Inflow hyd. No.

= 2

Reservoir name = WET POND

Peak discharge

= 80.42 cfs

Time interval

= 2 min

Max. Elevation

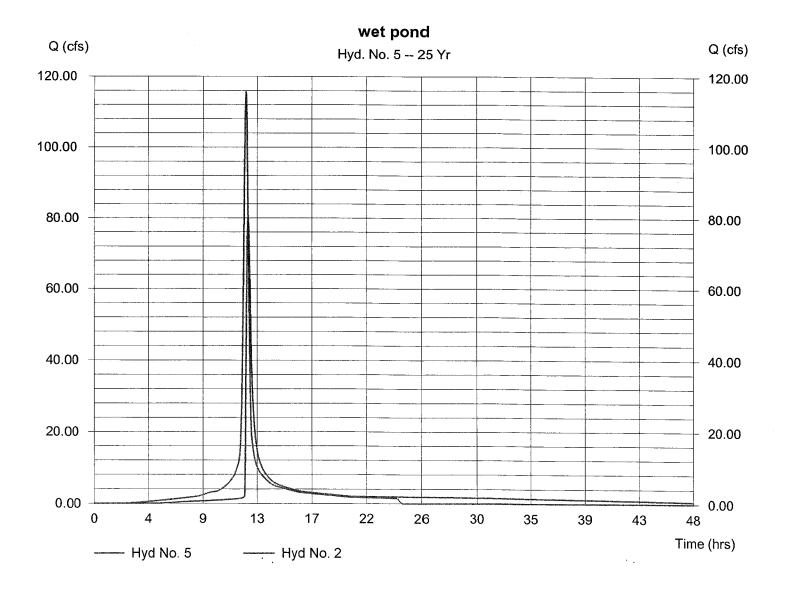
= 83.31 ft

Max. Storage

= 235,601 cuft

Storage Indication method used. Wet pond routing start elevation = 77.40 ft.

Hydrograph Volume = 421,283 cuft



# **Hydrograph Summary Report**

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Maximum storage (cuft)	Hydrograph description
1	SCS Runoff	52.98	2	734	239,937				PRE-DEVELOPMENt
2	SCS Runoff	147.05	2	726	544,951				9069POST-DEVELOPMENT
5	Reservoir	121.09	2	732	543,542	2	83.70	250,592	wet pond
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Hydraflow Hydrographs by Intelisolve

Wednesday, May 18 2005, 9:32 AM

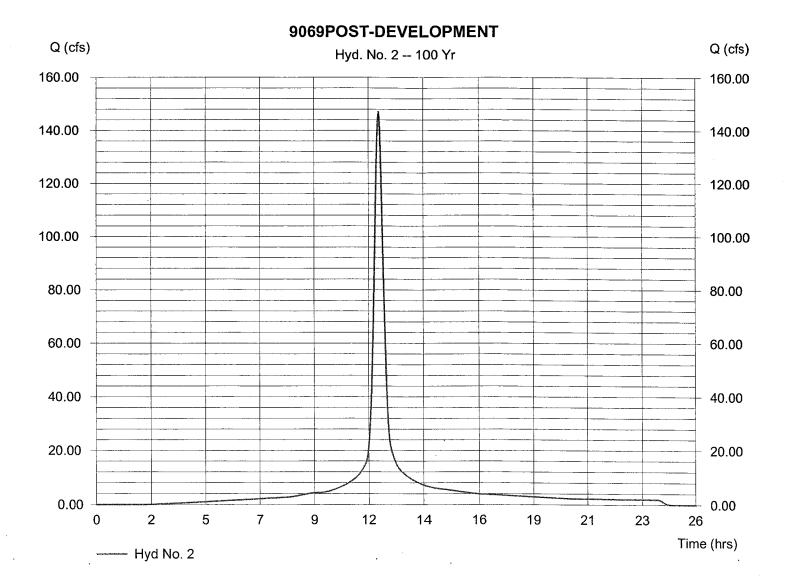
#### Hyd. No. 2

#### 9069POST-DEVELOPMENT

Hydrograph type = SCS Runoff
Storm frequency = 100 yrs
Drainage area = 20.94 ac
Basin Slope = 2.0 %
Tc method = USER
Total precip. = 8.00 in
Storm duration = 24 hrs

Peak discharge = 147.05 cfs
Time interval = 2 min
Curve number = 92
Hydraulic length = 3000 ft
Time of conc. (Tc) = 21 min
Distribution = Type II
Shape factor = 484

Hydrograph Volume = 544,951 cuft



Hydraflow Hydrographs by Intelisolve

Wednesday, May 18 2005, 9:28 AM

#### Hyd. No. 5

wet pond

Hydrograph type = Reservoir Storm frequency = 100 yrs

Inflow hyd. No. = 2

Reservoir name = WET POND

Peak discharge = 12

= 121.09 cfs

Time interval Max. Elevation

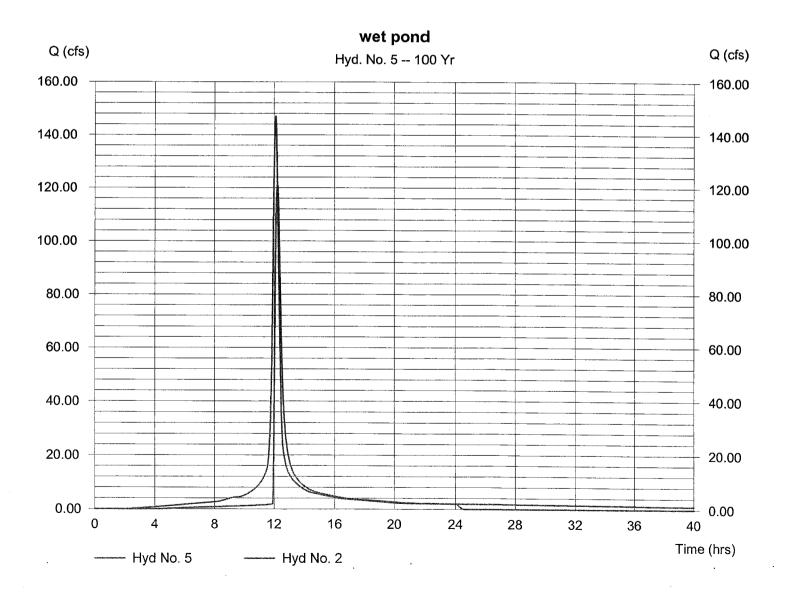
= 2 min

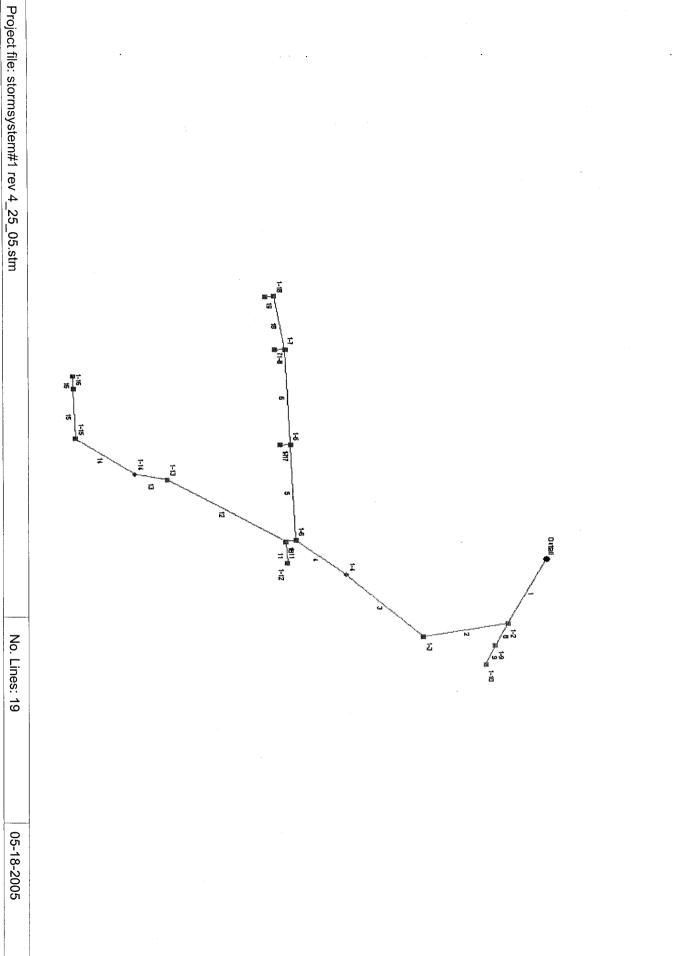
Max. Storage

= 83.70 ft = 250,592 cuft

Storage Indication method used. Wet pond routing start elevation = 77.40 ft.

Hydrograph Volume = 543,542 cuft





# · Storm Sewer Tabulation

Page 1

			1														-					
2005	te: 05-18-2005	Run Date:		19	Number of lines: 19	Numbe										05.stm	4_25	m#1 rev	stormsystem#1	File: stor	Project F	ן פַ
1-19 to 1-18	89.00	89.00	87.49	87.50	85.00	85.30	1.36	15	1.44	7.54	1.76	7.0	5.0	5.0	0.25	0.25	0.70	0.36	0.36	22.0	18	19
1-18 to 1-7	87.80	89.00	87.04	87.35	82.72	85.00	1.61	15	2.45	8.18	3.01	6.9	5.3	5.0	0.43	0.18	0.70	0.62	0.26	142.0	თ	8
1-17 to 1-6	87.80	87.80	86.68	86.75	81.46	82.18	3.00	24	3.93	39.18	12.34	7.0	5.0	5.0	1.76	1.76	0.90	1.96	1.96	24.0	Οī	17
1-16A to 1-16	89.60	89.60	89.50	89.52	84.36	84.50	0.41	24	1.52	14.51	4.78	7.0	5.0	5.0	0.68	0.68	0.90	0.76	0.76	34.0	. 15	16
1-16 to 1-15	90.75	89.60	89.27	89.45	83.73	84.36	0.48	24	3 2.63	15.63	8.26	6.9	5.4	5.0	1.20	0.51	0.90	1.33	0.57	132.0	14	15
1-15 to 1-14	93.50	90.75	88.23	88.91	82.91	83.73	0.48	24	1 4.56	3   15.71	14.33	6.7	6.2	5.0	2.14	0.94	0.90	2.38	1.05	170.0	13	1 4
1-14 to 1-13	91.53	93.50	87.80	88.09	82.53	82.91	0.49	24	9 4.46	2 15.89	14.02	6.5	6.8	0.0	2.14	0.00	0.90	2.38	0.00	77.0	12	13
1-13 to 1-11	88.29	91.53	86.14	87.55	80.97	82.53	0.49	24	7 4.77	9 15.77	14.99	6.5	7.1	5.0	2.31	0.17	0.90	2.57	0.19	321.0	10	12
1-12 to 1-11	88.29	89.70	86.14	86.23	80.97	83.40	4.19	15	2 2.11	13.22	2.59	4.7	18.0	18.0	0.55	0.55	0.90	0.61	0.61	58.0	10	1
1-11 to 1-5	88.29	88.29	85.34	85.50	80.20	80.97	3.21	24	5.85	6 40.51	18.36	4.6	19.0	19.0	3.99	1.13	0.90	4.43	1.25	24.0	4	10
1-10 to 1-9	85.50	86.33	84.28	84.37	79.00	80.00	1.79	15	2.08	8.63	2.55	6.3	8.0	8.0	0.41	0.41	0.90	0.45	0.45	56.0	00	9
1-9 to 1-2	86.50	85.50	83.99	84.17	77.15	79.00	2.89	24	3.80	3 38.45	11.93	5.9	10.0	10.0	2.03	1.62	0.90		1.80	64.0		œ
1-7 to 1-8	87.80	88.10	87.04	87.08	82.72	83.42	2.92	24	3   2.97	38.63	9.32	7.0	5.0	5.0	1.33	1.33	3	1.48	1.48	24.0	တ	7
1-6 to 1-7	87.80	87.80	86.68	86.88	81.46	82.72	0.50	36	3 2.64	7 47.16	18.67	6.7	6.2	5.0	2.79	1.03	0.90	3.24	1.14	252.0	Ŋ	0
1-5 to 1-6	88.29	87.80	85.34	86.07	80.20	81.46	0.50	36	5.09	5 47.16	35.95	ნ ა	7.8	5.0	5.68	1.13	0.90	6.45	1.25	252.0	4	ഗ
1-4 to 1-5	91.00	88.29	84.87	85.06	79.45	80.20	0.50	48	4.07	101.9	51.20	4.6	19.1	4 17.0	11.14	1.47	0.90	12.51	1.63	149.0	ω	4
1-3 to 1-4	89.30	91.00	84.53	84.83	78.23	79.45	0.50	48	4.02	3 101.8	50.46	4.5	19.7	0.0	11.14	0.00	0.90	12.51	0.00	243.0	2	ω
1-2 to 1-3	86.50	89.30	83.99	84.25	77.15	78.23	0.53	48	3 4.13	1 104.8	51.91	4.4	20.7	3 12.0	11.73	0.59	0.90	13.17	0.66	203.0	<u>~</u> `.	Ν
1-1 to 1-2	0.00	86.50	83.12	83.50	76.10	77.15	0.55	48	5.10	3 106.2	64.08	4.3	21.5	5.0	14.75	1.00	0.90	16.53	1.11	192.0	End	_
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												L		-			200#					

Via Hand Delivery

July 26, 2004

Scott J. Thomas, P.E. Senior Engineer Environmental Division James City County 101-E Mounts Bay Road Williamsburg, VA 23187

SP-150-03

Re:

Report of Subsurface Exploration and Geotechnical Engineering Analysis

WindsorMeade Marketplace BMP

Dear Scott:

Pursuant to your request, please find enclosed a copy of the referenced report from ECS, Ltd. dated July 20, 2004. Per your comments on the engineered site plan for the project, you requested a geotechnical study be performed on the BMP. Accordingly, the enclosed analysis should satisfy this site plan requirement.

If you have any questions or comments regarding the above, please feel free to contact me.

Sincerely,

James M. Gresock

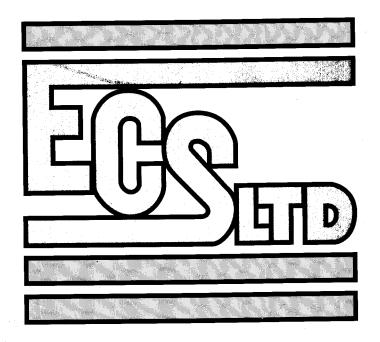
Senior Vice President - Development

JMG:lds

cc

Enclosure - as noted

Arch Marston/AES Consulting Engineers



#### REPORT OF

SUBSURFACE EXPLORATION AND GEOTECHNICAL ENGINEERING ANALYSIS

WINDSORMEADE MARKETPLACE BMP JAMES CITY COUNTY, VIRGINIA

**FOR** 

Mr. James Gresock

July 20, 2004

ECS Project No. 07:6958

Recommended lines of the Recommended lines of the recommendations of the losses.



#### ENGINEERING CONSULTING SERVICES, LTD.

Geotechnical \* Construction Materials \* Environmental

July 20, 2004

Mr. James M. Gresock S.L. Nusbaum Realty Company 9211 Forest Hill Avenue Suite 110 Richmond, Virginia 23235

ECS Project No. 07:6958

Reference:

Subsurface Exploration and Geotechnical Engineering Analysis

Proposed Windsormeade Marketplace BMP

Monticello Avenue

James City County, Virginia

Dear Mr. Gresock,

Engineering Consulting Services, Ltd. has completed a subsurface exploration and engineering evaluation of the above referenced project. This report presents the results of the subsurface exploration and engineering analyses including SWM pond design recommendations. We were provided with a copy of a plan from AES Consulting Engineers illustrating the proposed pond and dam area with proposed and existing topographic lines (elevations).

#### **Introduction:**

The project site is located within the proposed Windsormeade Marketplace in James City County, Virginia. At the time of our site reconnaissance, the site was wooded with heavy undergrowth.

The proposed project will consist of a new BMP (wet pond) and earth dam. The purpose of this exploration was to explore the soil and groundwater conditions at the site and to develop soils-related engineering recommendations to guide design and construction of the planned BMP facility. Our investigation included drilling three (3) soil borings to explore the subsurface soil and groundwater conditions, performing a site reconnaissance to observe general topography, and analyzing field data to develop appropriate geotechnical engineering recommendations regarding the BMP facility construction. A Boring Location Plan is included in Appendix I.

#### Field Exploration Procedures:

Three soil test borings were performed in the proposed BMP location to depths of 15 to 20 feet below existing ground surface. The soil test boring was performed with an ATV drill rig utilizing continuous flight, hollow stem augers to advance the borehole. Drilling slurry fluid was not used in this process.

Representative soil samples were obtained by means of the split-barrel sampling procedure in accordance with ASTM Specification D-1586. In this procedure, a 2-inch outside diameter split-barrel sampler is driven into the soil a distance of 24 inches by a 140-pound hammer falling 30 inches. After a 6-inch seating interval, the number of blows required to drive the sampler through the next 12-inch interval is termed the Standard Penetration Test (SPT) value and is indicated for each sample on the boring log. This value can be used as a qualitative indication of the in-place relative density and relative consistency of non-cohesive soils and cohesive soils, respectively. This indication is qualitative, since many factors can significantly affect the standard penetration resistance value and prevent a direct correlation between drill crews, drill rigs, drilling procedures, and hammer-rod-sampler assemblies.

Field logs of the soils encountered in the borings were maintained by the drill crew. After recovery, each sample was removed from the sampler and visually classified. Representative portions of each sample were sealed in glass jars and delivered to our laboratory in Williamsburg, Virginia, for further visual examination and laboratory testing.

#### **Subsurface Conditions:**

Experienced personnel from our office classified each soil sample in accordance with the Unified Soil Classification System (USCS) and/or the United States Department of Agriculture (USDA) textural classification system, as applicable. Select samples from the test borings were subjected to classification testing to confirm our visual classifications. The group symbols for each soil type are indicated in parentheses following the soil descriptions on the boring logs. The geotechnical engineer grouped the various soil types into the major zones noted on the boring logs. The stratification lines designating the interfaces between earth materials on the boring logs are approximate; in situ, the transitions may be gradual. A brief explanation of the USCS and a Reference Notes for Boring Log sheet is provided in Appendix IV of this report.

Our subsurface exploration and site reconnaissance determined that the surface of the site is generally covered with about 5 to 7 inches of topsoil. Underlying the surficial topsoil, subsurface soils were generally comprised of interbedded deposits of very loose to medium dense Silty and Clayey SAND (SM, SC), and soft to very stiff Sandy CLAYS (CL). The Standard Penetration Test (SPT) N-values recorded within these layers ranged from 2 to 22 blows-per-foot (bpf). Existing ground surface elevations ranged from 72 feett to 90 feet above mean sea level (msl) in the project area.

Groundwater was encountered at each boring location at approximately 6 to 18 feet bgs. Please note that groundwater levels are influenced by seasonal conditions and by periods of significant precipitation or prolonged drought. Due to the clay layers encountered, we expect that areas of perched groundwater will be encountered. Due to the depth of groundwater, it appears that it will be encountered during the proposed pond construction and will likely require groundwater control methods such as well pointing during construction.

#### **Subgrade Preparation and Earthwork Operations:**

The average depth of topsoil recorded in the test borings was about 5 to 7 inches. Stripping of wooded areas typically disturbs the soils to a greater depth due to the presence of root mat which often extends below the bottom of the topsoil. Therefore, for project planning purposes, we recommend a 8-inch stripping depth for this site to remove topsoil and associated organic matter. Isolated areas may require further cuts of an additional 12 inches or more due to tree stumps and heavy root mat from closely spaced trees, etc. The stripping depth should be evaluated at the time of construction by representatives of the Geotechnical Engineer. If the undercuts extend into large areas, the undercut volume could be reduced by the use of geotextiles or geogrids. The use of geosynthetic reinforcement should be evaluated by the geotechnical engineer at the time of construction. Cut and fill operations should extend a minimum of 5 feet beyond the project limits.

After stripping or cutting to the desired grade, and prior to fill placement, subgrades should be observed by the Geotechnical Engineer. Some of the soil subgrades had natural moisture contents which were above the soils' plastic limit. Therefore, soft soil conditions are anticipated after stripping and the contractor may be required to scarify, aerate and re-compact these soils prior to additional fill placement.

Any soft or unsuitable materials encountered, which cannot be stabilized by reworking the soil as discussed above, should be removed and replaced with an approved structural fill. Undercut volumes should be determined by cross-sectioning the area before and after undercut. We have found that calculating undercut volumes by truck counts is less accurate and generally results in additional expense to the owner. In order to minimize undercutting we recommend earthwork operations be performed during the drier times of the year.

We recommend the contract documents include an allowance for undercutting and/or reworking soft near surface soils (if encountered) and replacement with engineered fill. Add/deduct unit prices should also be established so adjustment for the actual volume of undercut can be made.

The Clayey and Silty Sands on the site may be excavated and re-used as structural fill. These soils may be used as fill on the site if they are properly prepared prior to placement. However, significant drying times may be required before the materials could be re-used as compacted fill. Hence these soils may be difficult to reuse without some form of moisture control. All proposed select fill soils for the BMP facility should be submitted to the geotechnical engineer for approval prior to their use on the project. If a fast track schedule is proposed which will not allow

appropriate drying times for wetter soils, imported fill material will be required to supplement some of these more wet soils.

We recommend imported engineered fill (select) material consisting of approved inorganic material classified as CL, SM, SM-SP, SP, SC or better containing less than about 70% by weight Silt or Clay and free of debris. This material should be placed in horizontal lifts not exceeding 8 inches in loose thickness, moisture conditioned to within +/- 3% of the optimum moisture content, and compacted to a minimum of 95% of the maximum dry density obtained in accordance with VTM-1, Standard Proctor method. Select fill slopes should be no greater than 3 horizontal to 1 vertical.

#### Earthen Embankments and Slope Stability:

Based on the provided plan, we understand that an existing low lying area is planned to be utilized as a stormwater management facility for the development. This storm water management pond will require an earth berm about 10 feet high. Based on the planned construction, we recommend an 8-feet wide key trench be constructed to a minimum depth of about 4 feet below the stripped subgrades. The key trench may extend deeper if the underlying soils are not considered suitable for support of the fill at the time of construction. The subgrades should be stripped of all organics and soft soils and be observed by the geotechnical engineer prior to the placement of compacted structural fill.

Two soil test borings were performed in the proposed SWM earthen dam area. The borings were drilled to a depth of about 20 feet below site grades. The soils located within the pond area consisted of predominately Silty and Clayey Sand (SM, SC) with some interbedded Sandy Clay. Only the CLAY soils are considered suitable for reuse as the dam core material. It is not anticipated that materials on site will provide enough materials for the dam core, so additional off-site material will be required to complete the core. Clay core material should classify as Sandy Clay (CL or CH) material. This material should be placed in horizontal lifts not exceeding 8 inches in loose thickness, moisture conditioned to within +-3% of the optimum moisture content, and compacted to a minimum 95% of the maximum dry density obtained in accordance with ASTM Specification D-698, Standard Proctor method. Slopes should be constructed no greater than 3 horizontal to 1 vertical. Also, the side slopes should be seeded to promote vegetation growth and further add to the stability of the slopes.

#### **Infiltration**

We understand the pond area may have up to a 7 ft cut. The sandy soils, at this elevation, are anticipated to have fairly high permeability and classify as Hydrologic Soil Group designation B (infiltration rates of about 0.52 to 1.0 inch/hour). The miscellaneous clay soils encountered will have Hydrologic Soil Group designations of C and D. Typically, soil with the Hydrologic Soil Group designations of A and B are considered to be suitable for Best Management Practices (BMP) that may utilize on-site filtration in their designs. Some soils designated as C type soils are considered suitable for infiltration practices but these soils would need to be evaluated on a case specific basis. Soils with group designations of D are generally not considered suitable for infiltration practices.

It is anticipated that this pond is being designed as wet pond with a planned permanent pool elevation. Due to the permeability rates of these soils, it is anticipated that the water level in the pond will fluctuate as the seasonal groundwater elevation fluctuates and during periods of wet or dry weather. Seepage losses could occur through the pond bottom or side slopes. If it is planned to maintain a permanent pool elevation, construction measures to minimize seepage losses will be necessary. Modification to the side slopes and pond bottom may be necessary in the form of a liner system.

In order to reduce seepage losses through the permeable soils, a liner consisting of lower permeability material may need to be placed on the sand side slopes and pond bottom. We considered three options to line the pond. The method selected should be based on a combination of cost and simplicity of construction. The following are not listed in any particular order of preference:

- Compacted Clay Soil Liner A minimum layer of 12 inches of moderately to highly plastic Clay soils should be placed on the slopes. Prior to the placement of this layer, all topsoil and organics should be removed to suitable natural or compacted fill soils. The on-site clay soils at the project site would be considered suitable for pond liner material. Soils should classify as CL and CH material and should conform to the following specifications: Permeability less than 1 x 10<sup>-6</sup> cm/sec, Plasticity Index not less than 15, Liquid Limit not less than 30, and clay particles not less than 30 percent. These materials should be suitable when compacted with a sheepsfoot compactor at a moisture content slightly above optimum moisture content to at least 95 percent of the Standard Proctor maximum dry density (ASTM D698). We also recommend a 12 inch layer of a suitable protective surface cover be placed on the clay soil liner to act as a buffer during dry months where the soils will tend to desiccate.
- Geocomposite Clay Liner (GCL) After excavation of about 6 inches of the existing topsoil, a GCL such as CETCO Bentomat ST may be placed on the slope. The GCL must be placed in an anchor trench at the top of the slope and then covered with a 12 inch layer of soil. This layer of protective soil could be any type of on-site soil as long as suitable compaction, as referenced above, could be attained.

• Geomembrane Liner - Pond liners are available in a number of materials such as PVC, polypropylene, HDPE, VLDPE and LLDPE. Installation is similar to the GCL in the use of an anchor trench and soil cover. There are materials which can be left exposed, but this might be an aesthetic problem or could be a safety issue as the material could be quite slick. To keep a soil cover from sliding off a smooth plastic liner, a textured liner should be considered. The thinnest textured liners appear to be about 30 mils (such as OxyGrip 30 mil Textured PVC by Occidental Chemical Corp. or Solmax 630T textured VFPE-LDPE by Solmax International). The selection of an appropriate material should be made after discussions with local suppliers to see which materials are readily available at a reasonable cost.

If a liner is planned for the pond the groundwater elevation will need to be lowered to a minimum of 2 feet below the proposed bottom of pond elevation prior to liner placement. Additionally, the water level in the pond, once the liner is placed, should be sufficient to prevent heaving of the liner once the groundwater elevation is allowed to return to its normal seasonal elevation. This can be achieved by re-directing water flow from the well-pointing operation back into the pond excavation once the liner is in place.

#### **Construction Considerations:**

The side slopes of the proposed pond must be properly prepared. All topsoil and organics should be removed to suitable natural soils. Most of the soils as mentioned above are considered suitable for slopes of 3H:1V or more. The slopes should be constructed utilizing engineered fill placed in controlled, horizontal, and compacted lifts that are benched into any existing slopes. On-site sandy or clayey soils are considered suitable for engineered fill to regrade the slopes. This material should be placed in horizontal lifts not exceeding 8 inches in loose thickness, moisture conditioned to within -/-3% of the optimum moisture content, and compacted to a minimum 95% of the maximum dry density obtained in accordance with ASTM Specification D-698, Standard Proctor method. Slopes should be constructed no greater than 3H:1V. Also, the side slopes should be seeded to promote vegetation growth and further add to the stability of the slopes and help to reduce surface sloughing failures.

The subgrade materials are moisture sensitive, and exposure to the environment may weaken the soils at the subgrade level if the excavations remain open for too long a time. If the bearing soils are softened by surface water intrusion or exposure, the softened soils must be removed and replaced by suitable select fill material.

In a dry, re-worked, and compacted state, the soil at the site will provide good subgrade support for fill placement and construction operations; however, when wet, this soil will degrade quickly with disturbance from contractor operations. Good site drainage should be maintained during earthwork operations which would help maintain the integrity of the soil.

Proper compaction control of fill is an important aspect of this project. Therefore, we recommend that all fill operations be observed full-time by a qualified soil technician to determine if minimum compaction requirements are being met.

#### **General Comments:**

This report has been prepared in order to aid in the evaluation of this site and to assist the Contractor, Architect and Engineer in the design and planning of the project. The report scope is limited to the specific project and location described, and the project description represents our understanding of the significant aspects relevant to soil and foundation characteristics.

We have appreciated being of service to you during the design phase of this project and look forward to its successful construction. If you should have any questions regarding the information and recommendations contained in this report or if we can be of any further assistance, please contact our office.

Respectfully,

ENGINEERING CONSULTING SERVICES, LTD

David Gordinier, E.I.T.

Project Engineer

DJG/WLW:kks

Appendix:

I. Boring Location Diagram (1)

II. Soil Test Boring Logs (3)

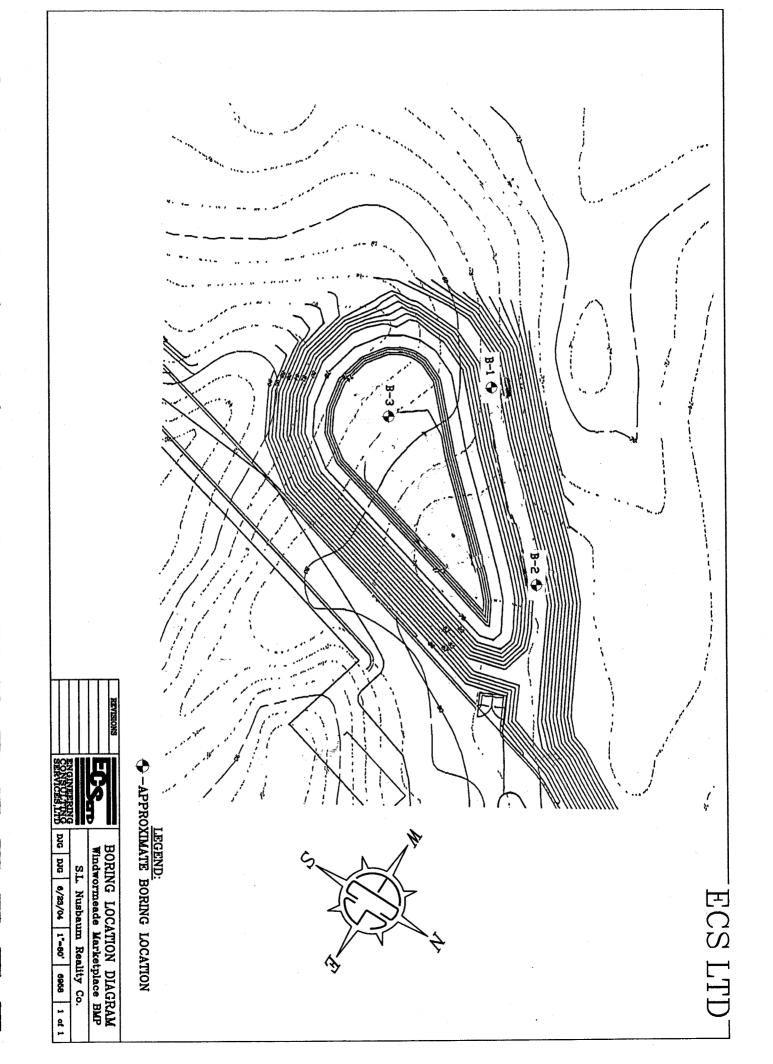
III. Laboratory Test Summary and Results (1)

IV. Unified Soil Classification System/Reference Notes for Boring Logs (2)

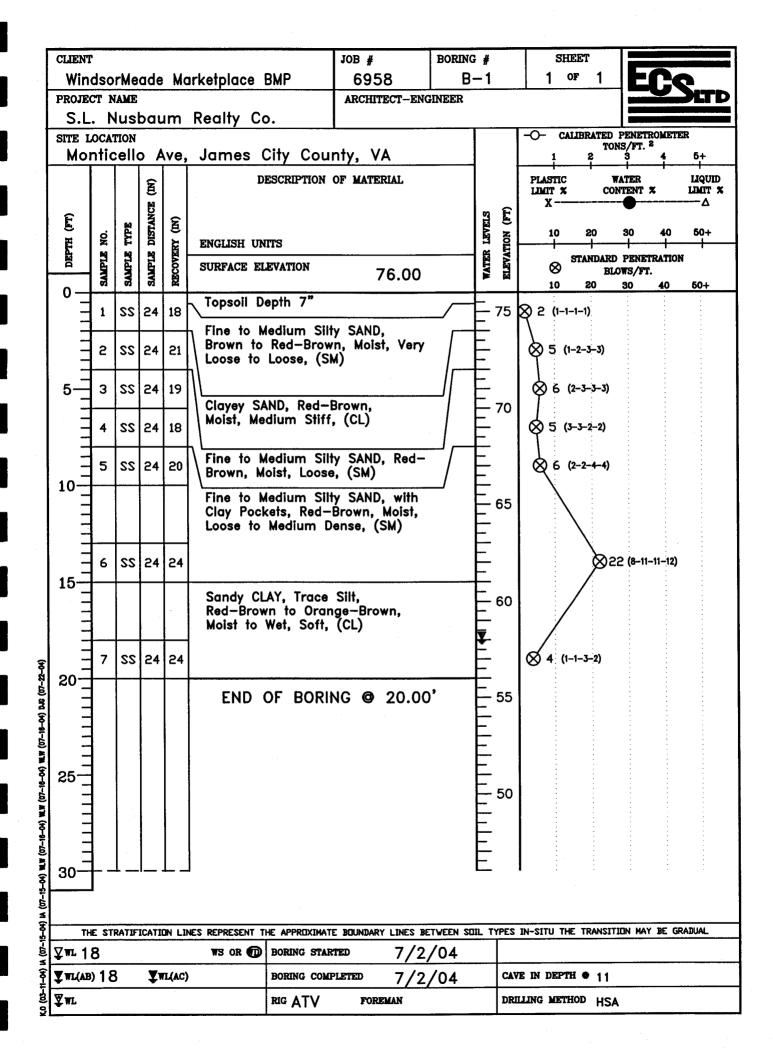
W. Lloyd Ward, P.E. Senior Engineer

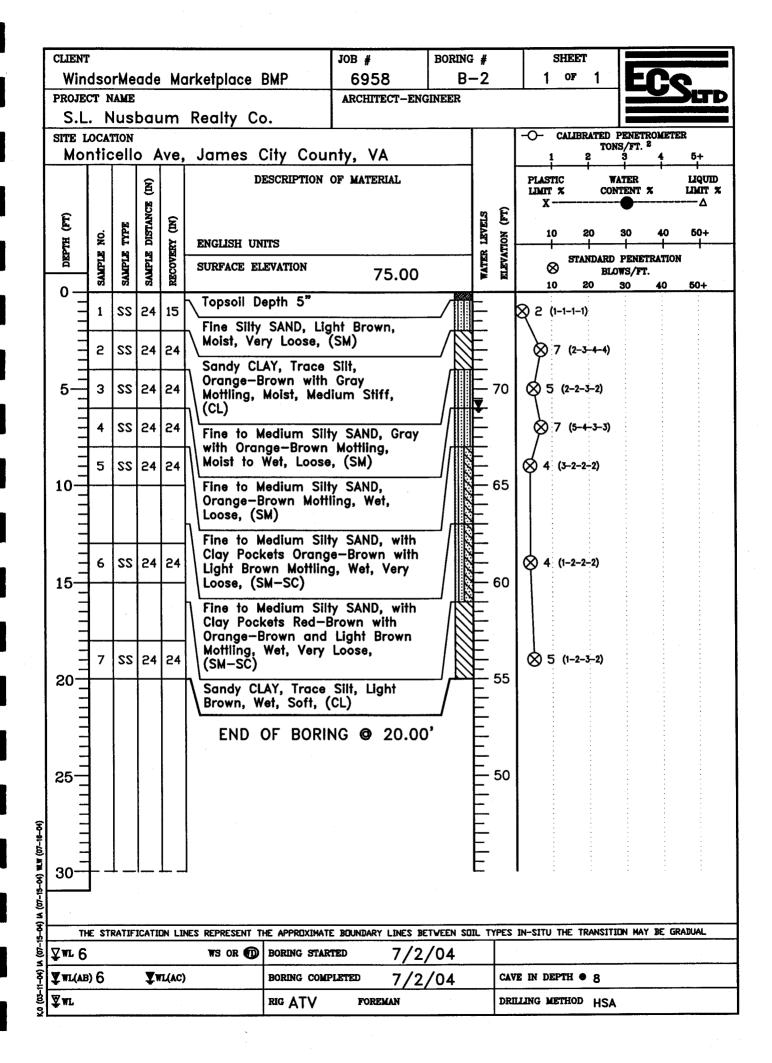
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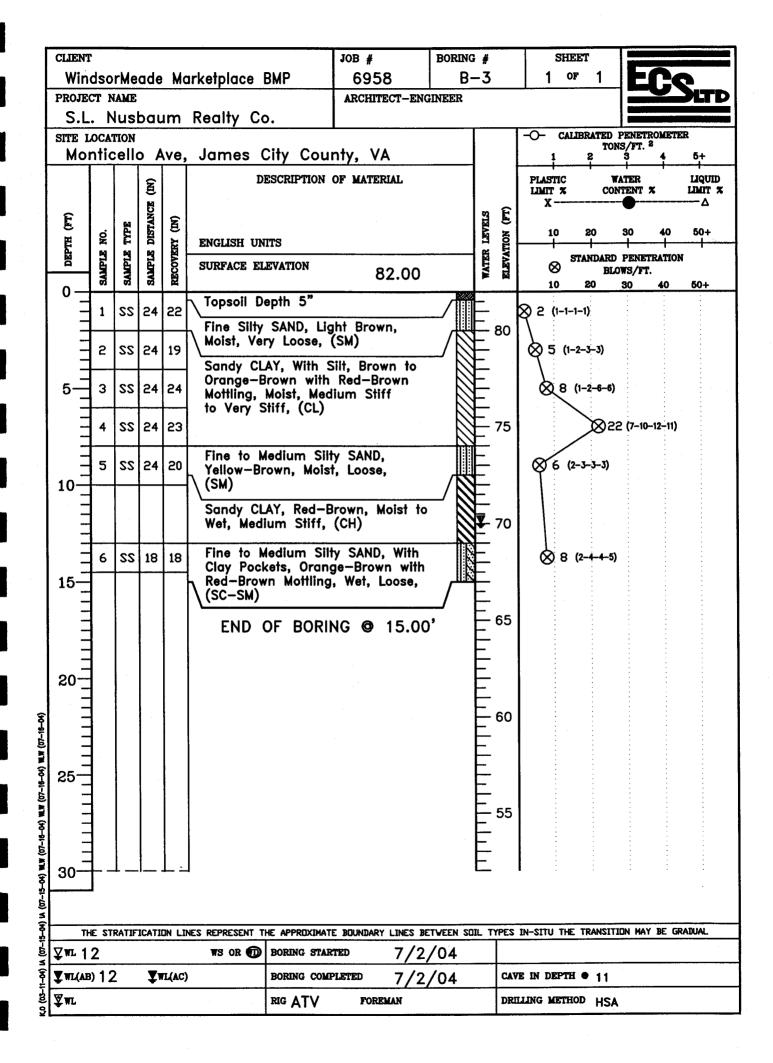
LĽOYD WARD No. 034612 APPENDIX I



APPENDIX II







APPENDIX III

# **Engineering Consulting Services, Ltd.**

**Laboratory Testing Summary** Williamsburg, VA

Date:

07/09/2004

**Project Number:** 6958 Project Name: Windsormeade Marketplace BMP

**Project Engineer:** <u>P</u>G Principal Engine MJG Summary By: IAA

					<u> </u>	
S-2	16	8	57.3	*		*
		24	50.9	*		*
(%)			Sieve	(pcf)	<u> </u>	<u> </u>
USC	Limit Limit	Index	No. 200	Dens	₹	ity   Moisture   Value
Sample Depth Moisture	id Plastic	Plasticity	Passing	Maxim	m	Maximum Optimum CBR
			Percent	ဂ္ဂ	ompa	Compaction

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V = Virginia Test Method S = Standard Proctor M = Modified Proctor

SummarySheet1.xls

DS = Direct Shear Con = Consolidation Hyd = Hydrometer

GS = Specific Gravity

CS = Cement Stabilization

LS = Lime Stabilization UCR = Unconfined Compression Rock UCS = Unconfined Compression Soil

OC = Organic Content SA = See Attached

NP = Non Plastic

\* = Test Not Conducted

Page 1

APPENDIX IV

# UNIFIED SOIL CLASSIFICATION SYSTEM (USCS)

Highly C		50%	Fine-	Greined pesses N	Soils lo. 200 sieve				,	More th	Coars an 50%	e-Crain retained	ed Soils on No.	200 s	ieve			Table
Highly Organic Soils	] 1	ilts and l Liquid l ater tha	imit		Silts and Cl. Liquid lim 50% or les	li		1	CO4	Sands than 50 rse fract No. 4	Son	re	50%	ravels or mor e fract on No.	re of tion	eve	Major division	Unified System of Classification
		1	I			· · ·	·	w	nds flb nes		can nds	w	ivels Ith nes			ean wels		n of Class
7	НО	윤	НЖ	or Or	5		<u> </u>	స	WS	S\$	WS	႙	SK CX	ڎ	3	CW	Group symbols	floation
Peat, muck, and other highly organic soils	Organic clays of medium to high plasticity	Inorganic clays of high plasticity, fat clays	Inorganie silts, micaceous or diatomaceous fine sands or silts, elastic silts	Organic silts and organic silty clays of low plasticity	Inorganic clays of low to modium plasticity, gravelly clays, sandy clays, silty clays, lean clays	sands	Inorganic silts, very fine sands, rock flour, silty or clayey fine	Clayey sands, sand-clay mixtures	Silty sands, sand-silt mixtures	Poorly graded sands and gravelly sands, little or no fines	Well-graded sands and gravelly sands, little or no fines	Clayey gravels, gravel-sand-clay mixtures	Silty gravels, gravel-sand-silt mixtures	gravel-sand mixtures, little or no fines	Poorly graded gravels and	Well-graded gravels and gravel- sand mixtures, little or no fines	Typical names	-
Visual-manual identification, see ASTM Designation D2488.	0 10 20		g	in Equation of A line:		8	More	or plasticity index less than 4	Atterpery limits plot balow "A" line	fication No. No. 200  Co Du x Du between A and Co Du between	200 sieve  C. 1 Dg/D. C. 1  (Dg/D. C. 7	e G1 eve G1 Bo	C.C. in s. Atterberg limits plot below "A" line or plasticity index less than 4	SW, S SM, S class	C iffication of the control of the c	alodar O	Classification criteria	Table " (Continued)

#### REFERENCE NOTES FOR BORING LOGS

#### I. Drilling and Sampling Symbols:

SS - Split Spoon Sampler

DC - Dutch Cone Penetrometer

PM - Pressuremeter

BS - Bulk Sample of Cuttings

ST - Shelby Tube Sampler

PA - Power Auger (no sample)

WS - Wash Sample

RB - Rock Bit Drilling

RC - Rock Core; NX, BX, AX

HSA - Hollow Stem Auger

Standard Penetration Test (SPT) refers to the blows per foot of a 140 lb hammer free falling 30 inches on a in. O.D. split-spoon sampler, as specified in ASTM D-1586. The SPT blow count is commonly referred t as the N-value. Typically the split-spoon sampler is driven to depths of 18 to 24 inches. The SPT result, N value, is commonly determined by summing the second and third 6-inch increments.

#### II. Correlation of Penetration Resistances to Soil Properties:

# COHESIVE SOILS (CLAY, SILT and COMBINATIONS)

# NON-COHESIVE SOILS (SAND, GRAVEL, SILT and COMBINATIONS)

CONSISTENCY	•	UNDRAINED SHEAR STRENGTH C, (PSF)
VERY SOFT	<2	<250
SOFT	3-5	250 - 500
MEDIUM STIFF	6 - 10	500 - 1000
STIFF	11 - 15	1000 - 2000
VERY STIFF	16-30	2000 - 4000
HARD	> 31	> 4000

DENSITY	SPT, N (Blows/Foot)	RELATIVE DENSITY (%)
VERY LOOSE	< 5	0 – 15
LOOSE	6 – 10	16 – 35
MEDIUM DENSE	11 – 80	36 – 65
DENSE	31 – 50	66 – 85
VERY DENSE	51 – 80	86 – 98
EXTREMELY DENSE	> 81	99 - 100

#### [Particle Size Identification]:

• Boulders:

8 inch diameter or more

Cobbles:

3 to 8 inch diameter

• Gravel:

Coarse

1 to 3 inch

Medium

1/2 to 1 inch

Sand:

Fine Coarse

1/4 to 1/2 inch
2.00 mm to 1/4 inch (diameter of pencil lead)

Medium

.42 mm to 2.00 mm (diameter of broom straw)

Fine

.074 mm to .42 mm (diameter of human hair)

#### III. Water Level Measurement Symbols:

WL - Water Level

WS - While Sampling

WD - While Drilling

ACR - After Casing Removal

WCI - Wet Cave In

DCI - Dry Cave In

BCR - Before Casing Removal

The water levels are those water levels actually measured in the borehole at the times indicated by symbol. The measurements are relatively reliable when augering, without adding drilling fluids granular soil. In clays and plastic silts, the accurate determination of water levels may require severy for the water level to stabilize. In such cases additional methods of measurement are generally applied.

# WindsorMeade Marketplace James City County Environmental

Submittal for early land disturbance July 2, 2004

50-150-03 scion

Prepared by:



AES Consulting Engineers 5248 Olde Towne Road. Suite 1 Williamsburg, VA 23188 (757) 253-0040 Fax: (757) 220-8994



614 Moorefield Park Drive Richmond, VA 23236 (804) 330-8040 • Fax (804) 330-9840

July 1, 2004

Mr. Scott Thomas Environmental Division Director James City County P.O. Box 8784, Building E Williamsburg, VA 23187

RE: Case No. SP-150-03. WindsorMeade Marketplace AES Job No. 9069-02

Dear Mr. Thomas:

This letter is a response to the requested changes made by the Environmental Division to the above referenced site plans. Please note that this submittal only includes the changes requested by the Environmental Division. Additional changes addressing other departments' comments will be made in the following submittal. These changes are being submitted in order to obtain a land disturbance permit for the Windsormeade Marketplace Site. Changes or revisions were made to these documents to address the items provided in your letter of May 19, 2004.

### **Environmental:**

### General Comments:

Plan Information. Comment # 9 was not fully addressed. Information shown for Outparcels 1, 2 and 3 on Environmental Inventory Sheet 2 is not consistent with information shown on Sheets 3, 4, 5 and 8. Provide consistent labeling for outparcels on all sheets.

The labeling has been modified on sheet 2 and should now be consistent on all the sheets.

### Erosion & Sediment Control Plan:

Standard E&SC Notes. The standard County erosion and sediment control notes could not be found in the plan set.

Mr. Thomas July 1, 2004 Page 2 of 4

The standard County erosion and sediment control notes were inadvertently omitted from the last submitted plans. Please refer to sheet 12 where these notes have been added.

3/.

Outparcel 4. Ensure that it is clear in Step # 4 of the Phase 2 sequence of construction on Sheet 12 that once Temporary Sediment Basin # 4 (SP-93-03) is removed and the retaining wall is being built that additional downslope erosion and sediment control measures may be necessary to be installed. Additional silt fence and culvert inlet protection measures may be necessary especially if removed following construction of WindsorMeade Way Road. There must be adequate erosion and sediment control measures for land-disturbing activities that occur for the wall following removal of temporary sediment basin # 4.

We have added silt fence to the downstream area per your request. We have also added a note explaining the erosion and sediment control in that area.

4.//

Outlet Protections. Show and label outlet protections at storm drainage outfall structures SS # 2-1 and SS # 1-1 consistent with Minimum Standard & Spec. 3.18 and 3.19 of the VESCH. Show class and thickness of rock, pad dimensions and quantities.

Standard outlet protection has been added to the plans per your request. We have included computations to support the design of these outfalls

Stormwater Management / Drainage:

5. BMP Points. According to the BMP worksheet, it appears that 10 BMP points were achieved for this site, independent of other WindsorMeade at Williamsburg and New Town west projects. In accordance with the stormwater management plan, provide the conservation easement plat as required for the back (north) 6.93 acres which are being taken for Natural Open Space credit (2.69 points). Also, ensure that the 2.05 acres of postdevelopment drainage area to wet pond SWM/BMP #1 (SP-93-03) which is being taken for structural point credit for this project is not double counted for credit associated with future WindsorMeade projects or the New Town west project.

A conservation easement plat will be provided for the area behind the shopping center per your request. Credit for the 2.05 acres of post development drainage area on our project to SWM/BMP #1 (SP-93-03) should only be credited on this project. The original overall SWM masterplan accounted for those 2.05 acres to be included from this project to SWM/BMP #1 (SP-93-03.)

6. Pond Benches. Information on Sheets 9 and 18 for wet pond BMP # 1 does not appear to comply with County BMP manual requirements for aquatic and safety benches. Provide the necessary benches or submit a written request for variance. A variance request must outline information to support granting of a variance to eliminate a bench or to reduce bench widths.

Please see the included written request for variance regarding the pond benches.

7. BMP 1 Hydraulics. Response to previous comment # 25 is acknowledged. A revised "Reservoir Report" could not be found in the revised design report dated April 12, 2004. Provide a new "Reservoir Report" data sheet for BMP # 1 to show input information into the pond's hydraulic model is consistent with your response and information on the plans. (Note: Besides the schematic diagram as provided, a reservoir input report is needed. The reservoir report must show sizes and elevations associated with the low flow orifice, principal spillway, emergency spillway and the pond barrel, consistent with the revised pond design and construction plan.)

A "Reservoir Report" has been included in this submittal package. We have provided a complete report for BMP #1.

8. Storm Design. Explain how storm drainage structure SS # 1-4 can have a drainage area and inlet time of concentration when construction plan Sheet 8 shows SS # 1-4 to be MH-1 structure. The same is true for storm structure SS # 1-13. Explain how this structure can have a drainage area and time of concentration when Sheet 8 shows this to be a MH-1. For the 15-inch pipe segment between storm drainage structure SS # 1-19 and SS # 1-18, computations in the design report show a pipe slope of 1.63 percent; however, Sheet 8 of the plans show slope at 1.36 percent. Ensure computations in the design report are consistent with information shown on the plans.

The computations correctly show no drainage area to the runs connected to these manholes (ex. run 3 is relative to MH4.) The time of concentration has been removed for the runs that have no drainage area. The flow values have not changed. We have corrected the slope of the pipe on the plans per your request.

9. Rock Forebay. Show separation geotextile (between rock and soil) for the forebay in BMP # 1 on the "Forebay Barrier BMP" detail on Sheet 18, consistent with

Mr. Thomas July 1, 2004 Page 4 of 4

### The separartion geotextile has been added to forebay detail per your request.

10. Loading Ramp. It appears the invert out elevation for the 10-inch storm drain from the loading ramp to storm drainage structure SS # 3-2 is incorrect. Using the upstream invert elevation (El. 85.5) and 100 ft. at 1 percent would make the invert out elevation at El. 84.5. Plan information on Sheet 9 shows the invert out at El. 88.5.

### The outfall from the loading dock has been modified.

11. Geotechnical. Previous comment # 32 was not addressed. Response indicates that a geotechnical report is forthcoming to show that existing soils beneath the wet pond are adequate to sustain a permanent pool as intended for a County type A-3 BMP. Land-disturbing cannot be released until this report is received and approved.

### The geotechinical engineer is currently performing field tests to verify this information.

12. Landscaping. Sheet L-1 of the landscape plan must show pond perimeter and bench landscaping and plantings, consistent with the requirements of the County BMP manual and Minimum Standard & Spec. 3.05 of the Virginia Stormwater Management Handbook, for a County type A-3 10 point wet pond.

## Landscaping comments will be addressed on the forthcoming landscaping plans.

I would like to thank you for your assistance in the review of this project. Should any further questions arise, please feel free to contact us.

Sincerely,

**AES Consulting Engineers** 

Bryan W. Stevenson, P.E.

Project Engineer

CC: Chris Johnson, Senior Planner

5248 Olde Towne Road • Suite 1 Williamsburg, VA 23188 (757) 253-0040 • Fax (757) 220-8994



614 Moorefield Park Drive Richmond, VA 23236 (804) 330-8040 • Fax (804) 330-9840

June 3, 2004

Mr. Scott Thomas Environmental Division Director James City County P.O. Box 8784, Building E Williamsburg, Virginia 23187

RE: Windsormeade Marketplace AES Project No. 9069

Dear Mr. Thomas:

AES Consulting Engineers, on behalf of SLN Williamsburg, LLC, respectfully requests an exception from the Director of the Environmental Division for the James City County extended wet pond BMP bench requirements.

A 5 foot aquatic bench has been provided around all of BMP#1. A 15 foot safety bench is provided on the north side of BMP #1. A 7 foot safety bench is provided on the south side of BMP #1. Although this reduced safety bench width is on the shopping center side of the basin, the BMP is located in a low traffic area. Additionally, we have provided guardrail between the shopping center and the south side of the basin. The 12 foot width for the safety and aquatic benches on the south side and the 20 foot width for the benches on the north side of the basins should provide an adequate recovery area for anyone performing maintenance on the BMP. Access to the riser structure is provided on the side with the 20' wide benches.

We appreciate your help with this matter and hope you will not hesitate to call if you have any further questions.

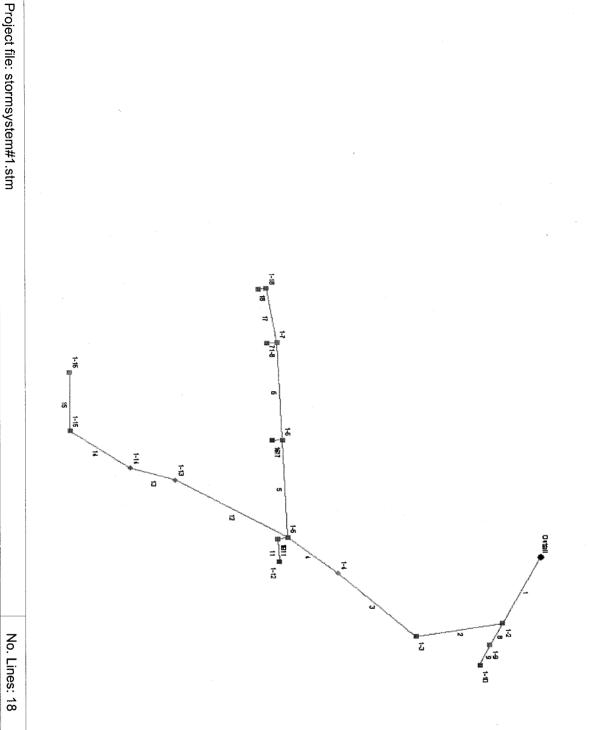
Sincerely,

**AES Consulting Engineers** 

Project Engineer

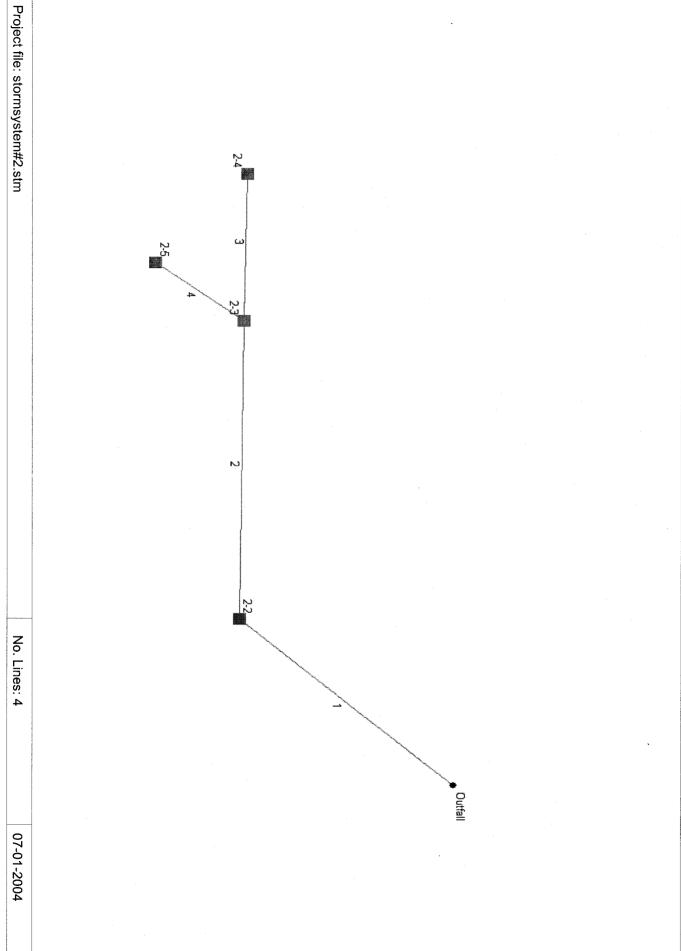
Hydraflow Plan View

REPRINTED TO SHOW NOTIME OF CONCENTRATION AT MANHOLES VOLUMES DID NOT CHANCTE



07-01-2004

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1-19 to 1-18	89.50	89.50	87.57	87.58	85.00	85.30	1.63	15	1.44	8.23	1.76	7.0	5.0	5.0	0.25	0.25	0.70	0.36	0.36	18.5	17	18
1-18 to 1-7	87.50	89.50	87.12	87.43	82.72	85.00	1.61	15	2.45	8.18	3.01	6.9	5.2	5.0	0.43	0.18	0.70	0.62	0.26	142.0	6	17
1-17 to 1-6	87.50	87.50	86.76	86.85	81.46	82.18	3.00	24	8 4.31	39.18	13.54	7.0	5.0	5.0	1.94	1.94	0.90	2.15	2.15	24.0	5	16
1-16 to 1-15	90.75	89.25	88.30	88.64	83.76	84.50	0.49	24	3 3.41	0 15.83	10.70	7.0	5.0	5.0	1.53	1.53	0.90	1.70	1.70	151.0	14	15
1-15 to 1-14	93.50	90.75	87.20	87.89	82.91	83.76	0.50	24	9 4.60	6 15.99	14.46	6.8	5.7	5.0	2.12	0.59	0.90	2.36	0.66	170.0	3	14
1-14 to 1-13	92.40	93.50	86.63	87.06	82.37	82.91	0.50	24	2 4.50	4 15.92	14.14	6.7	6.4	0.0	2.12	0.00	0.90	2.36	0.00	109.0	12	13
1-13 to 1-5	88.00	92.40	85.35	86.49	80.20	82.37	0.72	24	4 4.44	19.24	13.94	6.6	6.8	0.0	2.12	0.00	0.90	2.36	0.00	300.0	4	12
1-12 to 1-11	88.00	89.40	85.52	85.61	80.97	83.40	4.19	5	2 2.11	13.22	2.59	4.7	18.0	18.0	0.55	0.55	0.90	0.61	0.61	58.0	10	<u> </u>
1-11 to 1-5	88.00	88.00	85.35	85.38	80.20	80.97	3.21	24	1 2.45	40.51	7.71	4.6	19.0	19.0	1.67	1.13	0.90	1.86	1.25	24.0	4	10
1-10 to 1-9	85.50	86.50	84.29	84.38	79.00	80.00	1.79	15	2.08	8.63	2.55	6.3	8.0	8.0	0.41	0.41	0.90	0.45	0.45	56.0	00	9
1-9 to 1-2	86.50	85.50	84.00	84.18	77.15	79.00	2.89	24	5 3.80	38.45	11.93	5.9	10.0	10.0	2.03	1.62	0.90	2.25	1.80	64.0	_	œ
1-7 to 1-8	87.50	87.50	87.12	87.16	82.72	83.42	2.92	24	3 2.93	38.63	9.19	7.0	5.0	5.0	1.31	1.31	0.90	1.46	1.46	24.0	တ	7
1-6 to 1-7	87.50	87.50	86.76	86.96	81.46	82.72	0.50	36	6 2.63	8 47.16	18.58	6.7	6.2	5.0	2.77	1.03	0.90	3.22	1.14	252.0	Δi	တ
1-5 to 1-6	88.00	87.50	85.35	86.13	80.20	81.46	0.50	36	6 5.23	6 47.16	36.96	6.3	7.8	5.0	5.83	1.13	0.90	6.62	1.25	252.0	4	Ŋ
1-4 to 1-5	91.00	88.00	84.88	85.07	79.45	80.20	0.50	48	9 4.05	1 101.9	50.91	4.6	19.2	) 17.0	11.10	1.47	0.90	12.47	1.63	149.0	ω	4
1-3 to 1-4	89.25	91.00	84.55	84.85	78.23	79.45	0.50	48	3.99	8 101.8	50.18	4.5	19.8	0.0	11.10	0.00	0.90	12.47	0.00	243.0	N	ω
1-2 to 1-3	86.50	89.25	84.00	84.26	77.15	78.23	0.53	48	8 4.11	3 104.8	51.63	4.4	20.8	12.0	11.69	0.59	0.90	13.13	0.66	203.0		2
1-1 to 1-2	0.00	86.50	83.12	83.50	76.10	77.15	0.55	48	5.08	7   106.2	63.77	4.3	21.6	5.0	14.72	1.00	0.90	16.49	<u>-</u>	192.0	End	_
	(ft)	<b>3</b>	Æ	Æ	3	<b>3</b>	(%)	(in)	(ft/s)	(cfs)	r) (cfs)	in/hr)	(min)	(min)			(C)	(ac)	(ac)	æ		
	Dn	ę	Dn	گ	<u>p</u>	ę	Slope	Size					t Syst	Inlet	Total	Incr		Total	Incr		To	Line
Line ID	im Elev	Grnd / Rim Elev	HGL Elev	НОГ	Invert Elev	Inve	Pipe		<u> </u>	ul Cap	n Total	Rain	7.		Area x C		Rnoff	g Area	Drng	Len	Station	Sta
								-	-		-	-		1		1	-					



# Storm Sewer Tabulation

	TO BE
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	STORM
\	erev.
	7

Page 1

		4	ω	N	<u> </u>			
Proj							Line	Station
Project File: stormsystem#2.stm		N	2		End		- 5 7	g S
e: storn		54.0	80.0	163.0	139.0	∄		Len
nsysten		0.67	0.83	0.39	0.73	(ac)	Incr	Drng Area
າ#2.stm		0.67	0.83	1.89	2.62	(ac)	Total	Area
		0.90	0.90	0.90	0.90	(C)	0	Rnoff
		0.60	0.75	0.35	0.66		Incr	
		0.60	0.75	1.70	2.36		Total	Area x C
		5.0	5.0	5.0	5.0	(min)	Inlet	
-		5.0	5.0	5.8	6.5	(min)	t Syst	T
		7.0	7.0	6.8	6.6	ı) (in/hr)		Rain
		4.22	5.23	11.55	15.59	nr) (cfs)		in Total
		2   18.17	3 20.05	55 20.19	59 64.12	s) (cfs)		al Cap
	,					s) (ft/s)		
		3.44 1	1.66 24	3.68 24	2.21 36		(0	V <sub>el</sub>
		15				(in)	Size S	Pipe
		5.67	0.56	0.57	0.66	(%)	Slope	
Numbe		82.61	80.00	79.55	78.62	<b>æ</b>	Uр	Inver
Number of lines: 4		79.55	79.55	78.62	77.70	Æ	Dn	Invert Elev
4		83.99	83.86	83.56	83.17	( <del>t</del> )	Пр	
					***	=		HGL Elev
		83.82	83.82	83.26	83.12	<b>S</b> .	Dn	ev —
Run		87.75	85.24	87.30	90.12	<b>Æ</b>	η	Grad/
Run Date: 07-01-2004		87.30	87.30	90.12	79.70	( <del>‡</del>	Dn	Grad / Rim Elev
7-01-20							-	
24		2-3 to 2-5	2-3 to 2-4	2-2 to 2-3	2-1 to 2-2			Line ID
		UI	44	ω				₽
]			•	- mwest		L		

NOTES: Intensity = 140.36 / (Inlet time + 19.80) ^ 0.93; Return period = 10 Yrs.

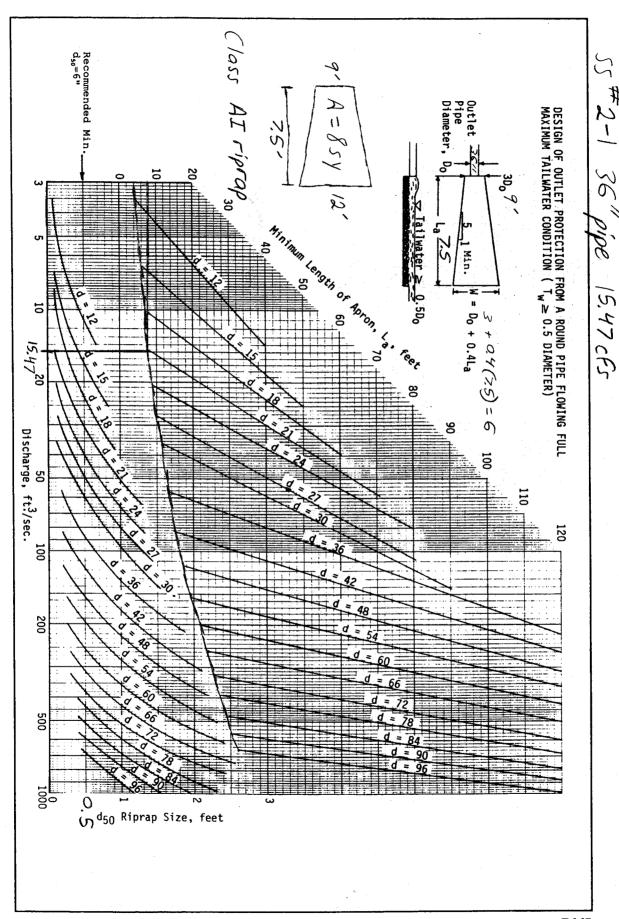


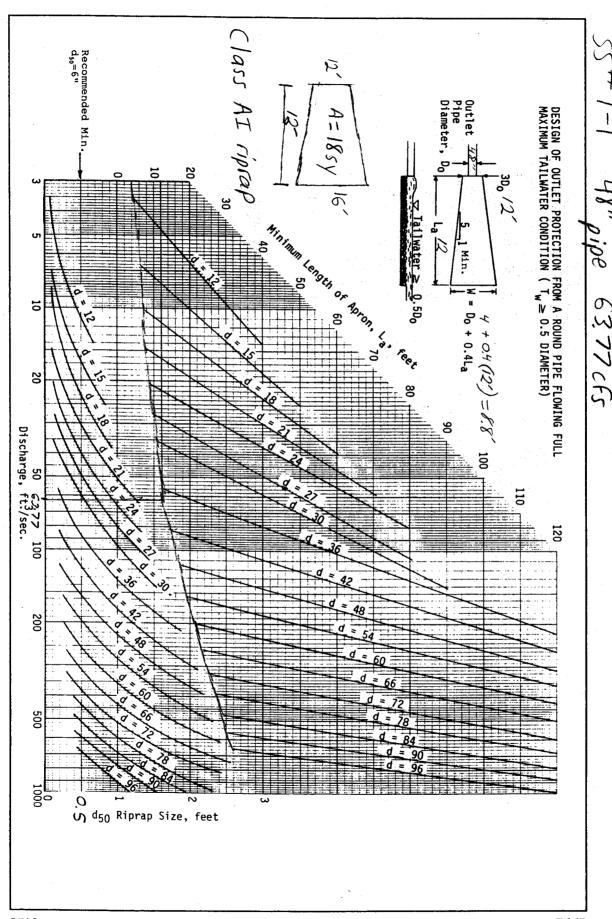
5248 Olde Towne Road, Suite 1 Williamsburg, Virginia 23188 (757) 253-0040 Fax: (757) 220-8994

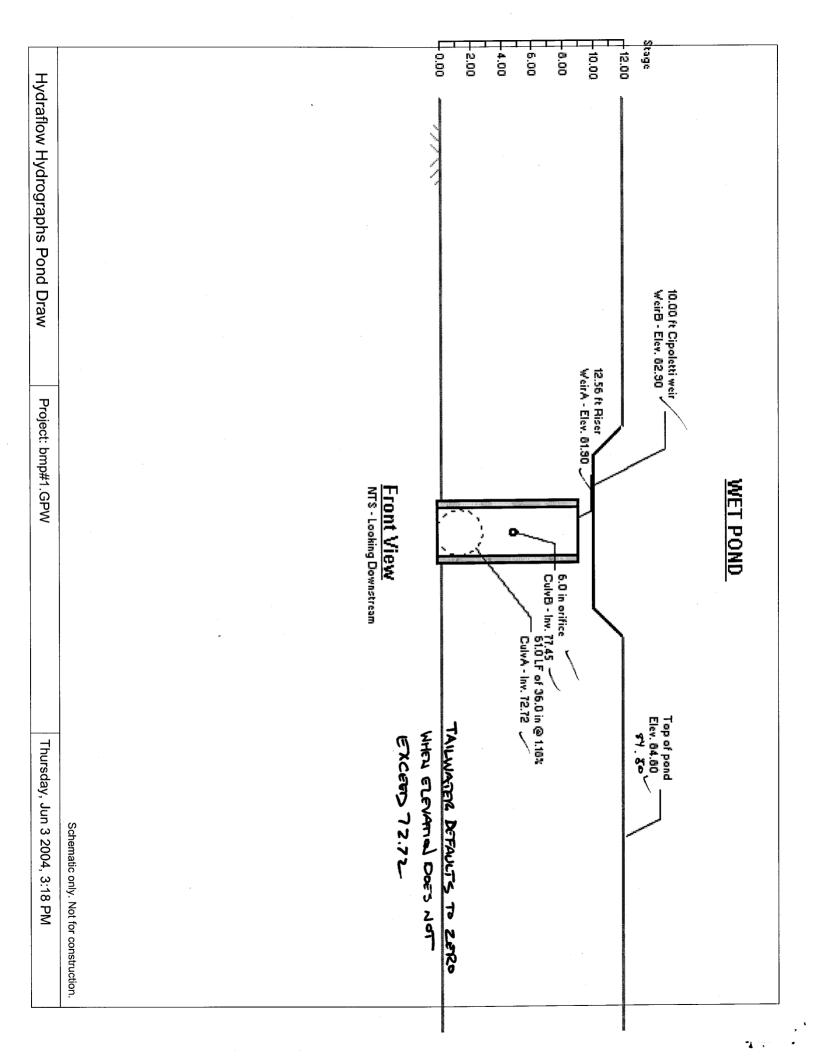
PROJECT WINDSORMEADE MARKETPLACE
PROJECT NO. ####
SUBJECT Spread Calc's
SHEET NO. 1
DATE #####
BY BWS

# STORM WATER INLET COMPUTATIONS

SS2-4	SS	SS2-3	SS2-2	
2-4	SS2-5	2-3	2-2	Number =
DI-2B	DI-2B	DI-2B	DI-2B	Type T
14	10	æ	8	Length
				Station
0.67	0.83	0.39	0.73	Drainage Area (Ac)
0.9	0.9	0.9	0.9	С
0.603	0.747	0.351	0.657	CA
0.603	0.747	0.351	0.657	$\Sigma$ CA
6.4	6.4	6.4	6.4	in/hr
3.859	4.781	2.246	4.205	Q-Inter (CFS)
1.119		0.95		Q Carry- Over (CFS)
9 4.978	0 4.78	1 3.19	0 4.205	Qt Gutter Flow
0.0	0.0	0.0	0.0	S Gutter
+	0.02	_	_	Slope (ft/ft) Sx Cross
0.02 1	22	0.02	0.02	Slope (ft/ft) T(Spread)
1.2	<u> </u>	9.3	10.5	
2 0.1	2	2	2	W (ft)
179	0.182	0.215	0.19	W/T
0.08	0.08	0.08	0.08	Sw (ft/ft)
4	4	4	4	Sw/Sx
0.456	0.51	0.564	0.51	Eo(#10)
0.015	0.015	0.015	0.015	n
2	2	2	2	Local Dep.
3.44	3.44	3.44	3.44	а
0.143	0.143	0.143	0.143	S'w =a/(12W)
0.085	0.093	0.101	0.093	Se (ft/ft) =Sx+SwEo
16.09	15.02	12.09	8 14.23	Lt (ft) 15 P Effec L
0.87	2 0.666	0.662	0.562	L/Lt d (ft)
7 0.975	6 0.861	2 0.858	a	E(#16) h (ft)
5 4.852	4.11	8 2.743	774 3.254	Q Int CFS d/h
0.127	0.665	13 0.454	0.95	Q Carryover
27	8	4	3	Spread
				Remark







### **Pond Report**

Hydraflow Hydrographs by Intelisolve

Thursday, Jun 3 2004, 3:10 PM

### Pond No. 2 - WET POND

### **Pond Data**

Pond storage is based on known contour areas. Average end area method used.

Stage /	Storage	Table
---------	---------	-------

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	73.00 🗸	6.701	0	0
1.00	74.00	12.612	9,657	9,657
2.00	75.00	13,689	13,151	22,807
3.00	76.00	14,799	14,244	37,051
4.00	77.00	15,942	15,371	52,422
5.00	78.00	22,057	19,000	71,421
6.00	79.00	27,489	24,773	96,194
7.00	80.00	29,673	28,581	124,775
8.00	81.00	31,917	30,795	155,570
9.00	82.00	34,224	33,071	188,641
10.00	83.00	36,580	35,402	224,043
11.00	84.00 /	38,898	37,739	261,782
11.80	84.80 🗸	40,842	31,896	293,678

### **Culvert / Orifice Structures**

### **Weir Structures**

	[A]	[B]	[C]	[D]		[A]	[B] /	[C]	[D]
Rise (in)	= 36.00 /	6.00 🗸	0.00	0.00	Crest Len (ft)	= 12.56	10.00	0.00	0.00
Span (in)	= 36.00	6.00	0.00	0.00	Crest El. (ft)	= 81.90	82.90	0.00	0.00
No. Barrels	= 1 ,	1 /	0	0	Weir Coeff.	= 3.33	3.33	0.00	0.00
Invert El. (ft)	= 72.72 /	77.45	0.00	0.00	Weir Type	= Riser	Ciplti		
Length (ft)	= 61.00	0.00	0.00	0.00	Multi-Stage	= Yes	No	No	No
Slope (%)	= 1.18	0.00	0.00	0.00					
N-Value	= .013	.013	.000	.000					
Orif. Coeff.	= 0.60	0.60	0.00	0.00					
Multi-Stage	= n/a	Yes	No	No	Exfiltration = 0	).000 in/hr (Cor	ntour) Tail	water Ele	ev. = 0.00 ft

Note: Culvert/Orifice outflows have been analyzed under inlet and outlet control.

Stage /	Storage /	Discharge	Table				Note: Odivi	STE OTHICC OUT	illows ridve b	con analyzou	ariosi imot ario	outor control.
Stage ft	Storage cuft	Elevation ft	CIv A cfs	Clv B cfs	Clv C cfs	Clv D cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	Total cfs
0.00	0	73.00	0.00	0.00			0.00	0.00				0.00
1.00	9,657	74.00	0.62	0.00			0.00	0.00				0.00
2.00	22,807	75.00	0.62	0.00			0.00	0.00				0.00
3.00	37,051	76.00	0.62	0.00			0.00	0.00				0.00
4.00	52,422	77.00	0.62	0.00			0.00	0.00				0.00
5.00	71,421	78.00	0.62	0.52			0.00	0.00				0.52
6.00	96.194	79.00	1.13	1.08			0.00	0.00				1.08
7.00	124,775	80.00	1.43	1.43			0.00	0.00				1.43
8.00	155.570	81.00	1.76	1.72			0.00	0.00				1.72
9.00	188.641	82.00	3.30	1.96			1.32	0.00				3.28
10.00	224.043	83.00	50.43	2.18			48.25	1.05				51.48
11.00	261,782	84.00	101.65	0.88			100.77	38.42				140.07
11.80	293,678	84.80	108.73	0.58			108.15	87.21				195.93

### Hydrograph Return Period Recap

lyd.		Inflow				Peak Out	flow (cfs)			,	Hydrograph description
о.	type (origin)	Hyd(s)	1-Yr	2-Yr	3-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr	description
	SCS Runoff		7.11	12.21	/		31.96	37.56 <b>/</b>		52.98	PRE-DEVELOPMENt
	SCS Runoff		43.64	57.71			103.54	115.38		146.77	9069POST-DEVELOPMENT
	Reservoir	2	1.75	3.76			62.16	80.12		120.86	wet pond
											·
							:				
							:				
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									<u> </u>		

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Maximum storage (cuft)	Hydrograph description
1	SCS Runoff	7.11	2	736	36,768			<del></del>	PRE-DEVELOPMENt
2	SCS Runoff	43.64	2	726	152,346				9069POST-DEVELOPMENT
5	Reservoir	1.75	2	902	151,107	2	81.11	159,368	wet pond
					·				
	#1.GPW			-	Poturn	Period: 1	Voor	Thursday	/, Jun 3 2004, 3:16 PM

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Maximum storage (cuft)	Hydrograph description
1	SCS Runoff	12.21	2	736	58,844				PRE-DEVELOPMENt
2	SCS Runoff	57.71	2	726	203,614				9069POST-DEVELOPMENT
5	Reservoir	3.76	2	812	202,281	2	82.02	189,333	wet pond
	-								
									·
	`								
	-								·
								·	
bmp	#1.GPW				Return	Period: 2	2 Year	Thursday	, Jun 3 2004, 3:16 PM

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Maximum storage (cuft)	Hydrograph description
1	SCS Runoff	31.96	2	736	145,833				PRE-DEVELOPMENt
2	SCS Runoff	103.54	2	726	376,296				9069POST-DEVELOPMENT
5	Reservoir	62.16	2	738	374,911	2	83.12	228,612	wet pond
	}								
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	-								
		;						·	
The second									
bmp	#1.GPW				Return I	Period: 1	0 Year	Thursday	Jun 3 2004, 3:16 PM
<u> </u>									Hydraflow Hydrographs by Intelisative

	erval peak nin) (min)	(cuft)	hyd(s)	elevation (ft)	storage (cuft)	Hydrograph description
1 SCS Runoff 37.56	2 734	170,769				PRE-DEVELOPMENt
2 SCS Runoff 115.38	2 726	421,869		<del></del>		9069POST-DEVELOPMENT
5 Reservoir 80.12	2 736	420,475	2	83.30	235,493	wet pond
		•				
						· · · · · · · · · · · · · · · · · · ·
	-					
bmp#1.GPW	<u> </u>	Return	Period: 2	5 Year	Thursday	, Jun 3 2004, 3:16 PM

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Maximum storage (cuft)	Hydrograph description
1	SCS Runoff	52.98	2	734	239,937				PRE-DEVELOPMENt
2	SCS Runoff	146.77	2	726	543,909		·		9069POST-DEVELOPMENT
5	Reservoir	120.86	2	732	542,501	2	83.70 0.H.W	250,461	wet pond
	,					-	<b>)</b> .n·		
							22.20		·
	:						Transition of the state of the		
bmp	#1.GPW				Return	Period: 1	100 Year	Thursday	, Jun 3 2004, 3:16 PM

# Windsormeade Marketplace James City County Environmental

April 12, 2004

SP-150-03

Prepared by:



AES Consulting Engineers 5248 Olde Towne Road. Suite 1 Williamsburg, VA 23188 (757) 253-0040 Fax: (757) 220-8994 http://www.aesva.com

# CALCULATION FOR SCS HYDROGRAPH GENERATION AND CHANNEL PROTECTION FOR SWMP POND #1 WINDSORMEADE MARKETPLACE AES Project No.:9069-02 December 20, 2003 REV: February 16, 2004

# PRE-DEVELOPMENT CONDITIONS TO POINT OF CONCERN A. Pre-Development Drainage Area to Point of Concern = B. Pre-development Land Use, Soil Classification and Calculation of Composite Curve Number

13.90 Acres

		<u>Soil Type</u>	Soil Hydrologic Group	Post-Development Land Use	Area of Land Use (in Acres)	Curve Number for Land Use (CN)	Adjusted (CN)
	1)	20-В	В	woods, good condition	0.21	58.0	12
	3)	11-B, 11-C, 14-B, 14-C, 15-D, 15-E, 15-F, 29-A	С	woods, good condition	12.11	72.0	872
	4)	11C, 20-B, 34-C	D	wwods, good condition	1.60	79	126
		Total Adjusted CN = Composite CN =			13.92		1,011 73
C.		evelopment Time of Concentration Calculations					
	1)	Overland Flow (maximum 300 feet) Surface description (table 5-7) Manning's roughness coefficient., n (table 5-7) Length of overland flow, L 2-year 24-hour rainfall, P2 Average slope of overland flow, s Travel time, Tt = (0.007*(n*L)^0.8)/(P2^0.5*s^0.	4)				Woods, Good Cond. 0.4 250 Feet 3.5 inches 0.04 feet per foot 0.54 hours
	2)	Shallow concentrated flow (maximum 300 feet) Surface description, paved or unpaved Length of shallow concentrated flow, L Average slope of shallow concentrated flow, s Average velocity, v Travel time, Tt = L/(3600°v)					Wooded, Good Cond. 300 Feet 0.03 feet per foot 2.8 feet per second 0.03 hours
	3)	Channel or Pipe Flow Length of channel flow, L Average velocity of channel flow, v Travel time, Tt = L/(3600°v)					0 Feet 2.5 feet per second 0.00 hours
		Total Time of Concentration =				or	0.57 hours 34 minutes

# POST-DEVELOPMENT CONDITIONS TO POINT OF CONCERN (for total site and Off-site Contributing Areas) A. Post-Development Drainage Area to Point of Concern = B. Post-development Land Use, Soil Classification and Calculation of Composite Curve Number

20.90 Acres

		Soil Type	Soil Hydrologic Group	Post-Development Land Use	Area of Land Use (in Acres)	Curve Number for Land Use (CN)	Adjusted (CN)	
	1)	20-B	С	woods, good condition	1.91	72.0	138	$\omega$
	3)	11-B, 11-C, 14-B, 14-C, 15-D, 15-E, 15-F, 29-A	Α	commercial	1.20	89.0	107	15.3 ACM.
	4)	11C, 20-B, 34-C	В	commercial	0.29	90	26	· .m/1
	6)	11-B, 11-C, 14-B, 14-C, 15-D, 15-E, 15-F, 29-A	С	commercial	16.20	94	1,523	1.4
	7)	20-B	D	commercial	1.26	95	120	
		Total Adjusted CN = Composite CN =		· ·	20.86		1,913 <b>92</b>	<del></del>
C.	Post-De	evelopment Time of Concentration Calculations						
	1)	Overland Flow (maximum 300 feet) Surface description (table 5-7) Manning's roughness coefficient., n (table 5-7) Length of overland flow, L 2-year 24-hour rainfall, P2 Average slope of overland flow, s Travel time, Tt = (0.007*(n*L)^0.8)/(P2^0.5*s^0.	.4)				Woods good co 0.4 100 Feet 3.5 inche 0.03 feet p 0.29 hours	es per foot
	2)	Shallow concentrated flow (maximum 300 feet) Surface description, paved or unpaved Length of shallow concentrated flow, L Average slope of shallow concentrated flow, s Average velocity, v Travel time, Tt = L/(3600*v)					paved 115 Feet 0.01 feet p 2.00 feet p 0.02 hours	per foot per second
	3)	Channel or Pipe Flow Length of channel flow, L Average velocity of channel flow, v Travel time, Tt = L/(3600°v)					812 Feet 5.6 feet p 0.04 hours	per second

Total Time of Concentration =

0.35 hours

or

21 minutes

### III. PROPOSED ESTIMATED POND(S) VOLUME

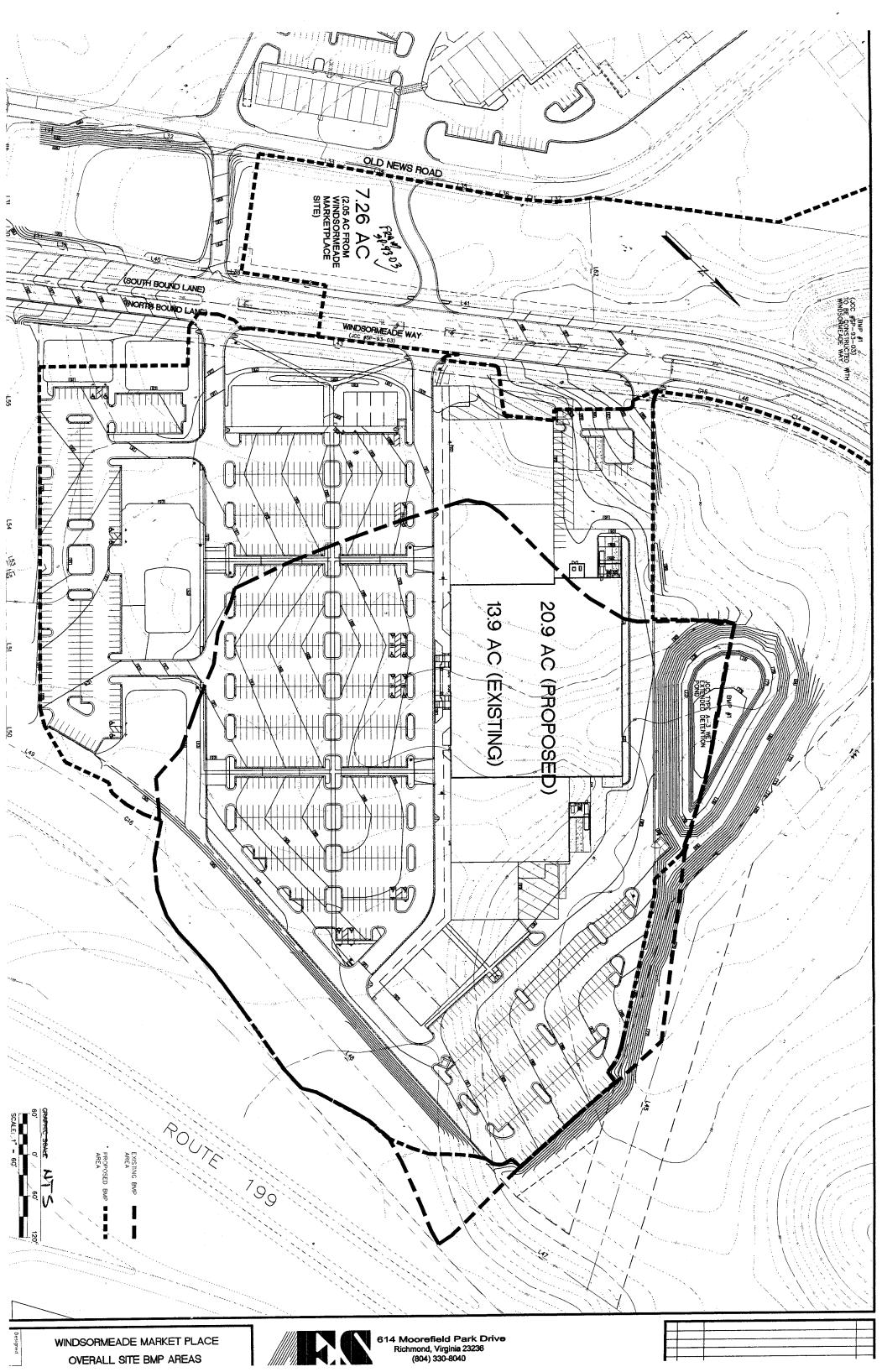
				Inc. Volume	Sum	Sum
		Area	Incremental Volume	(cu. yd.)	Volume	Volume
Elevation	<u>Depth</u>	(sq. ft.)	(cu. ft.)		(cu. ft.)	(cu. yd.)
<u>73</u>	Q	<u>6701</u>	<u>0</u>	0	0	0
74	1	12,612	9,657	358	9,657	358
75	1	13,689	13,151	487	22,807	845
76	1	14,799	14,244	528	37,051	1,372
77	1	15,942	15,371	569	52,422	1,942
78	1	22,057	19,000	704	71,421	2,645
79	1	27,489	24,773	918	96,194	3,563
80	1	29,673	28,581	1,059	124,775	4,621
81	1	31,917	30,795	1,141	155,570	5,762
82	1	34,224	33,071	1,225	188,641	6,987
83	1	36,580	35,402	1,311	224,043	8,298
84	1	38,898	37,739	1,398	261,782	9,696
85	1	40,842	39,870	1,477	301,652	11,172

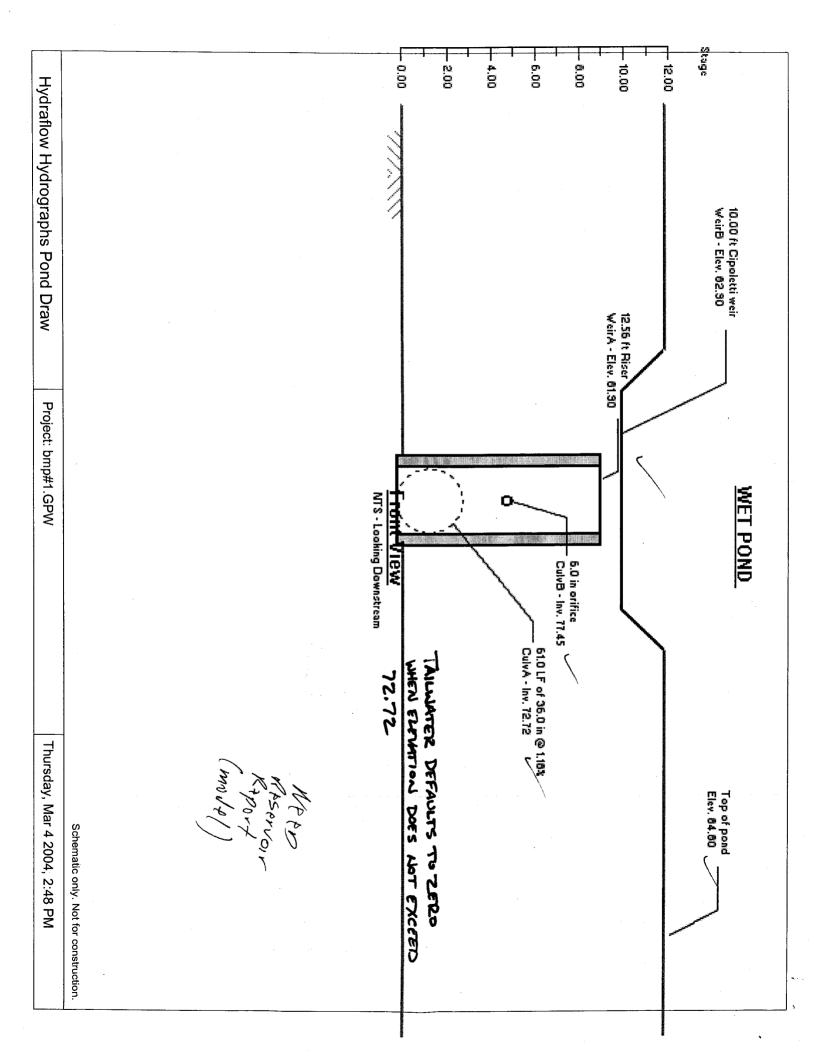
### IV. DETERMINING REQUIRED WATER QUALITY VOLUME

Due to preliminary considerations, it is desired to provide this site extended detention wet pond to achieve a 10 point BMP rating for the facility. Under the James City County guide lines for storm water management BMPs, the extended detention wet pond may have one half of the water quality volume stored in the permanent pool and one half of the water quality volume released in a 24-hour period.

Percent Impervious of the BMP Watershed, Post-Development 73.2% Drainage Area of the BMP Watershed 20.90 Impervious Acres of BMP Watershed 15.30 Calculation for Water Quality Volume, WQ WQ<sub>v</sub> = (2.0 inches per impervious acre) \*( impervious acres of BMP watershed) WQv = (2.0 inches)\*(1 ft / 12 inches) \* (43560 sq. Ft per acre) \* (impervious acres of BMP watershed)  $WQ_v = (2.0 \text{ inches})^*(1 \text{ ft / } 12 \text{ inches})^* (43560 \text{ sq. Ft per acre})^*$ 16.80 121968 cu. Ft WQ<sub>v</sub> = 60984 cu. Ft Required Volume for Permanent Pool 60984 cu. Ft Design Volume for Dry Storage (1" per Impervious Acre) WQ<sub>v</sub> (provided)= 60984 cu. Ft Water Quality Volume Provided for Wet pool Water Quality Volume Provided for Dry pool 124350 cu. Ft 185334 Total Water quality volume 81.9 Elevation of total WQv = Elevation of release inlet for 1/2 water quality volume = Average head, in feet, on release inlet = Average release rate calculation 1.4 cfs 124,350.0 cubic feet (24 hours x 60 minutes/hour x 60 seconds/ minute) Calculation of size of release inlet for 1/2 Water Quality Volume Diameter of Release Inlet = 2 \* ( Q / ((64.32 \* (h / 2)) ^ (1/2) \* 0.6 \* 3.14))) ^ (1/2) where, Q equals Average Release Rate, in cfs h equals Average Head, in feet 8 inches / Diameter of Release Inlet = 0.60 feet, or Note: A design with an orifice size of 6" will be used for channel protection requirements

1853347121968 CF 014.





# Hydrograph Return Period Recap

Hyd.	Hydrograph	Inflow				Peak Out	flow (cfs)	l <u></u> .			Hydrograph
No.	type (origin)	Hyd(s)	1-Yr	2-Yr	3-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr	description
1	SCS Runoff		7.11	12.21			31.99	37.60		53.03	PRE-DEVELOPMENt
2	SCS Runoff		43.66	57.74			103.59	115.43		146.84	9069POST-DEVELOPMENT
5	Reservoir	2	1.75	3.76			62.16	80.12		120.88	wet pond
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									1		
Proi	. file: bmp	#1.GPV	V						F	Run dat	te: 02-18-2004

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Maximum storage (cuft)	Hydrograph description
1	SCS Runoff	7.11	2	736	36,768				PRE-DEVELOPMENt
2	SCS Runoff	43.66	2	726	152,346				9069POST-DEVELOPMENT
5	Reservoir	1.75	2	902	147,696	2	81.11	159,364	wet pond
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Proj	. file: bmp	#1.GPV	V 	F	Return Pe	eriod: 1 y	r 	Run dat	te: 02-18-2004

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Maximum storage (cuft)	Hydrograph description
1	SCS Runoff	12.21	2	736	58,844				PRE-DEVELOPMENt
2	SCS Runoff	57.74	2	726	203,614	·			9069POST-DEVELOPMENT
5	Reservoir	3.76	2	812	195,647	2	82.02	189,332	wet pond
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Proi	i. file: bmp	⊥ #1 GPV	\ V	E	L Return Pe	eriod: 2 v	r	Run da	te: 02-18-2004
_ F10J	i. iiie. birip	# 1.GPV	V			<del>5</del> 110u. ∠ y	l	Turida	.G. UZ-1U-ZUU <del>4</del>

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Maximum storage (cuft)	Hydrograph description
1	SCS Runoff	31.99	2	736	145,833				PRE-DEVELOPMENT
2	SCS Runoff	103.59	2	726	376,296			<del></del>	9069POST-DEVELOPMENT
5	Reservoir	62.16	2	738	364,615	2	83.12	228,614	wet pond
Pro	⊥ j. file: bmp	#1.GP\	<b>N</b>	ı	Return Pe	eriod: 10	yr	Run da	te: 02-18-2004

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Maximum storage (cuft)	Hydrograph description
1	SCS Runoff	37.60	2	734	170,769				PRE-DEVELOPMENt
2	SCS Runoff	115.43 1		726	421,869			-	9069POST-DEVELOPMENT
5	Reservoir	80.12	2	736	409,431	2	83.30	235,495	wet pond
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						:			
									·
Pro	j. file: bmp	#1.GP\	N		Return P	eriod: 25	yr	Run da	te: 02-18-2004

Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Maximum storage (cuft)	Hydrograph description
SCS Runoff SCS Runoff Reservoir	53.03 146.84 120.88	2 2 2	734 726 732	239,937 543,909 530,212	2	83.70 Othur	  250,474	PRE-DEVELOPMENT 9069POST-DEVELOPMENT wet pond
	type (origin) SCS Runoff SCS Runoff Reservoir	type (origin) flow (cfs)  SCS Runoff 53.03 SCS Runoff 146.84 Reservoir 120.88	type (origin) flow (cfs) interval (min)  SCS Runoff 53.03 2  SCS Runoff 146.84 2	type (origin) flow (cfs) interval (min)  SCS Runoff 53.03 2 734 SCS Runoff 146.84 2 726 Reservoir 120.88 2 732	type (origin)   flow (cfs)   interval (min)   (cuft)    SCS Runoff   53.03   2   734   239,937    SCS Runoff   146.84   2   726   543,909    Reservoir   120.88   2   732   530,212	type (origin) (cfs) interval (min) (cuft) (cuft) (s) (cfs) (min) (cfs) (min) (cuft) (cfs) (c	type (origin)   flow (cfs)   interval (min)   (cuft)   hyd(s)   elevation (ft)    SCS Runoff   53.03   2   734   239.937        SCS Runoff   146.84   2   726   543.909     33.70   74.7    Reservoir   120.88   2   732   530.212   2   83.70   74.7    Original or	SCS Runoff   S3.03   2   734   239,937

Source: USDA-SCS Plate 3.18-4

180

### AES Project No. 9069 Job Title BMP No. 1

Area=	20.90 Acres	0.0327sq.mi.
CN=	91	·
Tc=	0.350 hr.	
P=	2.8 in.	Rainfall depth for 1yr return period
la=	0.198	Initial abstraction is all losses before runoff begins. le surface depressions, water intercepted by vegitation, evaporatation(SeeTR55 Chapter 2, Equation 2-1)
Qu=	630.41 csm/in	Unit Peak Discharge - Peak discharge per square mile per inch of runoff (Units are "cubic square miles per ing
Direct Runoff=	1.9 in.	Runoff in inches (See TR55 Chapter 2, Equation 2-1)
Qi=	38.82 cfs	Peak Inflow Discharge
Qo/Qi=	0.028	Ratio of Peak Inflow Discharge to Peak Outflow Discharge (See TR55 Chapter 6)
Qo=	1.08 cfs	Peak Outflow Discharge (See TR55 Chapter 6) Taken from Maryland Dept. of Stormwater Management Appendix D.1 figured.11.2. The curve for 24hr detention used in Chart 1 was scaled and a curve was fit to the data points. The resulting equation, which appears on the chart yeilds a very good fit.
Vs/Vr=		Ratio of Volume Stored to Volume Realeased (See TR55 Chapter 6). Value Computed
Vs=	2.113 Ac-Ft /	using equation for Figure 6-1 as shown in Appendix F.

Average Flow Rate (Qo) 1.08 cfs Average head= 1.55 ft.

Area of orifice= 0.18 sq.ft.

" of

Orifice diameter = 0.48 ft.
Orifice diameter = 5.7 in.

This offers a place to start. After routing the 1yr storm through the oriface check the out put to make sure that the Required Storage Volume is actually detaind for 24 hours. If not adjust the orifice size and recompute.

3.14

### TEMPORARY SEDIMENT BASIN DESIGN DATA SHEET

(with or without an emergency spillway)

INDSORMEADE MARKETRACE	
Location BEHIND SHAPING CENTER	
Total area draining to basin: 20,90 acres. $\phantom{aaaaaaaaaaaaaaaaaaaaaaaaaaaaaaaaaaa$	
e Design	
Minimum required volume = 67 cu. yds. x Total Drainage Area (acres).	
67 cu. yds. x $20.90$ acres = $1400$ cu. yds.	
Available basin volume = 2258 cu. yds. at elevation 77.45. (From storage - elevation curve)	
Excavate cu. yds. to obtain required volume*.	
* Elevation corresponding to required volume = invert of the dewatering orifice.	
Available volume before cleanout required.	
33 cu. yds. x $20.9$ acres = $690$ cu. yds.	
Elevation corresponding to cleanout level = $74.68$ .	
(From Storage - Elevation Curve)	

### **Dry Storage:**

(Min. = 1.0 ft.)

7. Minimum required volume = 67 cu. yds. x Total Drainage Area (acres).

67 cu. yds. x 20.90 acres = 1400 cu. yds.

Distance from invert of the dewatering orifice to cleanout level = Z 77 ft.

Total available basin volume at crest of riser\* = 6864 cu. yds. at 8. elevation 8190 . (From Storage - Elevation Curve)

\* Minimum = 134 cu. yds./acre of total drainage area.

TOTAL DAY STORES 4606 CY DESIGNED VITTH TOMP Diameter of dewatering orifice = 9. CHECKED AND DOOK NOT DECRENSE DEAL DOLL TIME

Diameter of flexible tubing = \_\_\_\_\_\_in. (diameter of dewatering orifice 10. plus 2 inches).

#### Preliminary Design Elevations

Crest of Riser = 01.9011. Top of Dam = 94.80Design High Water = 83.30 Upstream Toe of Dam = \_\_\_72.00 /

#### Basin Shape

Length of Flow 12. Effective Width

If > 2, baffles are not required \_\_\_\_\_\_ 2.

#### Runoff

 $Q_2 = \underbrace{57.74}_{\text{Cfs}} \text{ cfs} \qquad \text{(From Chapter 5)}$   $Q_{25} = \underbrace{115.45}_{\text{Cfs}} \text{ cfs}$ 13.

14.

#### Principal Spillway Design

With emergency spillway, required spillway capacity  $Q_p = Q_2 = \frac{99.74}{2}$  cfs. 15. (riser and barrel)

Without emergency spillway, required spillway capacity  $Q_p = Q_{25} =$ \_\_\_\_ cfs. (riser and barrel)

16. With emergency spillway:

Assumed available head (h) =  $\int$  ft. (Using Q<sub>2</sub>)

h = Crest of Emergency Spillway Elevation - Crest of Riser Elevation

Without emergency spillway:

Assumed available head (h) = 1.4 ft. (Using  $Q_{25}$ )

h = Design High Water Elevation - Crest of Riser Elevation

17. Riser diameter  $(D_r) = 48$  in. Actual head (h) = 13 ft. (From Plate 3.14-8.)

Note: Avoid orifice flow conditions.

- 18. Barrel length (l) = \_\_\_\_\_\_ ft.

  Head (H) on barrel through embankment = \_\_\_\_\_\_ ft.

  (From Plate 3.14-7).
- 19. Barrel diameter = 36 in.

  (From Plate 3.14-B [concrete pipe] or Plate 3.14-A [corrugated pipe]).
- 20. Trash rack and anti-vortex device

Diameter = 72 inches.

Height = \_\_\_\_\_ inches.

(From Table 3.14-D).

#### **Emergency Spillway Design**

- 21. Required spillway capacity  $Q_e = Q_{25} Q_p = 57.69$  cfs.
- 22. Bottom width (b) = 10 ft.; the slope of the exit channel (s) =

  ft./foot; and the minimum length of the exit channel (x) =

  ft.

  (From Table 3.14-C).

#### Anti-Seep Collar Design

- 23. Depth of water at principal spillway crest (Y) = 9 ft.

  Slope of upstream face of embankment (Z) = 3:1.

  Slope of principal spillway barrel  $(S_b) = 1.19$  %

  Length of barrel in saturated zone  $(L_s) = 35$  ft.
- 24. Number of collars required =  $\frac{2}{\sqrt{2}}$  dimensions =  $\frac{\sqrt{2}}{\sqrt{2}}$  (from Plate 3.14-12).

#### Final Design Elevations

Design High Water = <u>B3.30</u>

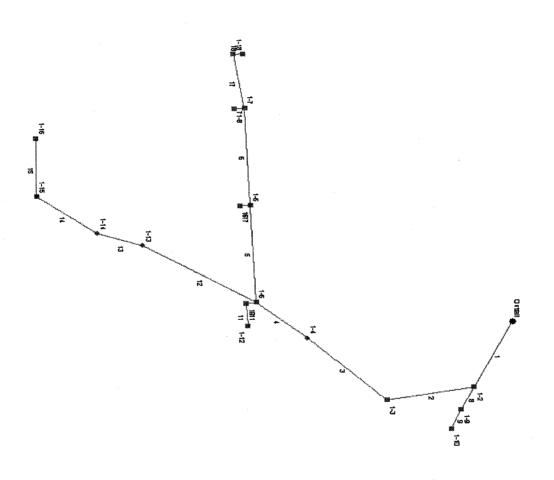
Emergency Spillway Crest = <u>B2.90</u>

Principal Spillway Crest = <u>B1.90</u>

Dewatering Orifice Invert = <u>77.45</u>

Cleanout Elevation = <u>74.68</u>

Elevation of Upstream Toe of Dam or Excavated Bottom of "Wet Storage Area" (if excavation was performed) = <u>72.00</u>



04-08-2004

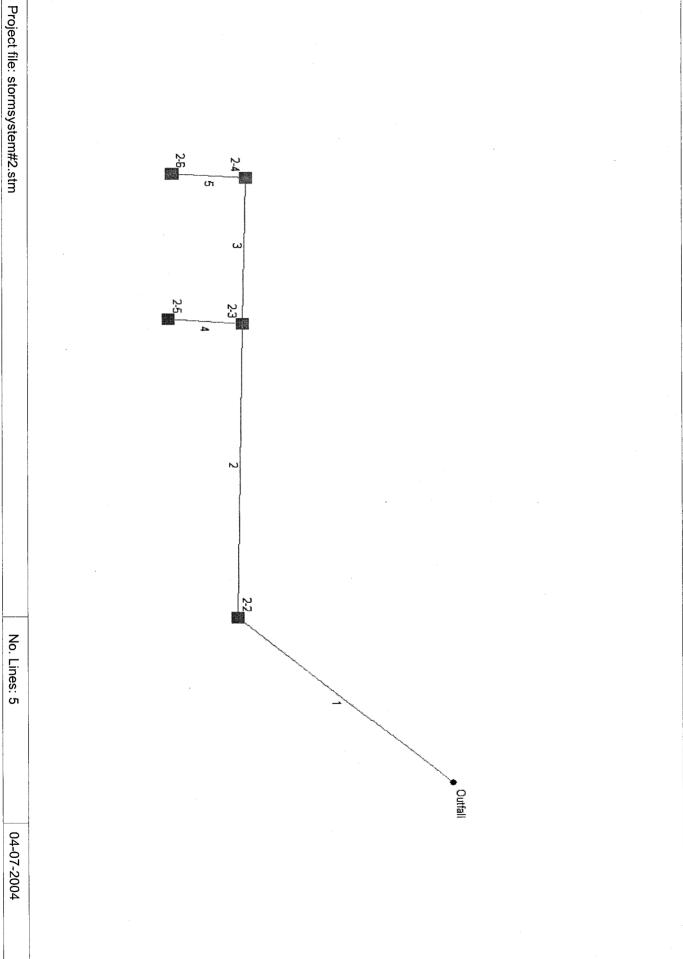
No. Lines: 18

Project file: stormsystem#1.stm

# **Storm Sewer Tabulation**

NO	Pr		18	17	16	5	14	13	12	<u> </u>	10	9	œ	7	თ	G	4	ω	N	_		Line	Sta
ES: Int	Project File:		17	თ	ζī	14	3	12	4	10	4	00		တ	Cī	4	ω	2		End	<u>-</u>	70	Station
ensity =			ģ,4	142.0	24.0	151.0	170.0	109.0	300.0	58.0	24.0	56.0	64.0	24.0	252.0 1.14	252.0	149.0~	243.0	203.0	192.0 1.11	<b>æ</b>		Len
: 140.36	msyste		0.36	0.26	24.0 - 2.15	1.70	0.66	0.00	0.00	0.61	1.25	0.45	1.80	1.46	7.14	1.25	1.63	0.00	0.66	1.1	(ac)	Incr	Drng
) (Inlet	stormsystem#1.stm		0.36	0.62	2.15	1.70 ✓	2.36	2.36	2.36	0.61	1.86	0.45	2.25	1.46	3.22	6.62	12.47	12.47	13.13	16.49	(ac)	Total	Drng Area
NOTES: Intensity = 140.36 / (Inlet time + 19.80) ^ 0.93;			0.70	0.70	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	Ĉ	COG	Rnoff
19.80) ^			0.25	0.18	1.94	1.53	0.59	0.00	0.00	0.55	1.13	0.41	1.62	1.31	1.03	1.13	1.47	0.00	0.59	1.00		Incr	
1			0.25	0.43	1.94	1.53	2.12	2.12	2.12	0.55	1.67	0.41	2.03	1.31	2.77	5.83	11.10	11.10	11.69	14.72		Total	Area x C
Return period =			5.0	5.0	5.0	5.0	5.0	5.0	(5 <sub>0</sub> )	18.0	19.0	8.0	10.0	5.0	5.0	5.0		(5.0) Mit.	12.01	5.0	(min)	Inlet	
period =			5.0	5.2	5.0	5.0	5.7	6.4	6.8	18.0	19.0	8.0	10.0	5.0	6.2	7.8	19.2	19.8	20.8	<u>21</u>	(min)	Syst	Tc
10 Yrs		 	7.0	6.9	7.0	7.0	6.8	6.7	6.6	4.7	4.6	6.3	5.9	7.0	6.7	6.3	4.6	4.5	4.4	4.3	(in/hr)		Rain
,,			1.76	3.01	13.54	10.70	14,46	14.14	13.94	2.59	7.71	2.55	11.93	9.19	18.58	36.96	50.91/	50.18	51.63	63.77	) (cfs)		Total
			8.23	8.18	4/39.18	0 15.83	6 /15.99	4 15.92	4 19.24	13.22	40.51	8.63	3 38.45	38.63	8 47.16	6 -47.16	101.9	8 101.8	3 104.8	7/106.2	(cfs)		Cap
			1.44	2.45	8 4.31	3 3.41	4.60	2 4.50	4 4.44	2 2.11	1 2.45	2.08	5 3.80	3 2.93	6 2.63	6 5.23	9 4.05	3.99	8 4.11	5.08	(ft/s)		V <sub>e</sub>
			<del>-</del> <del>-</del> 5	15	24	24•	24.	24	24	15	24	15	24	24	36 🔨	36~	48	48 1	48	48	(ii)	Size	
		1.362 1.362		1.61	3.00	0.49	0.50	0.50	0.72	4.19	3.21	1.79	2.89	2.92	0.50	0.50	0.50	0.50	0.53	0.55	(%)	Slope	Pipe
	Nun	300	_	85.00	82.18	84.50	83.76	82.91	82.37	83.40	80.97	80.00	79.00	83.42	82.72		80.20	79.45	78.23	77.15	(£)	e Up	
	Number of lines: 18		85.00	82.	<u>ر گر</u> 81.			82.37		80.97	80.20	79.00	77.15	•	81.46		ر 79.	78.23	/ 77.15		(£)	D	Invert Elev
	nes: 18			82.72 8	81.46	83.76~ 8	82.91 / 8		80.20 8					82.72 8	6 6 	80.20 🗸 8	79.45 - 8			76.10 8	=		
			87.58	87.43	86.85 <	88.64 /	87.89~	87.06 <	86.49	85.61 <	85.38~	84.38 /	84.18 /	87.16	86.96 <	86.13~	85.07 ′	84.85 ′	84.26 ′	83.50 <	∄	Ę	НОГ
		•	87.57	87.12~	86.76	88.30 ′	87.20 /	86.63 ~	85.35 ^	85.52	85.35	84.29	84.00 ~	87.12	86.76	85.35	84.88	84.55	84.00 /	83.12	(£)	Dn	Elev
	Run Date:		90.00	90.00	88.00~	89.75	91.25	94.00	92.90	89.90	88.50	87.00	86.00	88.00 🗸	88.00 ~	88.00 /	88.50	91.50	89.75	87.00	<b>(f)</b>	ç	Grnd / F
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	04-08-2004		1-19 to 1-18	1-18 to 1-7	1-17 to 1-6	1-16 to 1-15	1-15 to 1-14	1-14 to 1-13		1-12 to 1-11	1-11 to 1-5	1-10 to 1-9	1-9 to 1-2	1-7 to 1-8	1-6 to 1-7	1-5 to 1-6	1-4 to 1-5	1-3 to 1-4	1-2 to 1-3	1-1 to 1-2		_	Line ID
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# **Hydraflow Plan View**



# **Storm Sewer Tabulation**

TAILMAN BEWANT BARA

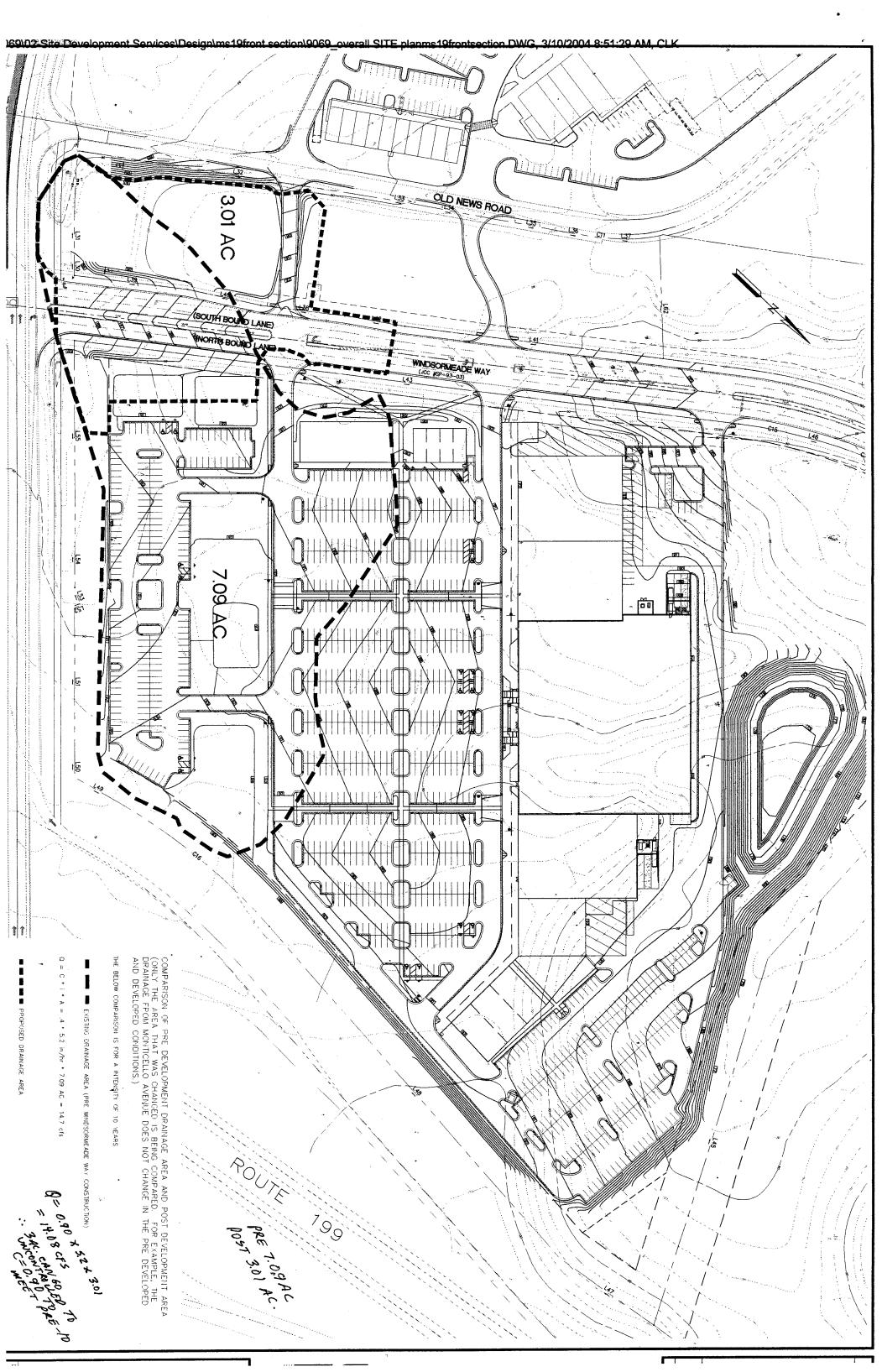
Page 1

Line (ft) (ac) (ac) (C) (min)  End 139.0 0.73 2.63 0.90 0.66 2.37 5.0  1 163.0 0.39 1.90 0.90 0.35 1.71 5.0  2 36.0 0.53 0.53 0.90 0.48 0.48 5.0  3 36.0 0.27 0.27 0.90 0.24 0.24 5.0  [Aucust 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	ation Len	🐫	Rnoff	3	Area x C	Tc	Syst	Rain	Total flow	Cap	V <sub>e</sub>		Pir Pir	Pipe Size Slope	ipe Slope	Slope	ipe Invert Elev	ipe Invert Elev HGL Elev	ipe Invert Elev HGL Elev	ipe Invert Elev HGL Elev
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stormsystem#2.stm Number of lines: 5																				
stormsystem#2.stm Number of lines: 5		·																		
stormsystem#2.stm Number of lines: 5																	- 140 A 150 AVA			
	Project File: storms	ystem#2.st	3											Numbe	r of lines:	51		Run D		Run Date: 04-07-2004

# **Storm Sewer Tabulation**

TAILMAN CHENCHA GAMES

Pr		-		Line	Sta
oject Fi		End	Line	10	Station
le: stor		50.0	∄		Len
msyste		1.13	(ac)	Incr	Drng
Project File: stormsystem#3.stm		1.13	(ac)	Total	Drng Area
3		0.90	Ĉ		Rnoff
		1.02	-	Incr	
		1.02		Total	Area x C
		5.0	(min)	Inlet	
		5.0	n) (min)	et Syst	Тс
		7.0			 ≥ <i>?</i> ?
			(in/hr) (cfs)		Rain Total
		7.11 21			
		21.18 5	(cfs) (f		Cap
		5.80	(ft/s)		<u>é</u>
		5	(in)	Size	Pipe
		7.70	(%)	Slope	· ·
Numb		81.55	<b>Æ</b>	Ę,	Inve
Number of lines: 1		77.70	( <del>t</del> )	D	Invert Elev
7		83.55	<b>æ</b>	두/	HG HG
	MK11005	83.12	<b>3</b>	<u> </u>	HGL Elev
Run Date:	MCLUPES 10" HOPE FROM (ONDING RAMP.	90.55	<b>(£)</b>	두	Grnd / R
ate: 04-07-2004	RAMP.	78.95	( <del>I</del>	뫄	Grnd / Rim Elev
-2004				,	Line ID



#### Table 2

#### Worksheet for BMP Point System

A. STRUCTURAL BMP POINT ALLOCATION

		Fraction of Site Served	Weighted
BMP	BMP Points	by BMP/	BMP Points
#1 WET ED		20.90 AC/31.44 AC = 2.05AC /31.44AC =	6.65
#4 WET ED	x	2.05AL /31.44AL =	0.65
CONSTRUCTED W	ALL MINDENSKINGATE INA X	=	
	X		

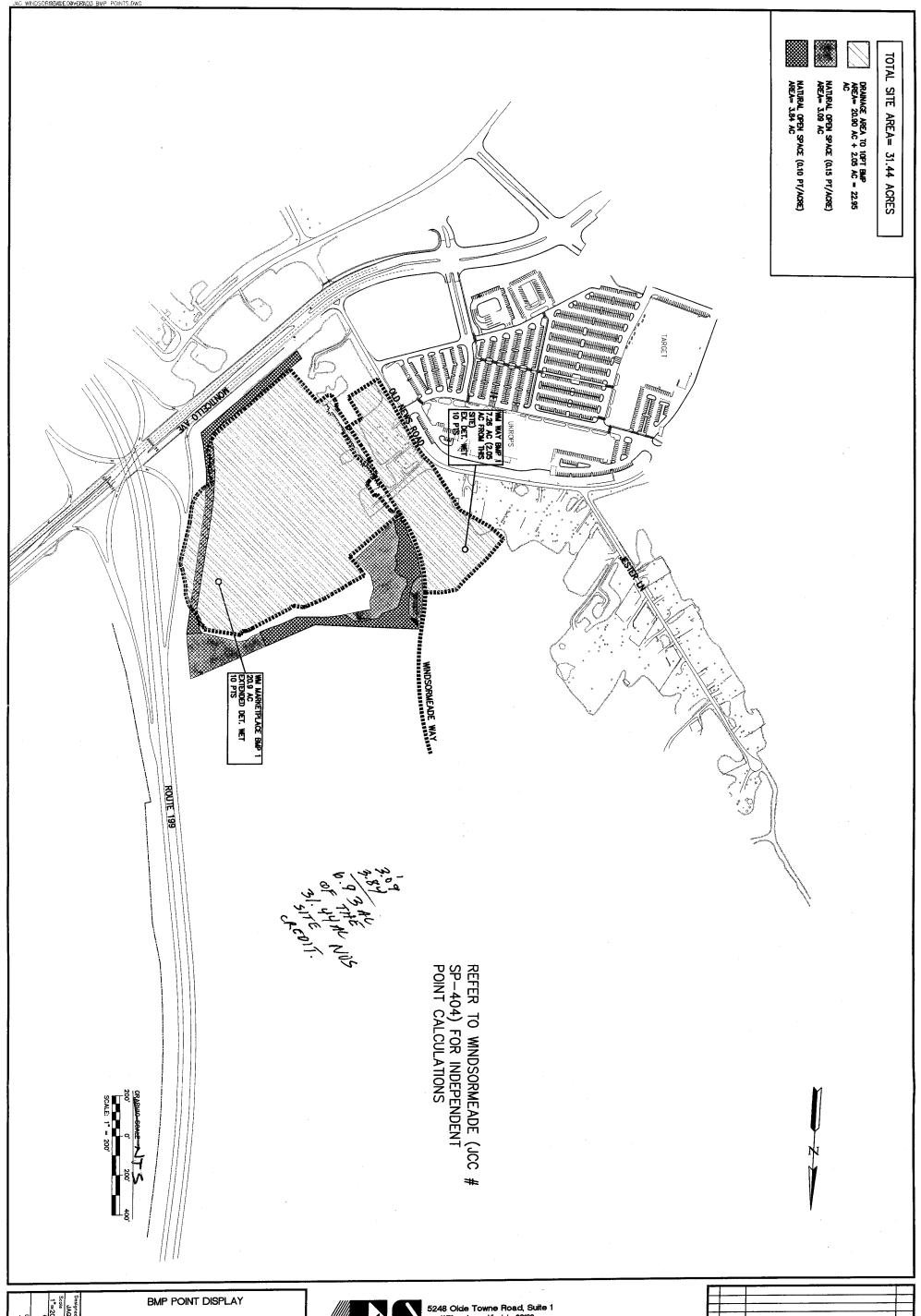
B. NATURAL OPEN SPACE CREDIT

Fraction of Site	Natural		Points for	_
Fraction of Site	Open Space Credit	er en <del>en en</del> en german	Natural Open Space	2
31.44AC 12.21% X	0,10	=	1.22	
3.09AC = 9.80% X	(0.1 per 1%) 0.15 (0.15 per 1%)	=	1.47	- -

TOTAL NATURAL OPEN SPACE CREDIT: 2.69

C. TOTAL WEIGHTED POINTS

goestion whether 2.05 Ac to the Windsor Meade WAY ROAD POND WAS already counted.



Designed Drawn
JAG GVC
Scale
1\*=200' Date
Project No.
Drawing No.
1 OF 1

CONSULTING ENGINEERS

5248 Olde Towne Road, Suite 1 Williameburg, Virginia 23188 (757) 253-0040 Fax (757) 220-8994

$\Box$			
4			
4			
+			
10.	DATE	REVISION / COMMENT / NOTE	BY



pe 203

#### James City County, Virginia Environmental Division

# **Stormwater Management / BMP Facilities Record Drawing and Construction Certification**

#### Standard Forms & Instructions

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Issue Date February 1, 2001



#### James City County, Virginia Environmental Division

# Stormwater Management / BMP Facilities Record Drawing and Construction Certification Forms

(Note: In accordance with the requirements of the Chesapeake Bay Preservation Ordinance, Chapter 23, Section 23-10(4), BMP's shall be designed and constructed in accordance with the manual entitled James City County Guidelines for Design and Construction of Stormwater Management BMP's. Erosion and sediment control policy and approved plans generally require that at the completion of the project and prior to release of surety, an "as-built" plan prepared by a registered Professional Engineer or Certified Land Surveyor must be provided for the drainage system for the project, including any Best Management Practice (BMP) facilities. In addition, for BMP facilities involving the construction of an impounding structure or dam embankment, certification is required by a Professional Engineer who has inspected the structure during its construction. Currently there are over 20 water quality type BMP's accepted by the County.)

#### <u>Section 1 – Site Information:</u>

Project Name:		eade Market Place			<u> </u>
Structure/BMP Name:		' 11 A O XXX' 1			
Project Location:		icello Ave., & Winds	orMeade Way		<del></del>
BMP Location:	Behind Bel				
County Plan No.:	SP	<u> </u>	05		
	Residential Commercial Institutional Public Other	☐ Business ☐ Office ☐ Industrial ☐ Roadway	Tax Map/Parcel No.: BMP ID Code (if known): Zoning District: Land Use: Site Area (sf or acres):	3831800001 PC 203 MU (Mixed U Shopping Cen 31.44 Ac.	Jse) w/proffers ter
Brief Description of S	tormwater Managen	nent/BMP Facility: <u>T</u>	ype A-3 Wet Extended Dete	ntion Pond	
Nearest Visible Landr	nark to SWM/BMP	Facility: Be	elk store		
Nearest Vertical Grou	nd Control (iflenous	· · ·			
	•	·		□ A 1.3	
_	etic Ground Control	USGS	☐ Temporary	☐ Arbitrary	☐ Other
Station Numb	er or Name:	No. 322			
Datum or Ref	erence Elevation:	NGVD 29			
Control Descr	iption:	3-1/4" disk in concre	ete		
Control Locat	ion from Subject Fac				

#### Section 2 - Stormwater Management / BMP Facility Construction Information: PreConstruction Meeting Held for Construction of SWM/BMP Facility: ☐ Yes ☐ No ☐ Unknown Approx. Construction Start Date for SWM/BMP Facility: Facility Monitored by County Representative during Construction: ☐ Yes ☐ No □ Unknown Name of Site Work Contractor Who Constructed Facility: Name of Professional Firm Who Routinely Monitored Construction: Date of Completion for SWM/BMP Facility: Date of Record Drawing/Construction Certification Submittal: (Note: Record Drawing and Construction Certifications are required within thirty (30) days of the completion of Stormwater Management and/or BMP facility construction. Record Drawings and Construction Certifications must be reviewed and approved by the James City County Environmental Division prior to final inspection, acceptance and bond or surety release.) <u>Section 3 – Owner / Designer / Contractor Information:</u> Owner/Developer: (Note: Site Owner or Applicant responsible for development of the project.) Name: SLN Williamsburg Associates, L.L.C. Mailing Address: 9211 Forest Hill Ave., Suite 110 Richmond, VA 23235 **Business Phone:** 804-320-7600 Fax:804-330-8924 Contact Person: Jim Gresock Title: (Note: Professional Engineer or Certified Land Surveyor responsible for the design and Design Professional: preparation of plans and specifications for the Stormwater Management / BMP facility.) Firm Name: AES Consulting Engineers Mailing Address: 5248 Olde Towne Rd., Suite 1 Williamsburg, VA 23188 **Business Phone:** 757-253-0040 Fax: 757-220-8994 Responsible Plan Preparer: G. Archer Marston, III, P.E. Title: Vice President Plan Name: WindsorMeade Market Place Firm's Project No. 9069-02 Plan Date: 12-29-06 Sheet No.'s Applicable to SWM/BMP Facility: **BMP Contractor:** (Note: Site Work Contractor directly responsible for construction of the Stormwater Management / BMP facility.) Name: Jack L. Massie Contractor Inc. Mailing Address: 3900 Cokes Lane Williamsburg, VA 23188 Business Phone: 757-566-8643 Fax: 757-566-8566 Contact Person: Scott Massie Site Foreman/Supervisor: Scott Massie Specialty Subcontractors & Purpose (for BMP Construction Only):

#### Section 4 - Professional Certifications:

Certifying Professionals: (Note: A Registered Professional Engineer of Certified Land Surveyor is responsible for preparation of a Record Drawing, sometimes referred to as an As-Built plan, for the drainage system for the project including any Stormwater Management/BMP Facilities. A Registered Professional Engineer is responsible for the inspection, monitoring and certification of Stormwater Management / BMP facilities during its construction.)

#### Record Drawing and Construction Certifications for Stormwater Management / BMP Facilities

Record Drawing Certification	Construction Certification
Firm Name: AES Consulting Engineers	Firm Name: ECS, Ltd.
Mailing Address: 5248 Olde Towne Rd., Suite 1	Mailing Address: 108 Ingram Rd., Unit 1
Williamsburg, VA 23188	Williamsburg, VA 23188
Business Phone: 757-253-0040	Business Phone: 757-229-6677
Fax: 757-220-8994	Fax: 757-229-9978
Name: G. Archer Marston, III, P.E.	Name: Michael I. Galli P. E
Title: Vice President	Name: Michael J. Galli, P.E. Title: Vice Resident
Signature:	Signaturez Muharfflull  Date: 5/3/06
Date:	Date: 5/3/06
I hereby certify to the best of my knowledge and belief that this record drawing represents the actual condition of the Stormwater Management / BMP facility. The facility appears to conform with the provisions of the approved design plan, specifications and stormwater management plan, except as specifically noted.	I hereby certify to the best of my knowledge and belief that this Stormwater Management / BMP facility was monitored and constructed in accordance with the provisions of the approved design plan, specifications and stormwater management plan, except as specifically noted.

(Seal)

(Seal)

Virginia Registered Professional Engineer Or Certified Land Surveyor

Virginia Registered Professional Engineer

#### **Section 4 – Professional Certifications:**

Certifying Professionals: (Note: A Registered Professional Engineer of Certified Land Surveyor is responsible for preparation of a Record Drawing, sometimes referred to as an As-Built plan, for the drainage system for the project including any Stormwater Management/BMP Facilities. A Registered Professional Engineer is responsible for the inspection, monitoring and certification of Stormwater Management / BMP facilities during its construction.)

#### Record Drawing and Construction Certifications for Stormwater Management / BMP Facilities

#### **Record Drawing Certification**

Record Drawing Certification	<b>Construction Certification</b>
Firm Name: AES Consulting Engineers	Firm Name: ECS, Ltd.
Mailing Address: 5248 Olde Towne Rd., Suite 1	Mailing Address: 108 Ingram Rd., Unit 1
Williamsburg, VA 23188	Williamsburg, VA 23188
Business Phone: 757-253-0040	Business Phone: 757-229-6677
Fax: 757-220-8994	Fax: 757-229-9978
Nome: C. Archen Maneters, III. D.E.	Name Mid-all City
Name: G. Archer Marston, III, P.E.  Title: Vice President	Name: Michael J. Galli
The. Vice resident	Title:
Signature: ////////////////////////////////////	Signature:
Date: 7/2//06	Date:
, , ,	
I hereby certify to the best of my knowledge and belief that this record drawing represents the actual condition of the Stormwater Management / BMP facility. The facility appears to conform with the provisions of the approved design plan, specifications and stormwater management plan, except as specifically noted.	I hereby certify to the best of my knowledge and belief that this Stormwater Management / BMP facility was monitored and constructed in accordance with the provisions of the approved design plan, specifications and stormwater management plan, except as specifically noted.
6. ARCHER MARSTON III No. 018232	
(Seal)	(Seal)

Virginia Registered Professional Engineer Or Certified Land Surveyor

Virginia Registered Professional Engineer

#### Section 5 - Record Drawing and Construction Certification Requirements and Instructions:

- PreConstruction Meeting Provides an opportunity to review SWM / BMP facility construction, maintenance and operation plans and address any questions regarding construction and/or monitoring of the structure. The design engineer, certifying professionals (if different), Owner/Applicant, Contractor and County representative(s) are encouraged to attend the preconstruction meeting. Advanced notice to the Environmental Division is requested. Usually, this requirement can be met simultaneously with Erosion and Sediment Control preconstruction meetings held for the project.
- A fully completed STORMWATER MANAGEMENT / BMP FACILITIES, RECORD DRAWING and CONSTRUCTION CERTIFICATION FORM and RECORD DRAWING CHECKLIST. All applicable sections shall be completed in their entirety and certification statements signed and sealed by the registered professional responsible for individual record drawing and/or construction certification.
- ☐ The Record Drawing shall be prepared by a Registered Professional Engineer or Certified Land Surveyor for the drainage system of the project including any Best Management Practices.
- Construction Certification. Construction of Stormwater Management / BMP facilities which contain impoundments, embankments and related engineered appurtenances including subgrade preparation, compacted soils, structural fills, liners, geosynthetics, filters, seepage controls, cutoffs, toe drains, hydraulic flow control structures, etc. shall be visually observed and monitored by a Registered Professional Engineer or his/her authorized representative. The Engineer must certify that the structure, embankment and associated appurtenances were built in accordance with the approved design plan, specifications and stormwater management plan and standard accepted construction practice and shall submit a written certification and/or drawings to the Environmental Division as required. Soil and compaction test reports, concrete test reports, inspection reports, logs and other required construction material or installation documentation may be required by the Environmental Division to substantiate the certification, if specifically requested. The Engineer shall have the authority and responsibility to make minor changes to the approved plan, in coordination with the assigned County inspector, in order to compensate for unsafe or unusual conditions encountered during construction such as those related to bedrock, soils, groundwater, topography, etc. as long as changes do not adversely affect the integrity of the structure(s). Major changes to the approved design plan or structure must be reviewed and approved by the original design professional and the James City County Environmental Division.
- Record Drawing and Construction Certifications are required within **thirty (30) days** of the completion of Stormwater Management / BMP facility construction. Submittals must be reviewed and accepted by James City County Environmental Division prior to final inspection, acceptance and bond/surety release.

Dual Purpose Facilities – Completion of construction also includes an interim stage for Stormwater Management / BMP facilities which serve dual purpose as temporary sediment basins during construction and as permanent stormwater management / BMP facilities following construction, once development and stabilization are substantially complete. For these dual purpose facilities, construction certification is required once the temporary sediment basin phase of construction is complete. Final record drawing and construction certification of additional permanent components is required once permanent facility construction is complete.

Interim Construction Certification is required for those dual purpose embankment-type facilities that are generally ten (10) feet or greater in dam height (\*) and may not be converted, modified or begin function as a permanent SWM / BMP structure for a period generally ranging from six (6) to eighteen (18) months or more from issuance of a Land Disturbance permit for construction.

Interim or final record drawing and construction certifications are not required for temporary sediment basins which are designed and constructed in accordance with current minimum standards and specifications for temporary sediment basins per the Virginia Erosion and Sediment Control Handbook (VESCH); have a temporary service life of less than eighteen (18) months; and will be removed completely once associated disturbed areas are stabilized, <u>unless</u> a distinct hazard to the public's health, safety and welfare is determined by the Environmental Division due to the size or presence of the structure or due to evidence of improper construction.

(\*Note: Dam Height as referenced above is generally defined as the vertical distance from the natural bed of the stream or waterway at the downstream toe of the embankment to the top of the embankment structure in accordance with 4VAC50-20-30, Virginia Impoundment Structure Regulations and the Virginia Dam Safety Program.)

- Record Drawings shall provide, at a minimum, all information as shown within these requirements and the attached **RECORD DRAWING CHECKLIST** specific to the type of SWM/BMP facility being constructed. Other additional record data may be formally requested by the James City County Environmental Division. (Note: Refer to the current edition of the James City County Guidelines for Design and Construction of Stormwater Management BMP's manual for a complete list of acceptable BMP's. Currently there are over 20 acceptable water quality type BMP's accepted by the County.)
- Record Drawings shall consist of blue/black line prints and a reproducible (mylar, sepia, diazo, etc.) set of the approved stormwater management plan including applicable plan views, profiles, sections, details, maintenance plans, etc. as related to the subject SWM / BMP facility. The set shall indicate "RECORD DRAWING" in large text in the lower right hand corner of each sheet with record elevations, dimensions and data drawn in a clearly annotated format and/or boxed beside design values. Approved design plan values, dimensions and data shall not be removed or erased. Drawing sheet revision blocks shall be modified as required to indicate record drawing status. Elevations to the nearest 0.1' are sufficiently accurate except where higher accuracy is needed to show positive drainage. Certification statements as shown in Section 4 of the Record Drawing and Construction Certification Form, or similar forms thereof, and professional signatures and seals, with dates matching that of the record drawing status in the revision or title block, are also required on all associated record drawing plans, prints or reproducibles.
- Submission Requirements. Initial and subsequent submissions for review shall consist of a minimum of one (1) blue/black line set for record drawings and one copy of the construction certification documents with appropriate transmittal. Under certain circumstances, it is understood that the record drawing and construction certification submissions may be performed by different professional firms. Therefore, record drawing submission may be in advance of construction certification or vice versa. Upon approval and prior to release of bond/surety, final submission shall include one (1) reproducible set of the record drawings, one (1) blue/black line set of the record drawings and one (1) copy of the construction certification. Also for current and/or future incorporation into the County BMP database and GIS system, it is requested that the record drawings also be submitted to the Environmental Division on a diskette or CD-ROM in an acceptable electronic file format such as \*.dxf, \*.dwg, etc. or in a standard scanned and readable format. The electronic file requirement can be discussed and coordinated with Environmental Division staff at the time of final submission.

(Key for Checklist is as follows: XX Acceptable N/A Not Applicable Inc Incomplete) I. Methods and Presentation: (Required for all Stormwater Management / BMP facilities.) XX All constructed facilities meet approved design plans, unless otherwise shown. Record information or deviations from approved design plan shown in clearly annotated format and/or boxed beside design values. Elevations to the nearest 0.1' unless higher accuracy is needed to show positive drainage. All plan sheets labeled with "RECORD DRAWING" in large text in lower right hand corner (Approved County Plan Number and BMP ID Code can be included if known). All plans sheet revision blocks modified to indicate date and record drawing status. All plan sheets have certification statements and certifying professional's signature and seal. Minimum Standards: (Required for all Stormwater Management / BMP facilities, as applicable.) All requirements of Section I (Methods and Presentation) apply to this section. Plan Views: Show general location, arrangement and dimensions. Location and alignment shall generally match approved design plans. Profile or elevations along top or berm of the facility. At a minimum, elevations are required at each end, at intervals not to exceed 50 feet and where low spots may be present. Top of embankment or berm elevations must be no less than design elevation plus any settlement Top widths, berm widths and embankment side slopes. Show length, width and depth of facility or grading, contours or spot elevations as required to verify permanent pool and design storage volumes were met or were reasonably close to the approved design. Evaluation of as-built grading, contours, spot elevations, or cross-sections, may be necessary by the professional to ensure approved design configurations, depths and volumes were closely maintained. If grading or elevations are significantly different from the approved plan, the Environmental Division shall be contacted immediately to determine whether the variation is acceptable or whether further evidence will be required. Facilities which do not closely resemble approved plan grades, elevations or configurations may require regrading by the Contractor; check volumetric computations; and/or a check hydraulic routing to ensure approved design water surface elevations, discharges or freeboard were closely maintained. LL 6. Cross-section of the embankment through the principal spillway or outlet barrel. Must extend at least 100 ft. downstream of the pipe outlet or to recorded site property line, whichever is closer. Proper correlation is required between principal spillway (control structure) crest, emergency spillway crest, orifice and weirs and the top of the dam or facility. All elevations and dimensions must reasonably match the design plan or be sequentially relative to each other and the facility must reflect the required design storage volume(s) and/or design depth. Profile or elevations along the entire centerline of the emergency spillway. Emergency spillway

Elevation of the principal spillway crest or outlet crest of the structure.

may be steeper, but no flatter or narrower than design.

<u> </u>	9.	Primary control structure (riser) diameter or dimensions, height, type of material and base size. Indicate provisions for access that are present such as steps, ladders, etc.
XX	10.	Dimensions, locations and elevations of outlet orifices, weirs, slots and drains.
<u> </u>	11.	Type and size of anti-vortex and trash rack device. Height, diameter, dimensions, bar spacings (if applicable) and elevations relative to the principal spillway crest. Indicate if lockable hatch is present or not.
Gestah Geodech	12.	Type, location, size and number of anti-seep collars or documentation of other methods utilized for seepage control. May need to obtain this information during construction.
bestech	13.	Top of impervious core embankment, core trench limits and elevation of cut-off trench bottom.  May need to obtain this information during construction.
XX	14.	Elevation of the principal spillway barrel (outlet pipe) inlet and outlet invert.
XX	15.	Outlet barrel diameter, length, slope, type and thickness class of material and type of flared end sections, headwall or endwall.
XX	16.	Outfall protection dimension, type and depth of rock and if underlain filter fabric is present.
XX	17.	BMP interior and periphery landscaping zones conform with arrangements and requirements of the approved design plan.
XX	18.	Maintenance plan taken from approved design plan transposed onto record drawing set.
人人	19.	Fencing location and type, if applicable to facility.
<u> X</u> «	20.	BMP vicinity properly cleaned of stockpiles and construction debris.
XX	21.	No visual signs of erosion or channel degradation immediately downstream of facility.
XX	22.	Any other information formally requested by the Environmental Division specific to the constructed SWM/BMP facility.

( Key for	Checkli	st is as follows: XX Acceptable <u>N/A</u> Not Applicable <u>Inc</u> Incomplete)
III.	Grou	p A – Wet Ponds (Includes A-1 Small Wet Ponds; A-2 Wet Ponds; A-3 Wet Ext Det Ponds.)
XX	A1.	All requirements of Section II, Minimum Standards, apply to Group A facilities.
_XX_	A2.	Principal spillway consists of reinforced concrete pipe with O-Ring gaskets for watertight joint construction. HDPR per approved plan.
XX	A3.	Sediment forebays or pretreatment devices provided at inlets to pond. Generally 4 to 6 ft. deep.
NA	A4.	Access for maintenance and equipment is provided to the forebay(s). Access corridors are at least 12 ft. wide, have a maximum slope of 15 percent and are adequately stabilized to withstand heavy equipment or vehicle use.
N/A	A5.	Adequate fixed vertical sediment depth markers installed in the forebay(s) for future sediment monitoring purposes.
_N/A_	A6.	Pond liner (if required) provided. Either clay liners, polyliners, bentonite liners or use of chemical soil additives based on requirements of the approved plan.
N/A	A7.	Minimum 6 percent slope safety bench extending a minimum of 15 feet outward from normal pool edge and/or an aquatic bench extending a minimum of 10 feet inward from the normal shoreline with a maximum depth of 12 inches below the normal pool elevation, if applicable, per the approved design plans. (Note: Safety benches may be waived if pond side slopes are no steeper than 4H:1V).
XX	A8.	No trees are present within a zone 15 feet around the embankment toe and 25 feet from the principal spillway structure.
XX	A9.	Wet permanent pool, typically 3 to 6 feet deep, is provided and maintains level within facility.
XX	A10.	Low flow orifice has a non-clogging mechanism.
XX	A11.	A pond drain pipe with valve was provided.
<u>_XX</u>	A12.	Pond side slopes are not steeper than 3H:1V, unless approved plan allowed for steeper slope.
N/A	A13.	End walls above barrels (outlet pipe) greater than 48 inch in diameter are fenced to prevent a fall hazard.

(Key for Checklist is as follows: XX Acceptable N/A Not Applicable Inc Incomplete)

#### X. Storm Drainage Systems (Associated with BMP's Only)

(Includes all incidental stormwater drainage conveyance systems associated with SWM/BMP facilities such as onsite or offsite storm drains, open channels, inlets, manholes, junctions, outlet protections, deflectors, etc. These facilities are external to the treatment function of, but are directly associated with drainage to and/or from a constructed SWM/BMP facility. The intent of this portion of the certification is to accurately identify the type and quantity of inflow or outflow points associated with the facility for future reference. The Professional may use his/her own discretion to determine inclusive facilities to meet the intent of this section. As a general rule, storm drainage systems would include incidental facilities to the nearest access structure upslope or downslope from the normal physical limits of the facility or 800 feet of storm drainage conveyance system length, whichever is less.)

XX	SD1.	All requirements of Section II, Minimum Standards, apply to Storm Drainage Systems.
----	------	---

SD2. Horizontal location of all pipe and structures relative to the SWM/BMP facility.

SD3. Type, top elevation and invert elevation of all access type structures (inlets, manholes, etc.).

SD4. Material type, size or diameter, class, invert elevations, lengths and slopes for all pipe segments.

SD5. Class, length, width and depth of riprap and outlet protections or dimensions of special energy dissipation structures.

#### XII. Other Systems (Includes any non-typical, specialty, manufactured or innovative stormwater

management/BMP practices or systems generally accepted for use as or in conjunction with other acceptable stormwater management / BMP practices. Requires evidence of prior satisfactory industry use and prior Environmental Division approval, waiver or exception.)

O1. All requirements of Section II, Minimum Standards, apply to this section.

O2. Certification criteria to be determined on a case-by-case basis by the Environmental Division specific to the proposed SWM/BMP facility.



# **Stormwater Management BMP Drawing/Construction Certification for a Notification of Submission of a Record** (Inspector's Review)

Inspector:	Date:
Joe Buchite	09/07/06

ID Code:	ntv R R	Project: BMP Facility: Plan No.: Assigned County RMP TD Code:
Other:	_	
Tina Cooke	<u> </u>	
Jason Beck	ت ا	
Mike Majdeski	À	

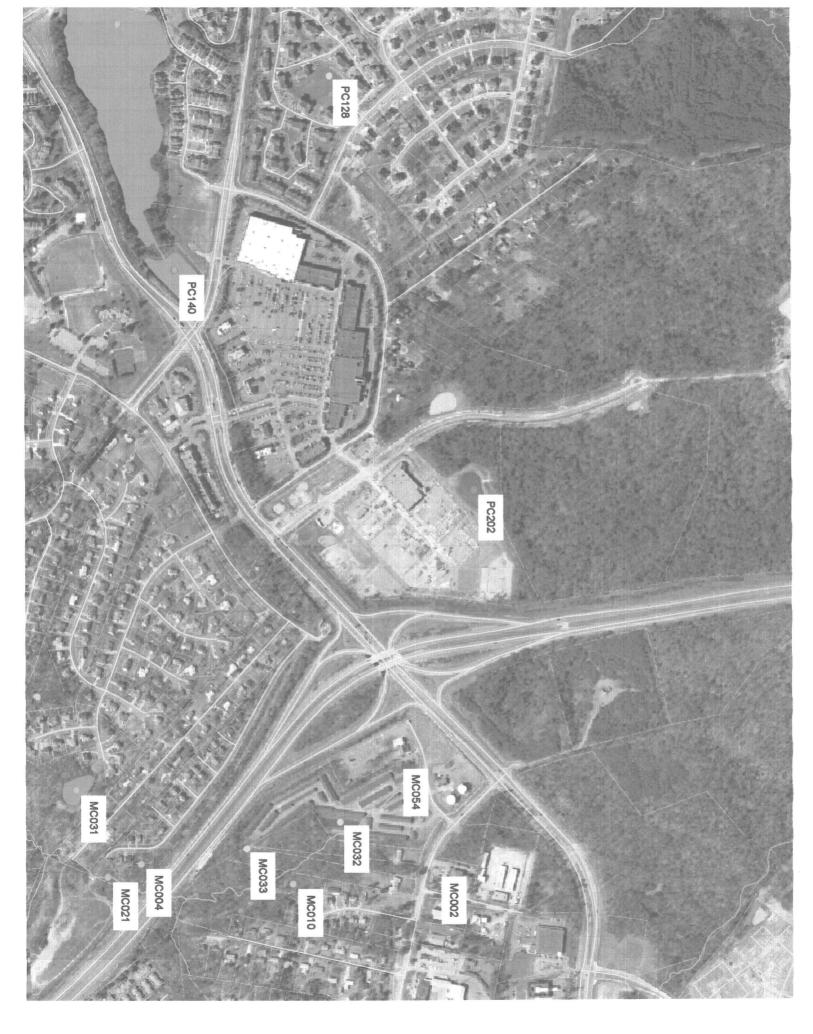
relevant changes were made in the field by the inspector beyond the approved site plan or this record drawing. Please review the information and return it to promptly, with any input, so the engineering group can proceed with the review of certification material. I received a transmittal for a Record Drawing and/or Construction Certification for the above referenced facility on \_\_\_\_\_\_\_\_ Prior to performing a full review of these certification items and a field inspection of the BMP, the information is being first forwarded to you for cursory review and input. This is a first screening to ensure the record drawing accurately portrays field observations by the inspector and to notify the engineering group if any

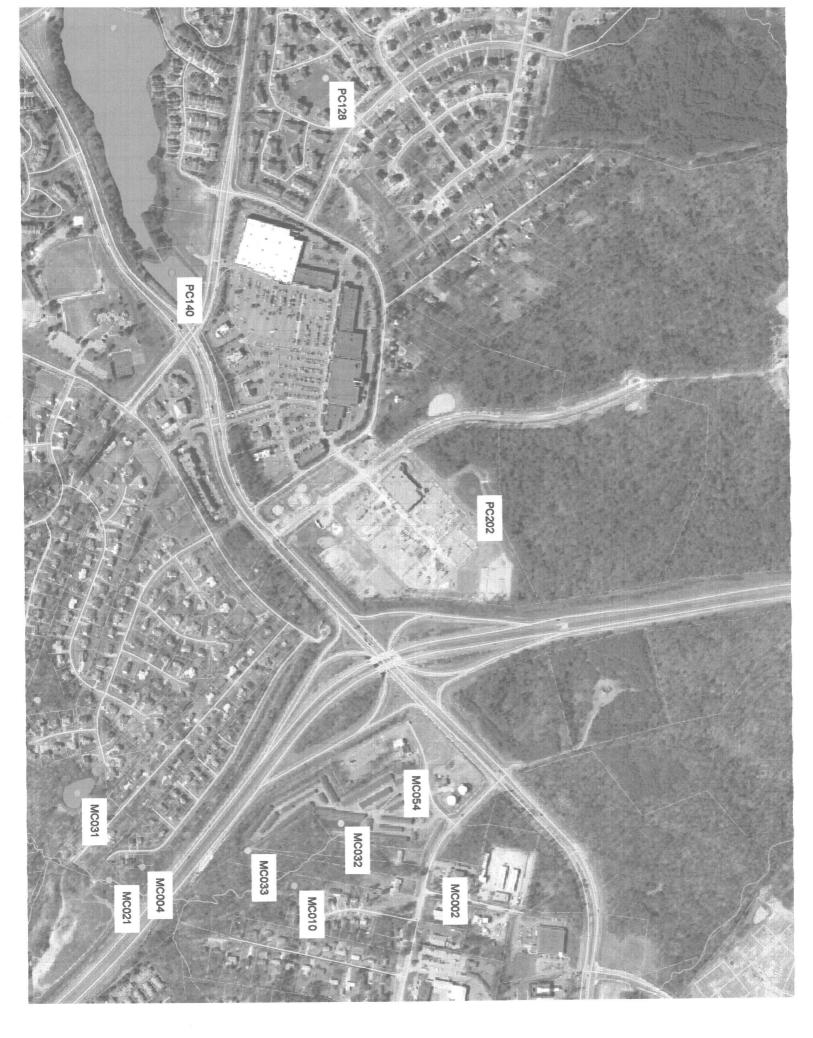
changes were made to the plan which would affect asbuilt review, then this information needs to be relayed verbally to the engineering group. (As an example, say the riser/barrel system for the BMP was approved by the inspector to be moved from that shown on the approved design plan due to poor soil conditions. During record drawing review, this would avoid comments being generated saying that the riser/barrel is in the wrong location or needs to be moved back to Please note that you do not need to perform a detailed field inspection. If the asbuilts do not accurately portray what the inspector saw in the field, or if any where the soils were poor.)

During engineering review, we will look at issues related to the BMP and its primary inflow and outflow conveyance systems, and may make comment on the following areas: Inspection/Maintenance agreement, Record Drawings (RD), Construction Certification (CC) and Construction-Related (CR) field items as it not related to the BMP, you must proceed with closing out these items on your own accord; or alternatively, if needed, these can be added to the BMP pertains to the BMP. If you have any other related non-BMP site issues such as site erosion, stabilization, removal of erosion & sediment controls, etc. that are

Again, only verbal response is necessary

Shared File: AsBuilts\Admin\Final\inspector.form







PC 203

#### James City County, Virginia Environmental Division

# **Stormwater Management / BMP Facilities Record Drawing and Construction Certification**

#### Standard Forms & Instructions

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Issue Date February 1, 2001



#### James City County, Virginia Environmental Division

## Stormwater Management / BMP Facilities Record Drawing and Construction Certification Forms

(Note: In accordance with the requirements of the Chesapeake Bay Preservation Ordinance, Chapter 23, Section 23-10(4), BMP's shall be designed and constructed in accordance with the manual entitled James City County Guidelines for Design and Construction of Stormwater Management BMP's. Erosion and sediment control policy and approved plans generally require that at the completion of the project and prior to release of surety, an "as-built" plan prepared by a registered Professional Engineer or Certified Land Surveyor must be provided for the drainage system for the project, including any Best Management Practice (BMP) facilities. In addition, for BMP facilities involving the construction of an impounding structure or dam embankment, certification is required by a Professional Engineer who has inspected the structure during its construction. Currently there are over 20 water quality type BMP's accepted by the County.)

#### **Section 1 – Site Information:**

Project Name: Structure/BMP Name: Project Location: BMP Location:	WindsorMeade Ma BMP #1 4900 Monticello A Behind Belk store	arket Place eve., & WindsorMea	de Way		
	SP Senting Benk store	- 2	05		
County Plan No.:	<u>sr</u>	- <del>-</del> <u>-</u>	05		
Project Type: Reside  Comm Institut Public Other	ercial Off tional Ind	ice BMP ustrial Zonin adway Land	Map/Parcel No.:  ID Code (if known):  g District:  Use:  Area (sf or acres):	3831800001 <b>PC 20 3</b> MU (Mixed Use Shopping Cente 31.44 Ac.	<del>/                                    </del>
Brief Description of Stormw	rater Management/BN	IP Facility: Type A-	-3 Wet Extended Deter	tion Pond	
Nearest Visible Landmark to	o SWM/BMP Facility	: Belk stor	re		
Nearest Vertical Ground Con  JCC Geodetic Gr Station Number or N	round Control	□ USGS	☐ Temporary	☐ Arbitrary	Other
Datum or Reference	Elevation: NGVE	29			
Control Description	: 3-1/4"	disk in concrete			
•	om Subject Facility: 5	SW			

#### Section 2 – Stormwater Management / BMP Facility Construction Information: ☐ Yes ☐ No □ Unknown PreConstruction Meeting Held for Construction of SWM/BMP Facility: Approx. Construction Start Date for SWM/BMP Facility: □ Unknown Facility Monitored by County Representative during Construction: ☐ Yes ☐ No Name of Site Work Contractor Who Constructed Facility: Name of Professional Firm Who Routinely Monitored Construction: Date of Completion for SWM/BMP Facility: Date of Record Drawing/Construction Certification Submittal: (Note: Record Drawing and Construction Certifications are required within thirty (30) days of the completion of Stormwater Management and/or BMP facility construction. Record Drawings and Construction Certifications must be reviewed and approved by the James City County Environmental Division prior to final inspection, acceptance and bond or surety release.) Section 3 – Owner / Designer / Contractor Information: Owner/Developer: (Note: Site Owner or Applicant responsible for development of the project.) Name: SLN Williamsburg Associates, L.L.C. Mailing Address: 9211 Forest Hill Ave., Suite 110 Richmond, VA 23235 **Business Phone:** 804-320-7600 Fax:804-330-8924 Contact Person: Jim Gresock Title: Design Professional: (Note: Professional Engineer or Certified Land Surveyor responsible for the design and preparation of plans and specifications for the Stormwater Management / BMP facility.) Firm Name: AES Consulting Engineers Mailing Address: 5248 Olde Towne Rd., Suite 1 Williamsburg, VA 23188 **Business Phone:** 757-253-0040 Fax: 757-220-8994 Responsible Plan Preparer: G. Archer Marston, III, P.E. Title: Vice President WindsorMeade Market Place Plan Name: Firm's Project No. 9069-02 Plan Date: 12-29-06 Sheet No.'s Applicable to SWM/BMP Facility: BMP Contractor: (Note: Site Work Contractor directly responsible for construction of the Stormwater Management / BMP facility.) Name: Jack L. Massie Contractor Inc. Mailing Address: 3900 Cokes Lane Williamsburg, VA 23188 Business Phone: 757-566-8643 Fax: 757-566-8566 Contact Person: Scott Massie Site Foreman/Supervisor: Scott Massie Specialty Subcontractors & Purpose (for BMP Construction Only):

#### Section 4 - Professional Certifications:

Certifying Professionals: (Note: A Registered Professional Engineer of Certified Land Surveyor is responsible for preparation of a Record Drawing, sometimes referred to as an As-Built plan, for the drainage system for the project including any Stormwater Management/BMP Facilities. A Registered Professional Engineer is responsible for the inspection, monitoring and certification of Stormwater Management / BMP facilities during its construction.)

#### Record Drawing and Construction Certifications for Stormwater Management / BMP Facilities

#### **Record Drawing Certification**

and stormwater management plan, except as specifically

#### **Construction Certification** Firm Name: AES Consulting Engineers Firm Name: ECS, Ltd. Mailing Address: 5248 Olde Towne Rd., Suite 1 Mailing Address: 108 Ingram Rd., Unit 1 Williamsburg, VA 23188 Williamsburg, VA 23188 Business Phone: 757-253-0040 Business Phone: 757-229-6677 Fax: 757-220-8994 Fax: 757-229-9978 Name: G. Archer Marston, III, P.E. Name: Michael J. Galli . P. 6 Title: Vice President Signature: Date: I hereby certify to the best of my knowledge I hereby certify to the best of my knowledge and belief that this record drawing represents the actual and belief that this Stormwater Management / BMP condition of the Stormwater Management / BMP facility was monitored and constructed in facility. The facility appears to conform with the accordance with the provisions of the approved provisions of the approved design plan, specifications design plan, specifications and stormwater

noted.

(Seal)

management plan, except as specifically

(Seal)

Virginia Registered Professional Engineer Or Certified Land Surveyor

Virginia Registered Professional Engineer

#### Section 4 - Professional Certifications:

Certifying Professionals: (Note: A Registered Professional Engineer of Certified Land Surveyor is responsible for preparation of a Record Drawing, sometimes referred to as an As-Built plan, for the drainage system for the project including any Stormwater Management/BMP Facilities. A Registered Professional Engineer is responsible for the inspection, monitoring and certification of Stormwater Management / BMP facilities during its construction.)

#### Record Drawing and Construction Certifications for Stormwater Management / BMP Facilities

Virginia Registered Professional Engineer

Or Certified Land Surveyor

Record Drawing Certification	Construction Certification
Firm Name: AES Consulting Engineers	Firm Name: ECS, Ltd.
Mailing Address: 5248 Olde Towne Rd., Suite 1	Mailing Address: 108 Ingram Rd., Unit 1
Williamsburg, VA 23188	Williamsburg, VA 23188
Business Phone: 757-253-0040	Business Phone: 757-229-6677
Fax: 757-220-8994	Fax: 757-229-9978
Name: G. Arabar Maratan, III. D.E.	Names Michael I Calli
Name: G. Archer Marston, III, P.E.  Title: Vice President	Name: Michael J. Galli
Title. Vice Fresident	Title:
Signature: ////////////////////////////////////	Signature:
Date: 7/2//06	Date:
<i>(</i>	
I hereby certify to the best of my knowledge and belief that this record drawing represents the actual condition of the Stormwater Management / BMP facility. The facility appears to conform with the provisions of the approved design plan, specifications and stormwater management plan, except as specifically noted.	I hereby certify to the best of my knowledge and belief that this Stormwater Management / BMP facility was monitored and constructed in accordance with the provisions of the approved design plan, specifications and stormwater management plan, except as specifically noted.
G. ARCHER MARSTON III  No. 018232	
(Seal)	(Seal

Virginia Registered

Professional Engineer

#### Section 5 - Record Drawing and Construction Certification Requirements and Instructions:

- PreConstruction Meeting Provides an opportunity to review SWM / BMP facility construction, maintenance and operation plans and address any questions regarding construction and/or monitoring of the structure. The design engineer, certifying professionals (if different), Owner/Applicant, Contractor and County representative(s) are encouraged to attend the preconstruction meeting. Advanced notice to the Environmental Division is requested. Usually, this requirement can be met simultaneously with Erosion and Sediment Control preconstruction meetings held for the project.
- □ A fully completed STORMWATER MANAGEMENT / BMP FACILITIES, RECORD DRAWING and CONSTRUCTION CERTIFICATION FORM and RECORD DRAWING CHECKLIST. All applicable sections shall be completed in their entirety and certification statements signed and sealed by the registered professional responsible for individual record drawing and/or construction certification.
- The Record Drawing shall be prepared by a Registered Professional Engineer or Certified Land Surveyor for the drainage system of the project including any Best Management Practices.
- Construction Certification. Construction of Stormwater Management / BMP facilities which contain impoundments, embankments and related engineered appurtenances including subgrade preparation, compacted soils, structural fills, liners, geosynthetics, filters, seepage controls, cutoffs, toe drains, hydraulic flow control structures, etc. shall be visually observed and monitored by a Registered Professional Engineer or his/her authorized representative. The Engineer must certify that the structure, embankment and associated appurtenances were built in accordance with the approved design plan, specifications and stormwater management plan and standard accepted construction practice and shall submit a written certification and/or drawings to the Environmental Division as required. Soil and compaction test reports, concrete test reports, inspection reports, logs and other required construction material or installation documentation may be required by the Environmental Division to substantiate the certification, if specifically requested. The Engineer shall have the authority and responsibility to make minor changes to the approved plan, in coordination with the assigned County inspector, in order to compensate for unsafe or unusual conditions encountered during construction such as those related to bedrock, soils, groundwater, topography, etc. as long as changes do not adversely affect the integrity of the structure(s). Major changes to the approved design plan or structure must be reviewed and approved by the original design professional and the James City County Environmental Division.
- Record Drawing and Construction Certifications are required within **thirty (30) days** of the completion of Stormwater Management / BMP facility construction. Submittals must be reviewed and accepted by James City County Environmental Division prior to final inspection, acceptance and bond/surety release.

**Dual Purpose Facilities** – Completion of construction also includes an interim stage for Stormwater Management / BMP facilities which serve dual purpose as temporary sediment basins during construction and as permanent stormwater management / BMP facilities following construction, once development and stabilization are substantially complete. For these dual purpose facilities, construction certification is required once the temporary sediment basin phase of construction is complete. Final record drawing and construction certification of additional permanent components is required once permanent facility construction is complete.

Interim Construction Certification is required for those dual purpose embankment-type facilities that are generally ten (10) feet or greater in dam height (\*) and may not be converted, modified or begin function as a permanent SWM / BMP structure for a period generally ranging from six (6) to eighteen (18) months or more from issuance of a Land Disturbance permit for construction.

Interim or final record drawing and construction certifications are not required for temporary sediment basins which are designed and constructed in accordance with current minimum standards and specifications for temporary sediment basins per the Virginia Erosion and Sediment Control Handbook (VESCH); have a temporary service life of less than eighteen (18) months; and will be removed completely once associated disturbed areas are stabilized, <u>unless</u> a distinct hazard to the public's health, safety and welfare is determined by the Environmental Division due to the size or presence of the structure or due to evidence of improper construction.

(\*Note: Dam Height as referenced above is generally defined as the vertical distance from the natural bed of the stream or waterway at the downstream toe of the embankment to the top of the embankment structure in accordance with 4VAC50-20-30, Virginia Impoundment Structure Regulations and the Virginia Dam Safety Program.)

- Record Drawings shall provide, at a minimum, all information as shown within these requirements and the attached **RECORD DRAWING CHECKLIST** specific to the type of SWM/BMP facility being constructed. Other additional record data may be formally requested by the James City County Environmental Division. (Note: Refer to the current edition of the James City County Guidelines for Design and Construction of Stormwater Management BMP's manual for a complete list of acceptable BMP's. Currently there are over 20 acceptable water quality type BMP's accepted by the County.)
- Record Drawings shall consist of blue/black line prints and a reproducible (mylar, sepia, diazo, etc.) set of the approved stormwater management plan including applicable plan views, profiles, sections, details, maintenance plans, etc. as related to the subject SWM / BMP facility. The set shall indicate "RECORD DRAWING" in large text in the lower right hand corner of each sheet with record elevations, dimensions and data drawn in a clearly annotated format and/or boxed beside design values. Approved design plan values, dimensions and data shall not be removed or erased. Drawing sheet revision blocks shall be modified as required to indicate record drawing status. Elevations to the nearest 0.1' are sufficiently accurate except where higher accuracy is needed to show positive drainage. Certification statements as shown in Section 4 of the Record Drawing and Construction Certification Form, or similar forms thereof, and professional signatures and seals, with dates matching that of the record drawing status in the revision or title block, are also required on all associated record drawing plans, prints or reproducibles.
- Submission Requirements. Initial and subsequent submissions for review shall consist of a minimum of one (1) blue/black line set for record drawings and one copy of the construction certification documents with appropriate transmittal. Under certain circumstances, it is understood that the record drawing and construction certification submissions may be performed by different professional firms. Therefore, record drawing submission may be in advance of construction certification or vice versa. Upon approval and prior to release of bond/surety, final submission shall include one (1) reproducible set of the record drawings, one (1) blue/black line set of the record drawings and one (1) copy of the construction certification. Also for current and/or future incorporation into the County BMP database and GIS system, it is requested that the record drawings also be submitted to the Environmental Division on a diskette or CD-ROM in an acceptable electronic file format such as \*.dxf, \*.dwg, etc. or in a standard scanned and readable format. The electronic file requirement can be discussed and coordinated with Environmental Division staff at the time of final submission.

(Key for Checklist is as follows: XX Acceptable N/A Not Applicable Inc Incomplete) Methods and Presentation: (Required for all Stormwater Management / BMP facilities.)  $\times \times$ All constructed facilities meet approved design plans, unless otherwise shown. Record information or deviations from approved design plan shown in clearly annotated format and/or boxed beside design values. 2. Elevations to the nearest 0.1' unless higher accuracy is needed to show positive drainage. All plan sheets labeled with "RECORD DRAWING" in large text in lower right hand corner (Approved County Plan Number and BMP ID Code can be included if known). All plans sheet revision blocks modified to indicate date and record drawing status. 5. All plan sheets have certification statements and certifying professional's signature and seal. П. Minimum Standards: (Required for all Stormwater Management / BMP facilities, as applicable.) All requirements of Section I (Methods and Presentation) apply to this section. Plan Views: Show general location, arrangement and dimensions. Location and alignment shall generally match approved design plans. Profile or elevations along top or berm of the facility. At a minimum, elevations are required at each end, at intervals not to exceed 50 feet and where low spots may be present. Top of embankment or berm elevations must be no less than design elevation plus any settlement allowances. Top widths, berm widths and embankment side slopes. Show length, width and depth of facility or grading, contours or spot elevations as required to verify permanent pool and design storage volumes were met or were reasonably close to the approved design. Evaluation of as-built grading, contours, spot elevations, or cross-sections, may be necessary by the professional to ensure approved design configurations, depths and volumes were closely maintained. If grading or elevations are significantly different from the approved plan, the Environmental Division shall be contacted immediately to determine whether the variation is acceptable or whether further evidence will be required. Facilities which do not closely resemble approved plan grades, elevations or configurations may require regrading by the Contractor; check volumetric computations; and/or a check hydraulic routing to ensure approved design water surface elevations, discharges or freeboard were closely maintained. LL 6. Cross-section of the embankment through the principal spillway or outlet barrel. Must extend at least 100 ft. downstream of the pipe outlet or to recorded site property line, whichever is closer. Proper correlation is required between principal spillway (control structure) crest, emergency spillway crest, orifice and weirs and the top of the dam or facility. All elevations and dimensions must reasonably match the design plan or be sequentially relative to each other and the facility must reflect the required design storage volume(s) and/or design depth. Profile or elevations along the entire centerline of the emergency spillway. Emergency spillway

Elevation of the principal spillway crest or outlet crest of the structure.

may be steeper, but no flatter or narrower than design.

<u>**</u>	9.	Primary control structure (riser) diameter or dimensions, height, type of material and base size. Indicate provisions for access that are present such as steps, ladders, etc.
XX	10.	Dimensions, locations and elevations of outlet orifices, weirs, slots and drains.
Les tak Gertak Gerdeck	11.	Type and size of anti-vortex and trash rack device. Height, diameter, dimensions, bar spacings (if applicable) and elevations relative to the principal spillway crest. Indicate if lockable hatch is present or not.
Gestah	12.	Type, location, size and number of anti-seep collars or documentation of other methods utilized for seepage control. May need to obtain this information during construction.
Credech	13.	Top of impervious core embankment, core trench limits and elevation of cut-off trench bottom.  May need to obtain this information during construction.
XX	14.	Elevation of the principal spillway barrel (outlet pipe) inlet and outlet invert.
XX	15.	Outlet barrel diameter, length, slope, type and thickness class of material and type of flared end sections, headwall or endwall.
XX	16.	Outfall protection dimension, type and depth of rock and if underlain filter fabric is present.
XX XX	17.	BMP interior and periphery landscaping zones conform with arrangements and requirements of the approved design plan.
XX	18.	Maintenance plan taken from approved design plan transposed onto record drawing set.
太太	19.	Fencing location and type, if applicable to facility.
XX	20.	BMP vicinity properly cleaned of stockpiles and construction debris.
<u> </u>	21.	No visual signs of erosion or channel degradation immediately downstream of facility.
<u> </u>	22.	Any other information formally requested by the Environmental Division specific to the constructed SWM/BMP facility.

(Key for Checklist is as follows: XX Acceptable N/A Not Applicable Inc Incomplete) III. Group A – Wet Ponds (Includes A-1 Small Wet Ponds; A-2 Wet Ponds; A-3 Wet Ext Det Ponds.) XXA1. All requirements of Section II, Minimum Standards, apply to Group A facilities. XXPrincipal spillway consists of reinforced concrete pipe with O-Ring gaskets for watertight joint A2. construction. HDPR per approved plan. Sediment forebays or pretreatment devices provided at inlets to pond. Generally 4 to 6 ft. deep. A3. A4. Access for maintenance and equipment is provided to the forebay(s). Access corridors are at least 12 ft. wide, have a maximum slope of 15 percent and are adequately stabilized to withstand heavy equipment or vehicle use. Adequate fixed vertical sediment depth markers installed in the forebay(s) for future sediment N/A A5. monitoring purposes. Pond liner (if required) provided. Either clay liners, polyliners, bentonite liners or use of chemical N/A A6. soil additives based on requirements of the approved plan. N/A A7. Minimum 6 percent slope safety bench extending a minimum of 15 feet outward from normal pool edge and/or an aquatic bench extending a minimum of 10 feet inward from the normal shoreline with a maximum depth of 12 inches below the normal pool elevation, if applicable, per the approved design plans. (Note: Safety benches may be waived if pond side slopes are no steeper than 4H:1V). XXA8. No trees are present within a zone 15 feet around the embankment toe and 25 feet from the principal spillway structure. Wet permanent pool, typically 3 to 6 feet deep, is provided and maintains level within facility. XXA9. XXLow flow orifice has a non-clogging mechanism. A10. XXA11. A pond drain pipe with valve was provided. Pond side slopes are not steeper than 3H:1V, unless approved plan allowed for steeper slope. XXA12. N/A End walls above barrels (outlet pipe) greater than 48 inch in diameter are fenced to prevent a fall A13.

(Key for Checklist is as follows: XX Acceptable N/A Not Applicable Inc Incomplete)

#### X. Storm Drainage Systems (Associated with BMP's Only)

(Includes all incidental stormwater drainage conveyance systems associated with SWM/BMP facilities such as onsite or offsite storm drains, open channels, inlets, manholes, junctions, outlet protections, deflectors, etc. These facilities are external to the treatment function of, but are directly associated with drainage to and/or from a constructed SWM/BMP facility. The intent of this portion of the certification is to accurately identify the type and quantity of inflow or outflow points associated with the facility for future reference. The Professional may use his/her own discretion to determine inclusive facilities to meet the intent of this section. As a general rule, storm drainage systems would include incidental facilities to the nearest access structure upslope or downslope from the normal physical limits of the facility or 800 feet of storm drainage conveyance system length, whichever is less.)

SD1. All requirements of Section II, Minimum Standards, apply to Storm Drainage Systems.

XX SD2. Horizontal location of all pipe and structures relative to the SWM/BMP facility.

SD3. Type, top elevation and invert elevation of all access type structures (inlets, manholes, etc.).

SD4. Material type, size or diameter, class, invert elevations, lengths and slopes for all pipe segments.

SD5. Class, length, width and depth of riprap and outlet protections or dimensions of special energy dissipation structures.

XII. Other Systems (Includes any non-typical, specialty, manufactured or innovative stormwater

management/BMP practices or systems generally accepted for use as or in conjunction with other acceptable stormwater management / BMP practices. Requires evidence of prior satisfactory industry use and prior Environmental

Division approval, waiver or exception.)

O1. All requirements of Section II, Minimum Standards, apply to this section.

O2. Certification criteria to be determined on a case-by-case basis by the Environmental Division

specific to the proposed SWM/BMP facility.

#### **AES CONSULTING ENGINEERS**

Engineering, Surveying, and Planning
5248 Olde Towne Road, Suite 1

5248 Olde Towne Road, Suite 1 WILLIAMSBURG, VIRGINIA 23188

> Phone: (757) 253-0040 Fax: (757) 220-8994

### LETTER OF TRANSMITTAL

ATTN:	Scott Thomas		DATE 7/21/06	JOB NO.	
			7/21/06 FROM:	9069-02	
CO.:	James City Coun	ty Env.	Gwen Scha	atzman	
Address:	101-E Mounts Ba	y Rd.	RE WindsorMeaderMarippace1//CI)		
	Williamsburg, VA	23185	Williasolvicado ividi	<b>RECEIVED</b>	
cc:				31	
WE ARE	SENDING YOU THE	FOLLOWING ITEMS:	☐ Attached ☐ Under separate cover	ENVIRONMENTAL ENVIRONMENTAL DIVIS	
	⊠ Original(s)      ⊠ Prin	t(s)	Specification(s)	Change Order	
	☐ Copy of letter(s)	Other:			
COPIES 2	DATE No. of Pag 4/28/05 3	Record Drawings f	DESCRIPTION for BMP		
2	1,29,00	BMP Certification	O. DIVII		
THESE A	ARE TRANSMITTED a	s checked below:			
☐ Fo	r your approval	☐ For your signature	☐ For review an	d comment	
	r your use	☐ As you requested	 ☐ As requested		
	her:		_ ,		
- <del>-</del>	_				
REMARKS:		SP-150-03 SP-00 Z-05 >	Ameno#1		
			PC203	•	

# WindsorMeade Market Place

# BMP RECORD DRAWINGS

# LEGEND

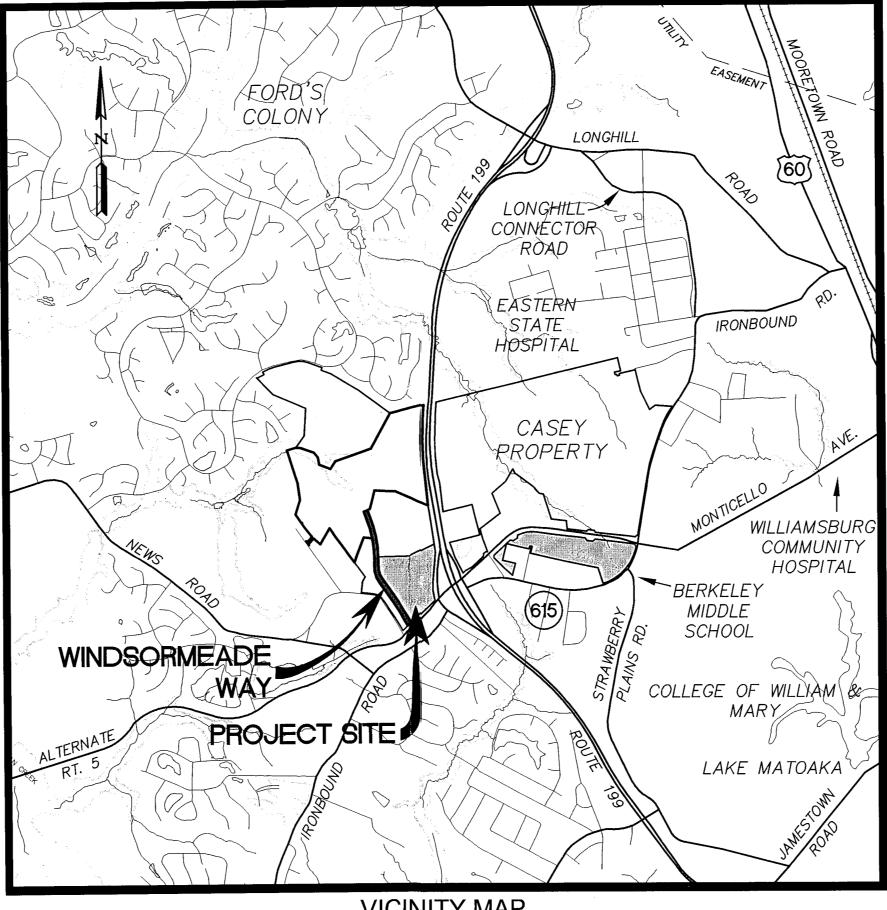
PROPOSED PROPOSED **BLOW-OFF ASSEMBLY** GRAVITY SEWER CLEAN OUT WATER METER GRAVITY SEWER (BY OTHERS) CENTERLINE BASELINE STORM SEWER FORCE MAIN ---- EX. FM ----G DITCH/SWALE GROUND ELEVATION EXISTING CONTOUR ELEV.

# NOTES:

- THE SITE IS CURRENTLY ZONED MIXED USE WITH PROFFERS. FOR PROFFERS REFERENCE JCC CASE NO. Z-03-01 AND MP-02-97 AND CASE NO. Z-05-03 AND MP-06-03 APPROVED BY THE BOARD OF SUPERVISORS ON DECEMBER 11, 2001.
- CONTRACTOR SHALL BE RESPONSIBLE FOR CONTACTING 'MISS UTILITY' FOR EXISTING UTILITY LOCATIONS PRIOR TO COMMENCING
- CONTRACTOR SHALL BE RESPONSIBLE FOR THE COORDINATION OF CONSTRUCTION EFFORTS WITH THE VIRGINIA POWER COMPANY, VERIZON TELEPHONE, APPROPRIATE CABLE COMPANY AND OTHERS THAT MAY BE REQUIRED.
- THE CONTRACTOR SHALL SATISFY HIMSELF AS TO ALL SITE CONDITIONS PRIOR TO CONSTRUCTION
- THE CONTRACTOR IS RESPONSIBLE FOR OBTAINING ALL NECESSARY PERMITS PRIOR TO COMMENCEMENT OF WORK TO INCLUDE, BUT NOT LIMITED TO, JAMES CITY COUNTY LAND DISTURBANCE, VDOT LAND USE PERMIT, AND ANY DEMOLITION PERMITS.
- 6. EXISTING UTILITY LOCATIONS INDICATED ARE APPROXIMATE. FIELD VERIFY PRIOR TO COMMENCING THE WORK.
- 7. ALL UTILITIES WILL BE PLACED UNDERGROUND
- 8. JCSA SHALL BE GRANTED ACCESS EASEMENTS TO WATER AND SEWER LOCATED WITHIN PRIVATE RIGHT-OF-WAYS.
- 9. A PRECONSTRUCTION CONFERENCE SHALL BE HELD ON-SITE BETWEEN THE COUNTY, THE PROJECT ENGINEERS AND THE CONTRACTOR PRIOR TO ISSUANCE OF A LAND DISTURBING PERMIT.
- 10. ALL SANITARY SEWER AND WATER DISTRIBUTION FACILITIES MUST HAVE A MINIMUM HORIZONTAL SEPARATION DISTANCE OF 5' BETWEEN IT AND ALL OTHER FIXED STRUCTURES SUCH AS: DROP INLETS, LIGHT POLES, STORM SEWER PIPES, ETC.
- 11. THE CONTRACTOR IS REQUIRED TO SECURE ALL NECESSARY PERMITS FOR FOR THE ABANDONMENT OR DEMOLITION OF ALL EXISITING WELLS/WATERLINES AND SEPTIC FIELDS IN ACCORSANCE WITH JAMES CITY COUNTY VIRGINIA DEPARTMENT OF HEALTH REGULATIONS. CONTACT VIRGINIA DEPARTMENT OF HEALTH AT 757-253-4813
- 12. VERIFY ALL DIMENSIONS AND NOTIFY JAMES CITY SERVICE AUTHORITY PRIOR TO ANY EXCAVATION OR DEMOLITION WITHIN
- 13. PARKING SPACES SHALL BE DELINEATED BY PAVEMENT STRIPING. HANDICAP PARKING. SPACES SHALL BE DESIGNATED BY ABOVE GROUND SIGNS PER USBC REQUIREMENTS.
- 14. THE TOPOGRAPHIC DATA REPRESENTED ON THIS DRAWING IS SUPPLIED BY OWNER/DEVELOPER. CONTOUR INTERVAL = 2 FEET.
- 15. ALL SECURITY LIGHTING IS TO BE LOCATED A MINIMUM OF 10' OFF THE EDGE OF PAVEMENT AND SHALL NOTE BE POSITIONED
- 16. ALL COMPONENTS OF THE WATER DISTRIBUTION AND SANITARY SEWER SYSTEM SHALL BE INSTALLED AND TESTED IN ACCORDANCE WITH THE LATEST EDITION OF THE AUTHORITY STANDARDS AND SPECIFICATIONS FOR WATER DISTRIBUTION AND SANITARY SEWER SYSTEMS, THE HRPDC REGIONAL STANDARDS, AND THE COMMONWEALTH OF VIRGINIA WATERWORKS AND SEWERAGE REGULATIONS. THE CONTRACTOR SHALL USE ONLY NEW MATERIALS, PARTS AND PRODUCTS ON ALL PROJECTS. ALL MATERIALS SHALL BE STORED SO AS TO ASSURE THE PRESERVATION OF THEIR QUALITY AND FITNESS FOR THE WORK. A COPY OF THE JCSA STANDARDS AND REGIONAL STANDARDS MUST BE KEPT ON-SITE BY THE CONTRACTOR DURING THE FULL TIME OF INSTALLING, TESTING, AND CONVEYING THE FACILITIES TO JCSA.
- 17. STORM STRUCTURES, SEWER AND BEDDING SHALL CONFORM TO THE VDOT ROAD AND BRIDGE STANDARDS AND VDOT SPECIFICATIONS. ALL PIPE BEDDING SHALL BE IN ACCORDANICE WITH PB-1 AND MANUFACTURER SPECS. AND GUIDELINES, AND MANHOLES DEEPER THAN 4 FEET SHALL HAVE STEPS (ST-1). ALL REINFORCED CONCRETE PIPE (RCP) SHALL BE CLASS III UNLESS OTHERWISE NOTED. STORM SEWER OUTSIDE OF VDOT R.O.W. CAN BE HIGH DENSITY POLYETHYLENE (HDPE).
- 18. ALL EXISTING STRUCTURES LOCATED ON THE SITE ARE TO BE DEMOLISHED AND WILL REQUIRE A DEMOLITION PERMIT. THIS PERMIT CAN BE ACQUIRED FROM THE JAMES CITY COUNTY CODE COMPLIANCE DEPARTMENT TELEPHONE NUMBER:
- 19. NO TREES, SHRUBS, FENCES OR OBSTACLES SHALL BE PLACED WITHIN A JCSA EASEMENT WHICH WOULD RENDER THE EASEMENT INACCESSIBLE BY EQUIPMENT. SHRUBS SHALL BE A MINIMUM OF 5 FEET, AND TREES A MINIMUM OF 10 FEET, FROM THE CENTER OF WATER AND SEWER PIPELINES.
- 20. CONTACT MR. SAL SIBILIA 72 HOURS IN ADVANCE OF ALL PAVEMENT MARKINGS/SIGN INSTALLATIONS AT (757) 925-1679.
- 21. ALL SIGNAGE SHALL BE IN ACCORDANCE WITH ARTICLE II, DIWISION 3 OF THE JAMES CITY COUNTY ZONING ORDINANCE.
- 22. OUTSIDE SALES AND STORAGE OF MERCHANDISE IS PROHIBITED.
- 23. HVAC EQUIPMENT AND OTHER UTILITIES, DOWNSPOUTS, AND GUTTERS SHALL BE PAINTED TO MATCH THE EXTERIOR COLOR OF THE BUILDING SURFACE MATERIAL COLOR. BASES OF THE LIGHT POLES SHOULD BE PINTED TO MATCH THE COLOR OF
- 24. ONLY JCSA PERSONNEL ARE AUTHORIZED TO OPERATE VALVIES ON EISTING JCSA WATER MAIN.
- 25. WATER METERS MUST BE LOCATED A MINIMUM OF 2' FROM SIDEWALKS AND BACK OF CURBS AND 18" FROM EDGE OF DRIVEWAYS.
- 26. THE OWNER SHALL IMPLEMENT AN ANNUAL PERFORMANCE EVALUATION/INSPECTION OF THE BACKFLOW PREVENTION DEVICE AND COORDINATE WITH JOHN WILSON, JCSA UTILITY SPECIAL COORDINATOR, AT (757) 259-4138. THE BACKFLOW PREVENTER SHALL BE TESTED, MAINTAINED, AND OPERATED IN ACCORDANCE WITH JCSA STANDARDS.

JCC# SP-2-05 AMENDMENT TO JCC# SP-150-03

## JAMES CITY COUNTY, VIRGINIA

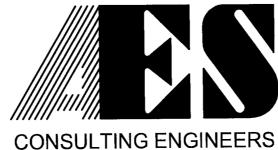


VICINITY MAP SCALE: 1"=2000"

DECEMBER 29, 2003 PROJECT NO.: 9069-02

SITE PLAN AMENDMENT: 1-12-05

"THE SANITARY SEWER, WATER, AND DRAINAGE STRUCTURE LOCATIONS AND GRADES SHOWN ON THESE DRAWINGS, ARE ACCURATE AND COMPLETE MARSTON, III TO THE BEST OF MY KNOWLEDGE AND BELIEF AND I CERTIFY THAT I, OR MY AGENT, HAVE MADE SUFFICIENT INSPECTION TO ENSURE THE ACCURACY OF THIS STATEMENT." DATE ARCHER G. MARSTON III



WILLIAMSBURG • RICHMOND

5248 Olde Towne Road, Suite 1 Williamsburg, Virginia 23188 (757) 253-0040 Fax (757) 220-8994

SITE PLAN AMENDMENT (AMENDMENT TO SP #150-03, APPROVED NOVEMBER 12, 2004) THE FOLLOWING IS A DESCRIPTION OF THE REVISIONS MADE TO THE PLAN UNDER THE SITE PLAN AMMENDMENT AND THE REVISED FOOTPRINT OF BUILDING #5. ADDED A SANITARY LATERAL FOR THIS BUILDING. REVISED RELATIVE "REQUIRED" PARKING

COUNTS. GRADING IN THIS AREA WAS ADJUSTED TO ACCOMODATE NEW FOOTPRINT (FIRST SUBMITTAL.) ADJUSTED 10" LOADING DOCK OUTFALL ON PLANS AND ON WATERLINE PROFILE "D" AND SANITARY PROFILE MH#7 TO MH#3 (SECOND SUBMITTAL.)

2. ADDED DUMPSTER SOUTH OF BUILDING #8. IN CONJUNCTION WITH THIS DUMPSTER, ALSO ADDED STAIRS AND A RETAINING WALL. REVISED GRADING TO ACCOMODATE DUMPSTER AND WALL (FIRST SUBMITTAL.)

3. ADDED A PRIVATE 6" FIRE LINE, A DETECTOR CHECK VALVE ASSEMBLY AND A POST INDICATOR VALVE TO BUILDING #8 AND 4" LINE TO A FIRE SERVICE CONNECTION. ALSO ADDED A NOTE RELATIVE TO THE BACKFLOW PREVENTION AT BUILDING #8. 4" LINE IS SHOWN ON THE SEWER LINE PROFILE ON SHEET 14. (SECOND SUBMITTAL)

4. ADDED A MONUMENT SIGN AT THE FRONT OF THE SITE (SOUTHEAST SIDE) (FIRST SUBMITTAL.)

5. REMOVED THE SMALL BUILDING ADJACENT TO THE SOUTH SIDE OF BUILDING #1 (FIRST SUBMITTAL.)

6. ADJUSTED FIRE LINE, SANITARY SEWER LATERAL AND WATER SERVICE LINE TO BETTER SERVE BUILDING 1 & 2 (FIRST SUBMITTAL.)

7. ADDED NOTES TO THE COVER SHEET REGARDING REVIEW OF PLANS BY THE JAME'S CITY COUNTY PLANNING COMMISSION AND

9. ADDED PRIVATE STORM DRAINAGE EASEMENTS TO THE PLANS FOR ALL MAJOR STORM SEWER CONVEYING WATER ACROSS THE SITE TO THE BMP (SECOND SUBMITTAL) ALSO INCLUDED THE NATURAL OPEN SPACE EASEMENTS ON SHEETS 3, 4 AND 6 (SECOND SUBMITTAL)

10. MODIFIED OUTFALL STONE AT BMP FROM CLASS AT RIPRAP TO CLASS I RIPRAP (SECOND SUBMITTAL.)

11. ADDED INTERNAL PROPERTY LINES TO SHEETS 2, 3, 5, 6, & 7 (SECOND SUBMITTAL)

12. ADDED A POST INDICATOR VALVE TO THE 8" FIRE SERVICE WATERLINE TO THE MAINTENANCE BUILDING AT THE REAR (NORTH SIDE) OF THE SITE (SECOND SUBMITTAL)

#### INDEX OF SHEETS

SHEET NO.	DESCRIPTION
1	COVER SHEET
2	ENVIRONMENTAL INVENTORY PLAN
3	OVERALL SITE LAYOUT PLAN
4	OVERALL UTILITY PLAN
5	SITE AND UTILITY PLAN
6	SITE AND UTILITY PLAN
7	SITE AND UTILITY PLAN
8	BMP POND AS-BUILT
9	GRADING, DRAINAGE, AND E&S PLAN
10	GRADING, DRAINAGE, AND E&S PLAN
11	ROAD PLAN
12	EROSION & SEDIMENT CONTROL PLAN-PHASE I
13	WATER & SEWER PROFILES
14	WATER & SEWER PRIOFILES
15	WATER LINE PROFILE'S
16	NOTES & DETAILS
17	NOTES & DETAILS
18	BMP NOTES & DETAILS
19	LIGHTING PLAN

OWNER INFORMATION: C.C. CASEY, LTD. CO.

721 RICHMOND ROAD WILLIAMSBURG, VIRGINIA. 23185-3541 TELEPHONE: (757) 229-3702

**DEVELOPER INFORMATION:** SLN WILLIAMSBURG ASSOCIATES, L.L.C. 9211 FOREST HILL AVENUE, SUITE 110 RICHMOND, VIRGINIA, 23235 CONTACT: JIM GRESOCK TELEPHONE: (804) 320-7600

FAX: (804) 330-8924

#### CERTIFIED RESPONSIBLE LAND DISTURBER

AES CONSULTING ENGINEERS 5248 OLDE TOWNE ROAD, SUITE 1 WILLIAMSBURG, VIRGINIA. 23188 TELEPHONE: 757-253-0040

#### SITE DATA

(38-3)(1-02), (38-3)(1-34), (38-3)(1-07)TAX MAP PARCEL No. (38-3)(1-05), (38-3)(1-06), (38-3)(1-08)MU (MIXED USE) WITH PROFFERS 100.00 % 1,369,671 S.F.± 31.44 AC.± TOTAL PROJECT AREA: 49.40 % IMPERVIOUS AREA: 50.60 % GREEN SPACE: 1,087,693 S.F.± 24.97 AC.± DISTURBED AREA: FEMA PANEL NUMBER 510201 0035 B, DATED 2/6/91 FLOOD HAZARD MAP: NOTE: SITE IS LOCATED IN ZONE 'X' (AREAS DETERMINED TO BE OUTSIDE THE 500 YEAR FLOOD PLAIN)

COUNTY WATERSHED:

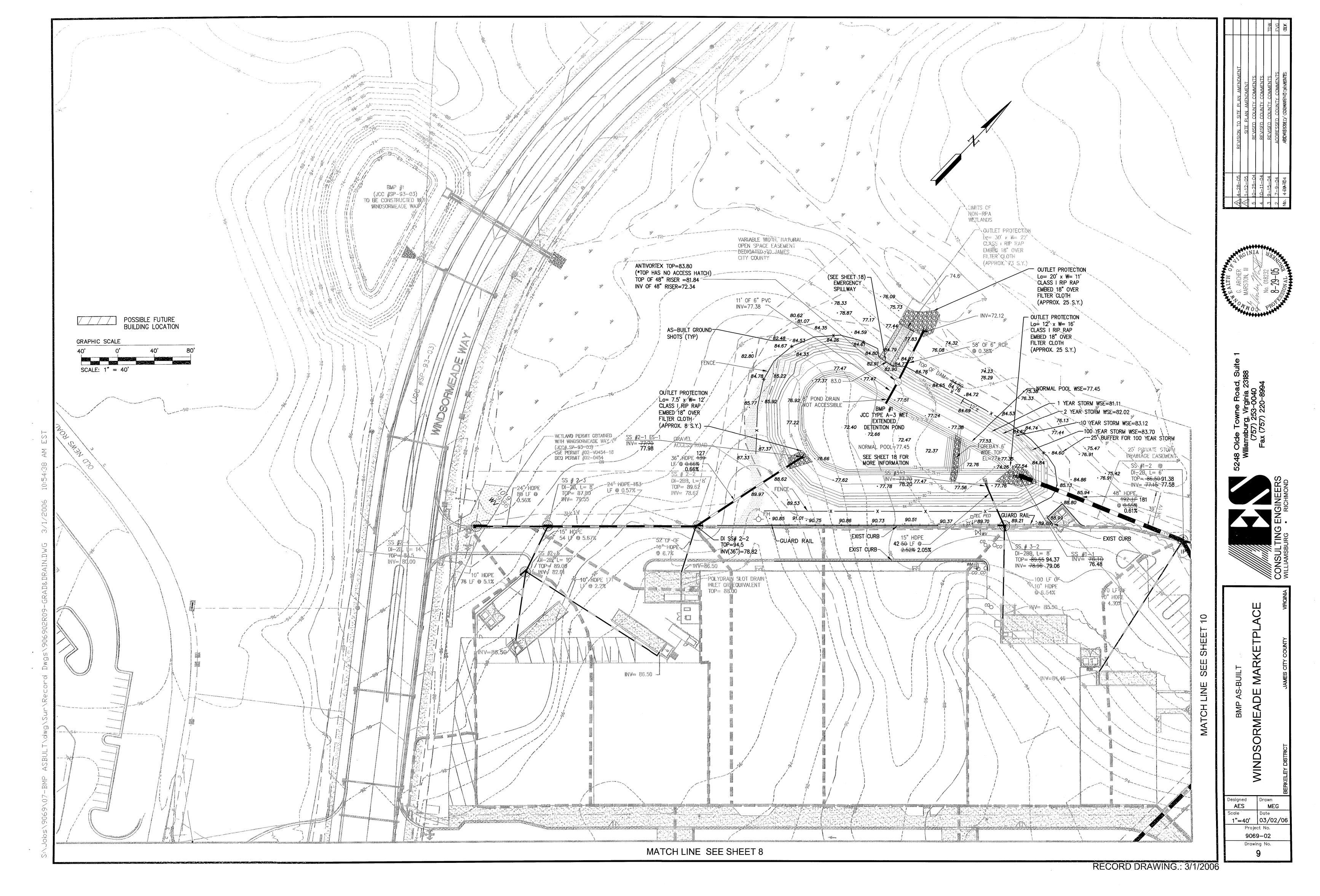
THIS PROJECT IS SITUATED IN SUBWATERSHEDS 209 AND 210. COUNTY CATCHMENTS ARE 209-101-1 AND 210-202-1 OF THE POWHATAN CREEK WATERSHED.

THIS PLAN WAS REVIEWED ON FEBRUARY 2, 2004 BY JAMES CITY COUNTY PLANNING COMMISSION IN ACCORDANCE WITH SECTION 24-147 (a)(1)(d) OF ZONING ORDINANCE

NOTE:
THE PROPOSED AMENDMENTS OF THIS PLAN WERE REVIEWED BY THE NEW TOWN DESIGN REVIEW BOARD AT A MEETING ON 12/16/04

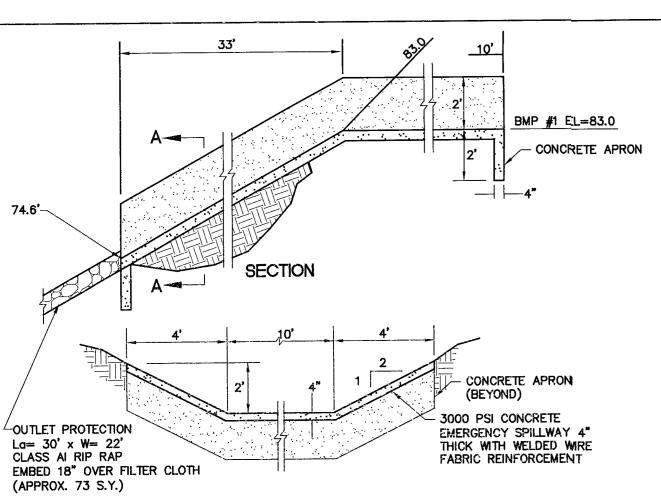
	4/28/05	REVISION TO SITE PLAN AMENDMENT	AES
	1/12/05	SITE PLAN AMENDMENT	AES
5	10/25/04	REVISED COUNTY COMMENTS	AES
4	10/11/04	REVISED COUNTY COMMENTS	AES
3	09/15/04	REVISED COUNTY COMMENTS	AES
2	07/09/04	ADDRESSED COUNTY COMMENTS	AES
1	04/09/04	ADDRESSED COUNTY COMMENTS	AES
No.	DATE	REVISION / COMMENT / NOTE	BY

RECORD DRAWING.: 3/1/2006

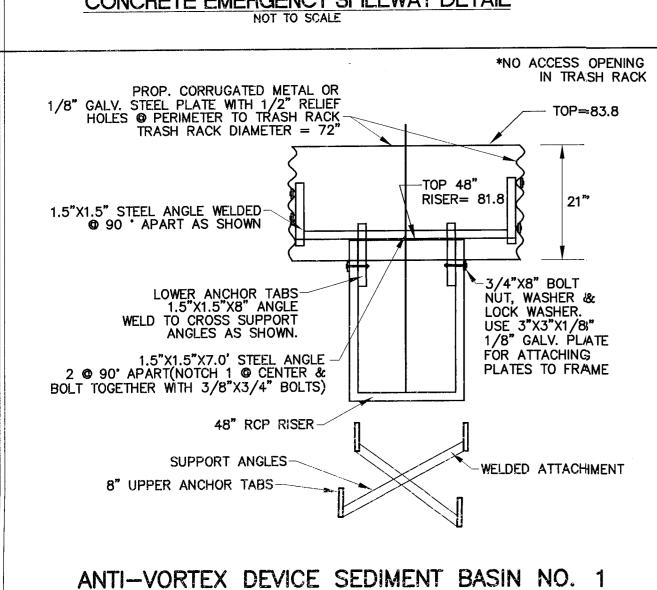


#### CONVERSION OF SEDIMENT BASINS INTO BMP FACILITIES

BMP FACILITIES WILL INITIALLY BE CONSTRUCTED AS SEDIMENT BASINS REQUIRING EXCAVATION TO PROVIDE ADEQUATE STORAGE. ONCE J.C.C. ENVIRONMENTAL IDIVISION GIVES CONCURRENCE TO REMOVE THE SEDIMENT BASIN FACILITIES, ANY EXCESS EARTH OR SEDIMENT SHALL BE REMOVED AND DISPOSED OF BY CONTRACTOR. REMOVE TEMPORARY ITEMS FROM BASIN 1 AND INSTALL RIP—RAP FOREBAY. THE SEDIMENT BASIN SHALL BE REGRADED AND SEEDED.

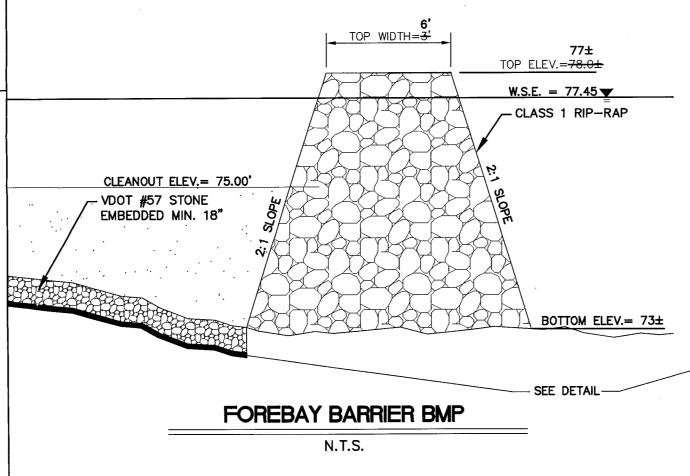


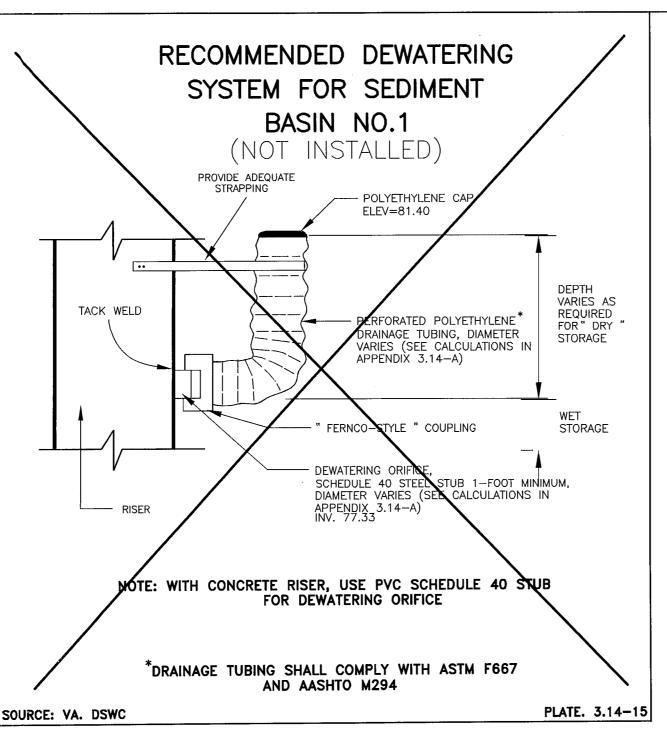
SECTION A-A
CONCRETE EMERGENCY SPILLWAY DETAIL
NOT TO SCALE

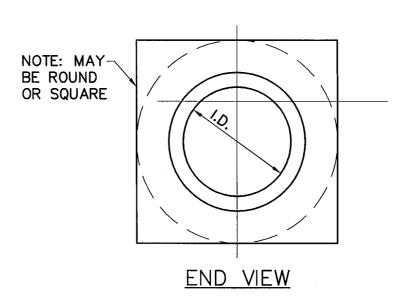


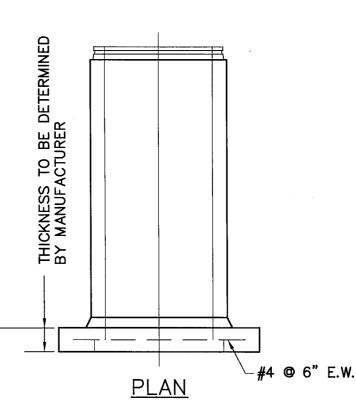
#### NOTE:

IT IS UNDERSTOOD THAT PREPARATION OF RECORD DRAWINGS AND CONSTRUCTION CERTIFICATIONS AS REQUIRED FOR PROJECT FACILITIES MAY NOT NECESSARILY BE PERFORMED BY THE PLAN PREPARER. THESE COMPONENTS MAY BE PERFORMED BY OTHERS. PLEASE REFER TO NOTE 7 OF THE GENERAL NOTES (THIS SHEET) FOR CONSTRUCTION OF STORMWATER BASINS.









NOTE: PRE-CAST COLLAR TO COMPLY WITH VESCH MINIMUM STANDARD AND SPECIFICATION 3.02

PRE-CAST CONCRETE
ANTI-SEEP COLLAR
N.T.S.

#### STORMWATER MANAGEMENT/ BMP FACILITY MAINTENANCE PLAN

PROPER MAINTENANCE OF THIS FACILITY IS ENCOURAGED TO PREVENT THE INTRODUCTION OF DEBRIS AND SEDIMENT IN TO THE FACTILITY, SPILLWAY(S) AND DOWNSTREAM WATERWAYS. FOLLOWING INSTALLATION OF THE FACILITY AND ESTABLISHMENT OF VEGETATION IN DISTURBED AREAS, INSPECTIONS FOR SEDIMENT BUILDUPS WILL BE PERFORMED AT LEAST QUARTERLY. IT IS ANTICIPATED THAT UNDER NORMAL CONDITIONS, SEDIMENT REMOVAL FROM THE FACILITY WILL BE REQUIRED ONCE EVERY 10 YEARS. IF OTHER CONSTRUCTION OR RELATED ACTIVITIES ARE PERFORMED ON UPSLOPE PARCELS, ADEQUATE PROTECTION SHOULD BE PROVIDED AND INSPECTIONS PERFORMED AT LEAST ONCE WEEKLY OF THESE NEWLY DISTRIBUTED AREAS AS WELL AS INSPECTIONS FOR ACCUMULATED SEDIMENTS AT TWO BMP FACILITY.

A DESIGNATED REPRESENTATIVE OF THE OWNER WILL INSPECT THE BMP STRUCTURE AFTER EACH SIGNIFICANT RAINFALL EVENT OR THE FOLLOWING WORKING DAY IF A WEEKEND OR HOLIDAY OCCURS. A SIGNIFICANT RAINFALL FOR THIS STRUCTURE IS DEFINED AS ONE (1) INCH OR MORE OF GAUGED RAINFALL WITHIN A 24 HOUR PERIOD. ONCE PER YEAR, A REPRESENTATIVE OF THE COUNTY MAY JOINTLY INSPECT THE STRUCTURE. APPROPRIATE ACTION, PERFORMED AT THE COST OF THE OWNER, WILL BE TAKEN TO ENSURE APPROPRIATE MAINTENANCE. KEYS TO LOCKED ACCESS POINTS SHALL BE MADE AVAILABLE TO COUNTY INSPECTION PERSONNEL UPON REQUEST.

INSPECTION AND MAINTENANCE OF THE FACILITY WILL CONSIST OF THE FOLLOWING ADDITIONAL MEASURES:

1. THE INSPECTION FOR SEDIMENT BUILDUP WILL BE PERFORMED BY VISUAL INSPECTION AND A PHYSICAL DETERMINATION OF SEDIMENT DEPTH WITHIN THE STORAGE AREA. SEDIMENT REMOVAL IS REQUIRED USING A RUBBER—WHEELED BACKHOE. AT THE SAME TIME, OR AT LEAST ONCE PER YEAR, THE RISER BOTTOM AND OUTLET PIPE SHALL BE CLEANED OF ACCUMULATED SEDIMENTS. DISPOSE OF SEDIMENTS REMOVED FROM THE FACILITY AT AN ACCEPTABLE DISPOSAL AREA. SEDIMENT SHALL NOT BE ALLOWED TO ACCUMULATE IN DEPTHS GREATER THAN 1—FOOT. NO SEDIMENT SHALL BE ALLOWED TO ACCUMULATE TO PREVENT THE PROPER FUNCTION OF ANY PIPE OR CUI VERT.

2. PERFORM MAINTENANCE MOWING OF GRASSED AREAS AT LEAST TWICE EACH YEAR. GRASSES SUCH AS TALL FESCUE SHOULD BE MOWED IN EARLY SUMMER AFTER EMERGENCE OF THE HEADS ON COOL SEASON GRASSES AND IN LATE FALL TO PREVENT SEEDS OF ANNUAL WEEDS FROM MATURING. MOWING OF LEGUMES CAN BE LESS FREQUENT TREES AND SHRUBS SHOULD NOT BE PERMITTED TO GROW ON ANY PART OF THE GRADED EMBANKMENT.

3. PERFORM SOIL SAMPLING ON STABILIZED BMP SOIL AREAS ONCE EVERY FOUR (4) YEARS. SOIL SAMPLING AND TESTING SHOULD BE PERFORMED BY A QUALIFIED INDEPENDENT TESTING LABORATORY. APPLY ADDITIONAL LIME AND FERTILIZER IN ACCORDANCE WITH TEST

4. IN STABILIZED BMP AREAS, IF VEGETATION COVERS LESS THAN 40% OF SOIL SURFACES, LIME, FERTILIZE AND SEED IN ACCORDANCE WITH RECOMMENDATIONS FOR NEW SEEDLINGS, AS LISTED IN DAM CONSTRUCTION NOTES. IF VEGETATION COVERS MORE THAN 40% BUT LESS THAN 70% OF SOIL SURFACES, LIME FERTILIZE AND OVERSEED IN ACCORDANCE WITH CURRENT SEEDLING RECOMMENDATIONS.

5. PERFORM QUARTERLY INSPECTIONS OF THE RELEASE STRUCTURES, RISER SECTION AND CREST OF SPILLWAY FOR THE OBSERVANCE OF COLLECTED DEBRIS. IMMEDIATELY REMOVE ANY DEBRIS TO MAINTAIN THE INTEGRITY OF THE STRUCTURE AND PROVIDE AN ATTRACTIVE APPEARANCE. DURING QUARTERLY INSPECTIONS, THE POND DRAIN VALVE, USUALLY LEFT IN THE VALVE "CLOSED" POSITION, SHALL BE INSPECTED AND OPERATED THROUGH TWO COMPLETE FULL-OPEN TO FULL-CLOSE TO FULL-OPEN CYCLES.

6. PERFORM YEARLY STRUCTURAL INSPECTIONS OF THE FACILITY FOR DAMAGE. STRUCTURAL INSPECTION SHALL BE PERFORMED ON THE CONCRETE RISER, ANTI-VORTEX DEVICE, TRASH RACK, ORIFICE/ WEIR(S), OUTLET BARREL AND POND EMBANKMENT. IF DAMAGE IS EVIDENT, FURTHER INVESTIGATION BY A PROFESSIONAL ENGINEER MAY BE REQUIRED TO ASSESS THE CONTINUED INTEGRITY OF THE STRUCTURE.

7. PERFORM QUARTERLY INSPECTIONS OF THE GRADED SIDE SLOPES OF THE FACILITY FOR SIGNS OF ANIMAL/ RODENT BORROWS OR SLOPE EROSION. IMMEDIATELY PERFORM NECESSARY REPAIRS, REFILLING OR RESEEDING AS APPROPRIATE.

8. RECORD KEEPING. THE LANDOWNER OR DESIGNATED REPRESENTATIVE SHALL KEEP REASONABLE, ACCURATE WRITTEN RECORDS OF INSPECTIONS PERFORMED ON THE STRUCTURE. RECORDS SHALL DOCUMENT ROUTINE MAINTENANCE AND/ OR REPAIRS PERFORMED. COPIES SHALL BE PROVIDED TO

9. THE FACILITY SHALL NOT BE MODIFIED IN ANY WAY WITHOUT PRIOR CONSENT/ APPROVAL OF

# GENERAL NOTES FOR CONSTRUCTION OF STORMWATER BASINS

1. THE CONTRACTOR SHALL PROVIDE ALL WORK AND MATERIALS NEEDED TO CONSTRUCT THE STORMWATER BASIN, STORMWATER MANAGEMENT PONDS, BEST MANAGEMENT PRACTICES, SEDIMENT BASINS AND SEDIMENT TRAPS. THE WORK SHALL INCLUDE ALL LABOR, MATERIALS, EQUIPMENT AND MATERIALS NEEDED FOR THE COMPLETION OF GRADING AND EARTHWORK ASSOCIATED WITH THE

THE COUNTY UPON REQUEST.

2. THE CONTRACTOR SHALL CONSULT AND PROVIDE FOR THE SERVICES
OF A GEOTECHNICAL ENGINEER. THE GEOTECHNICAL ENGINEER SHALL
PROVIDE TEST RESULTS ON PLACED DAM MATERIALS, IDENTIFYING
SOIL CLASSIFICATION, PERMEABILITY, PLASTICITY INDEX, AND
COMPACTION. ALL TIESTS SHALL BE IN CONFORMANCE WITH ASTM
STANDARDS. THE COST OF THE SERVICES OF THE GEOTECHNICAL
ENGINEER SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR.
SATISFACTORY GEOTECHNICAL RESULTS ARE NEEDED PRIOR TO FINAL APPROVAL.

3. ALL INSPECTIONS IREQUIRED FOR THE WORK SHALL BE PERFORMED BY A GEOTECHNICAL ENGINEER AT THE EXPENSE OF THE GENERAL CONTRACTOR.

4. ON—SITE EXCAVATED MATERIAL, IF DETERMINED SUITABLE FOR USE IN DAM CONSTRUCTION BY A GEOTECHNICAL ENGINEER, MAY BE USED FOR DAM CONSTRUCTION. SHOULD ADDITIONAL MATERIAL BE REQUIRED, THE CONTIRACTOR SHALL IDENTIFY THE NEED FOR MATERIAL TO THE OWNER, AS ADDITIONAL BORROW MATERIAL MAY BE AVAILABLE ON THE PROPERTY. ALL EXCAVATED MATERIAL DETERMINED BY THE GEOTECHNICAL ENGINEER TO BE UNSUITABLE SHALL BE DISPOSED OF PROPERLY AT THE CONTRACTOR'S EXPENSE. ALL EXCAVATED MATERIAL NOT REQUIRED FOR BACKFILLING SHALL EITHER BE DEPOSITED ON SITE AND SPREAD BY THE CONTRACTOR, OR SHALL BE DEPOSITED IN AN AREA ON THE PROPERTY AS DIRECTED BY THE OWNER. THE CONTRACTOR SHALL PROVIDE PROPER STABILIZATION, AND EROSION AND SEDIMENT CONTROL MEASURES NEEDED TO CONTROL AS PER THE VESCH THIRD EDITION.

5. UNDERCUT FOR THE FOUNDATION OF THE DAM EMBANKMENT SHALL BE IN ACCORDANCE WITH THE GEOTECHNICAL ENGINEER'S RECOMMENDATION. THE FOUNDATION SHALL BE BACKFILLED WITH SOILS CLASSIFIED AS SM, SC, OR CL UNDER THE UNIFIED SOIL CLASSIFICATION SYSTEM. SOILS SHALL HAVE A MINIMUM OF 15% BY WEIGHT FINES, HAVING A PLASTICITY INDEX OF 30% AND A PERMEABILITY OF 0.0004 IN./SEC. OR LESS. FILL SHALL BE COMPACTED IN 12—INCH LIFTS, OR AS DIRECTED BY THE GEOTECHNICAL ENGINEER, TO A DRY DENSITY OF 95% OF THE STANDARD PROCTOR MAXIMUM DRY DENSITY (ASTM D-698). EXCAVATION FOR THE DAM KEY SHALL BE IN ACCORDANCE TO THE GEOTECHNICAL ENGINEER'S RECOMMENDATION. HEIGHT, DEPTH, AND WIDTH OF THE KEY SHALL BE IN ACCORDANCE WITH THE GEOTECHNICAL ENGINEER'S RECOMMENDATIONS. THE KEY SHALL BE FORMED USING SOILS CLASSIFIED AS SC OR CL, WITH A PERMEABILITY OF 0.0004 IN./SEC. OR LESS.

6. THE DAM CORE SHALL BE AS CONSTRUCTED WITH NON-EXPANSIVE SC OR CL CLAYEY MATERIAL WITH PERMEABILITY OF 0.0004 IN./SEC. OR LESS. THE FILL OF THE CORE SHALL BE MADE IN 12-INCH LIFTS, OR AS DIRECTED BY THE GEOTECHNICAL ENGINEER, TO AT LEAST 95% OF THE STANDARD PROCTOR MAXIMUM DRY DENSITY (ASTM D-698). SIZE, SHAPE, WIDTH, DEPTH, AND HEIGHT OF THE DAM CORE SHALL BE IN ACCORDANCE WITH THE GEOTECHNICAL ENGINEER'S RECOMMENDATIONS. TO COVER THE DAM CORE, A SILTY FINE SAND OR CLAYEY SOIL (SM., SC, OR CL) SHALL BE PLACED. A VEGETATIVE COVER USING VDOT EC-2 EROSION CONTROL BLANKETS SHALL BE PLACED ON DAM SLOPES AND CREST TO PREVENT EROSION.

7. THE STORMWATER MANAGEMENT / BMP FACILITIES SHOWN ON THESE PLANS REQUIRE THE SUBMISSION, REVIEW AND APPROVAL OF RECORD DRAWING(S) AND CONSTRUCTION CERTIFICATION PRIOR TO RELEASE OF THE POSTED BOND / SURETY. THE GEOTECHNICAL ENGINEER IS TO ENSURE THAT HIS / HER INSPECTION OF THE SWM / BMP CONSTRUCTION ACTIVITY IS PERFORMED DURING AND FOLLOWING CONSTRUCTION OF THE SWM / BMP IN ACCORDANCE WITH THE JAMES CITY COUNTY ENVIRONMENTAL DIVISION STORMWATER MANAGEMENT / BMP FACILITIES DESIGN GUIDELINES HANDBOOK, DATED AUGUST 30, 2000.

8. THE CONTRACTOR IS REQUIRED TO SUBMIT SPECIFICATIONS OF THE POND LINER MATERIAL THAT IS TO BE USED, IF OTHER THAN NATURAL CLAY TO THE JAMES CITY COUNTY ENVIRONMENITAL DIVISION. SYNTHETIC LINERS MUST HAVE THE APPROVAL OF THE JAMES CITY COUNTY ENVIRONMENTAL DIVISION BEFORE INSTALLATION. THE CONTRACTOR IS TO INSTALL THE SYNTHETIC LINER IN STRICT ACCORDANCE WITH THE MANUFACTURERS RECOMMENDATIONS.

4-28-05 REVISION TO SITE PLAN AMENDMENT
1-12-05 SITE PLAN AMENDMENT
10-25-04 REVISED COUNTY COMMENTS
10-11-04 REVISED COUNTY COMMENTS
9-15-04 REVISED COUNTY COMMENTS
9-55-64 AREVISED COUNTY COMMENTS
10-11-04 REVISED COUNTY COMMENTS
1-55-64 ARECHESTED COUNTY COMMENTS
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MARSTON, III ZA NO. 018232 ACTION ALL STONAL STONAL

248 Olde Towne Road, Suite Williamsburg, Virginia 23188 (757) 253-0040 Fax (757) 220-8994



BMP NOTES AND DETAILS

WINDSORMEADE MARKETPLACE

Sames CITY COUNTY VIRGINIA

WINDSORMEADE MARKETPLACE

Sames CITY COUNTY VIRGINIA

AS SHOWN 12/2/03

Project No.

9069-02

Drawing No.

# WindsorMeade Market Place

# BMP RECORD DRAWINGS

# **LEGEND**

#### PROPOSED PROPOSED WATER BLOW-OFF ASSEMBLY **GRAVITY SEWER** CLEAN OUT WATER METER GRAVITY SEWER S → S (BY OTHERS) CENTERLINE/BASELINE STORM SEWER PROPERTY LINE © DITCH/SWALE GROUND ELEVATION EXISTING CONTOUR ELEV. FIRE HYDRANT ASSEMBLY

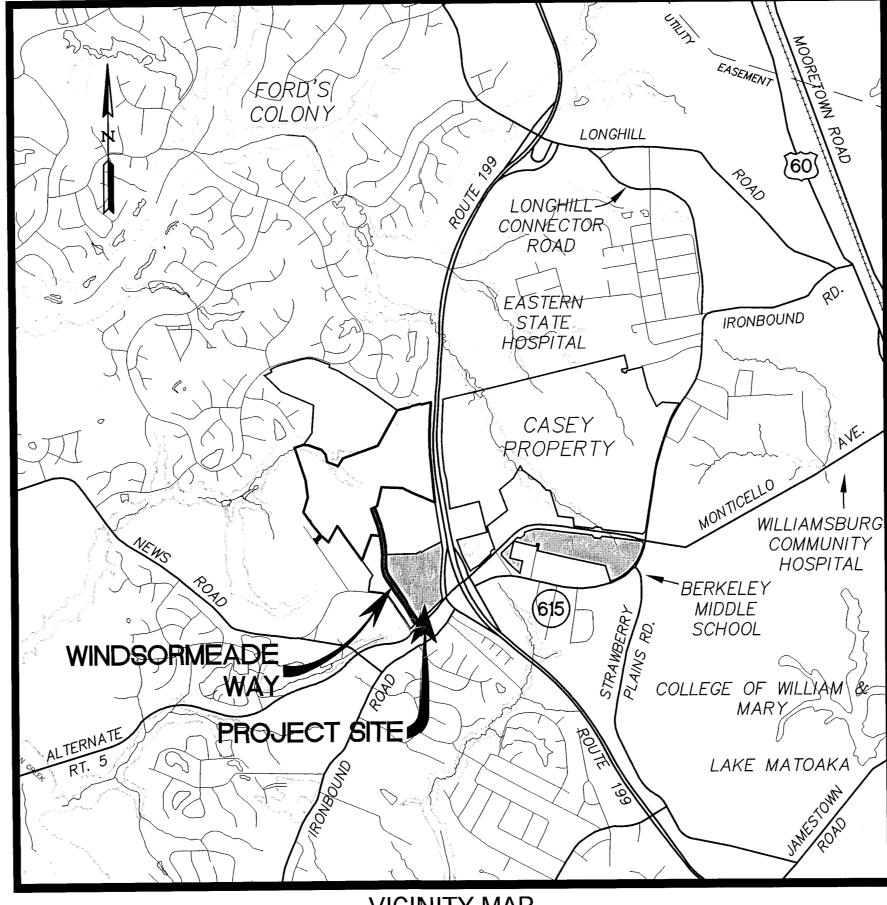
# NOTES:

THE SITE IS CURRENTLY ZONED MIXED USE WITH PROFFERS. FOR PROFFERS REFERENCE JCC CASE NO. Z-03-01 AND

- CONSTRUCTION.
- CONTRACTOR SHALL BE RESPONSIBLE FOR THE COORDINATION OF CONSTRUCTION EFFORTS WITH THE VIRGINIA POWER COMPANY, VERIZON TELEPHONE, APPROPRIATE CABLE COMPANY AND OTHERS THAT MAY BE REQUIRED.
- THE CONTRACTOR SHALL SATISFY HIMSELF AS TO ALL SITE CONDITIONS PRIOR TO CONSTRUCTION
- THE CONTRACTOR IS RESPONSIBLE FOR OBTAINING ALL NECESSARY PERMITS PRIOR TO COMMENCEMENT OF WORK TO INCLUDE, BUT NOT LIMITED TO, JAMES CITY COUNTY LAND DISTURBANCE, VDOT LAND USE PERMIT, AND ANY DEMOLITION PERMITS.
- 6. EXISTING UTILITY LOCATIONS INDICATED ARE APPROXIMATE. FIELD VERIFY PRIOR TO COMMENCING THE WORK.
- 7. ALL UTILITIES WILL BE PLACED UNDERGROUND
- 8. JCSA SHALL BE GRANTED ACCESS EASEMENTS TO WATER AND SEWER LOCATED WITHIN PRIVATE RIGHT-OF-WAYS.
- 9. A PRECONSTRUCTION CONFERENCE SHALL BE HELD ON-SITE BETWEEN THE COUNTY, THE PROJECT ENGINEERS AND THE CONTRACTOR PRIOR TO ISSUANCE OF A LAND DISTURBING PERMIT.
- 10. ALL SANITARY SEWER AND WATER DISTRIBUTION FACILITIES MUST HAVE A MINIMUM HORIZONTAL SEPARATION DISTANCE OF 5' BETWEEN IT AND ALL OTHER FIXED STRUCTURES SUCH AS: DROP INLETS, LIGHT POLES, STORM SEWER PIPES, ETC.
- 11. THE CONTRACTOR IS REQUIRED TO SECURE ALL NECESSARY PERMITS FOR FOR THE ABANDONMENT OR DEMOLITION OF ALL EXISITING WELLS/WATERLINES AND SEPTIC FIELDS IN ACCORSANCE WITH JAMES CITY COUNTY VIRGINIA DEPARTMENT OF HEALTH REGULATIONS. CONTACT VIRGINIA DEPARTMENT OF HEALTH AT 757-253-4813
- 12. VERIFY ALL DIMENSIONS AND NOTIFY JAMES CITY SERVICE AUTHORITY PRIOR TO ANY EXCAVATION OR DEMOLITION WITHIN
- 13. PARKING SPACES SHALL BE DELINEATED BY PAVEMENT STRIPING. HANDICAP PARKING. SPACES SHALL BE DESIGNATED BY ABOVE GROUND SIGNS PER USBC REQUIREMENTS.
- 14. THE TOPOGRAPHIC DATA REPRESENTED ON THIS DRAWING IS SUPPLIED BY OWNER/DEVELOPER. CONTOUR INTERVAL = 2 FEET.
- 15. ALL SECURITY LIGHTING IS TO BE LOCATED A MINIMUM OF 10' OFF THE EDGE OF PAVEMENT AND SHALL NOTE BE POSITIONED IN DITCH LINES.
- 16. ALL COMPONENTS OF THE WATER DISTRIBUTION AND SANITARY SEWER SYSTEM SHALL BE INSTALLED AND TESTED IN ACCORDANCE WITH THE LATEST EDITION OF THE AUTHORITY STANDARDS AND SPECIFICATIONS FOR WATER DISTRIBUTION AND SANITARY SEWER SYSTEMS, THE HRPDC REGIONAL STANDARDS, AND THE COMMONWEALTH OF VIRGINIA WATERWORKS AND SEWERAGE REGULATIONS. THE CONTRACTOR SHALL USE ONLY NEW MATERIALS, PARTS AND PRODUCTS ON ALL PROJECTS. ALL MATERIALS SHALL BE STORED SO AS TO ASSURE THE PRESERVATION OF THEIR QUALITY AND FITNESS FOR THE WORK. A COPY OF THE JCSA STANDARDS AND REGIONAL STANDARDS MUST BE KEPT ON-SITE BY THE CONTRACTOR DURING THE FULL TIME OF INSTALLING, TESTING, AND CONVEYING THE FACILITIES TO JCSA.
- 17. STORM STRUCTURES, SEWER AND BEDDING SHALL CONFORM TO THE VDOT ROAD AND BRIDGE STANDARDS AND VDOT SPECIFICATIONS. ALL PIPE BEDDING SHALL BE IN ACCORDANCE WITH PB-1 AND MANUFACTURER SPECS. AND GUIDELINES, AND MANHOLES DEEPER THAN 4 FEET SHALL HAVE STEPS (ST-1). ALL REINFORCED CONCRETE PIPE (RCP) SHALL BE CLASS III UNLESS OTHERWISE NOTED. STORM SEWER OUTSIDE OF VDOT R.O.W. CAN BE HIGH DENSITY POLYETHYLENE (HDPE).
- 18. ALL EXISTING STRUCTURES LOCATED ON THE SITE ARE TO BE DEMOLISHED AND WILL REQUIRE A DEMOLITION PERMIT. THIS PERMIT CAN BE ACQUIRED FROM THE JAMES CITY COUNTY CODE COMPLIANCE DEPARTMENT TELEPHONE NUMBER: 757-253- 6626
- 19. NO TREES, SHRUBS, FENCES OR OBSTACLES SHALL BE PLACED WITHIN A JCSA EASEMENT WHICH WOULD RENDER THE EASEMENT INACCESSIBLE BY EQUIPMENT. SHRUBS SHALL BE A MINIMUM OF 5 FEET, AND TREES A MINIMUM OF 10 FEET, FROM THE CENTER OF WATER AND SEWER PIPELINES.
- 20. CONTACT MR. SAL SIBILIA 72 HOURS IN ADVANCE OF ALL PAVEMENT MARKINGS/SIGN INSTALLATIONS AT (757) 925-1679.
- 21. ALL SIGNAGE SHALL BE IN ACCORDANCE WITH ARTICLE II, DIVISION 3 OF THE JAMES CITY COUNTY ZONING ORDINANCE.
- 22. OUTSIDE SALES AND STORAGE OF MERCHANDISE IS PROHIBITED.
- 23. HVAC EQUIPMENT AND OTHER UTILITIES, DOWNSPOUTS, AND GUTTERS SHALL BE PAINTED TO MATCH THE EXTERIOR COLOR OF THE BUILDING SURFACE MATERIAL COLOR. BASES OF THE LIGHT POLES SHOULD BE PINTED TO MATCH THE COLOR OF
- 24. ONLY JCSA PERSONNEL ARE AUTHORIZED TO OPERATE VALVES ON EISTING JCSA WATER MAIN.
- 25. WATER METERS MUST BE LOCATED A MINIMUM OF 2' FROM SIDEWALKS AND BACK OF CURBS AND 18" FROM EDGE OF DRIVEWAYS.
- 26. THE OWNER SHALL IMPLEMENT AN ANNUAL PERFORMANCE EVALUATION/INSPECTION OF THE BACKFLOW PREVENTION DEVICE AND COORDINATE WITH JOHN WILSON, JCSA UTILITY SPECIAL COORDINATOR, AT (757) 259-4138. THE BACKFLOW PREVENTER SHALL BE TESTED, MAINTAINED, AND OPERATED IN ACCORDANCE WITH JCSA STANDARDS.

JCC# SP-2-05 AMENDMENT TO JCC# SP-150-03

## JAMES CITY COUNTY, VIRGINIA



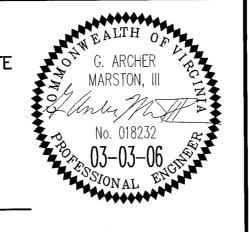
**VICINITY MAP** SCALE: 1"=2000"

DECEMBER 29, 2003 PROJECT NO.: 9069-02

SITE PLAN AMENDMENT: 1-12-05

DATE

'THE SANITARY SEWER, WATER, AND DRAINAGE STRUCTURE LOCATIONS AND GRADES SHOWN ON THESE DRAWINGS, ARE ACCURATE AND COMPLETE TO THE BEST OF MY KNOWLEDGE AND BELIEF AND I CERTIFY THAT I, OR MY AGENT, HAVE MADE SUFFICIENT INSPECTION TO ENSURE THE ACCURACY OF THIS STATEMENT."



ARCHER G. MARSTON III

**CONSULTING ENGINEERS** WILLIAMSBURG • RICHMOND

5248 Olde Towne Road, Suite 1 Williamsburg, Virginia 23188 (757) 253-0040 Fax (757) 220-8994

SITE PLAN AMENDMENT (AMENDMENT TO SP #150-03, APPROVED NOVEMBER 12, 2004)

REVISED FOOTPRINT OF BUILDING #5. ADDED A SANITARY LATERAL FOR THIS BUILDING. REVISED RELATIVE "REQUIRED" PARKING COUNTS, GRADING IN THIS AREA WAS ADJUSTED TO ACCOMODATE NEW FOOTPRINT (FIRST SUBMITTAL.) ADJUSTED 10" LOADING DOCK OUTFALL ON PLANS AND ON WATERLINE PROFILE "D" AND SANITARY PROFILE MH#7 TO MH#3 (SECOND SUBMITTAL.)

2. ADDED DUMPSTER SOUTH OF BUILDING #8. IN CONJUNCTION WITH THIS DUMPSTER, ALSO ADDED STAIRS AND A RETAINING WALL. REVISED GRADING TO ACCOMODATE DUMPSTER AND WALL (FIRST SUBMITTAL.)

3. ADDED A PRIVATE 6" FIRE LINE, A DETECTOR CHECK VALVE ASSEMBLY AND A POST INDICATOR VALVE TO BUILDING #8 AND A 4" LINE TO A FIRE SERVICE CONNECTION. ALSO ADDED A NOTE RELATIVE TO THE BACKFLOW PREVENTION AT BUILDING #8. A 4" LINE IS SHOWN ON THE SEWER LINE PROFILE ON SHEET 14. (SECOND SUBMITTAL)

4. ADDED A MONUMENT SIGN AT THE FRONT OF THE SITE (SOUTHEAST SIDE) (FIRST SUBMITTAL.)

5. REMOVED THE SMALL BUILDING ADJACENT TO THE SOUTH SIDE OF BUILDING #1 (FIRST SUBMITTAL.)

6. ADJUSTED FIRE LINE, SANITARY SEWER LATERAL AND WATER SERVICE LINE TO BETTER SERVE BUILDING 1 & 2 (FIRST

7. ADDED NOTES TO THE COVER SHEET REGARDING REVIEW OF PLANS BY THE JAMES CITY COUNTY PLANNING COMMISSION AND THE NEW TOWN DESIGN REVIEW BOARD (SECOND SUBMITTAL)

8. ADDED 10" ROOF LEADER OUTFALL PIPES UNDER FIRST SUBMITTAL OF SITE PLAN AMMENDMENT. REMOVED THESE OUTFALL

9. ADDED PRIVATE STORM DRAINAGE EASEMENTS TO THE PLANS FOR ALL MAJOR STORM SEWER CONVEYING WATER ACROSS THE SITE TO THE BMP (SECOND SUBMITTAL) ALSO INCLUDED THE NATURAL OPEN SPACE EASEMENTS ON SHEETS 3, 4 AND 6 (SECOND SUBMITTAL)

10. MODIFIED OUTFALL STONE AT BMP FROM CLASS A1 RIPRAP TO CLASS 1 RIPRAP (SECOND SUBMITTAL.)

11. ADDED INTERNAL PROPERTY LINES TO SHEETS 2, 3, 5, 6, & 7 (SECOND SUBMITTAL)

12. ADDED A POST INDICATOR VALVE TO THE 8" FIRE SERVICE WATERLINE TO THE MAINTENANCE BUILDING AT THE REAR (NORTH SIDE) OF THE SITE (SECOND SUBMITTAL)

### INDEX OF SHEETS

	IN OF OTHER TO
SHEET NO.	DESCRIPTION
<b>1</b> 2	COVER SHEET  ENVIRONMENTAL INVENTORY PLAN
3 4	OVERALL SITE LAYOUT PLAN OVERALL UTILITY PLAN
5 6 7	SITE AND UTILITY PLAN SITE AND UTILITY PLAN SITE AND UTILITY PLAN
8	BMP POND AS-BUILT
9 10 11	GRADING, DRAINAGE, AND E&S PLAN GRADING, DRAINAGE, AND E&S PLAN ROAD PLAN
12 13 14 15	EROSION & SEDIMENT CONTROL PLAN—PHASE I WATER & SEWER PROFILES WATER & SEWER PROFILES WATER LINE PROFILES
16 17 <b>18</b> 19	NOTES & DETAILS NOTES & DETAILS BMP NOTES & DETAILS LIGHTING PLAN

#### OWNER INFORMATION:

C.C. CASEY, LTD. CO. 721 RICHMOND ROAD WILLIAMSBURG, VIRGINIA. 23185-3541 TELEPHONE: (757) 229-3702

#### **DEVELOPER INFORMATION:**

SLN WILLIAMSBURG ASSOCIATES, L.L.C. 9211 FOREST HILL AVENUE, SUITE 110 RICHMOND, VIRGINIA. 23235 CONTACT: JIM GRESOCK TELEPHONE: (804) 320-7600 FAX: (804) 330-8924

#### CERTIFIED RESPONSIBLE LAND DISTURBER:

AES CONSULTING ENGINEERS 5248 OLDE TOWNE ROAD, SUITE 1 WILLIAMSBURG, VIRGINIA. 23188 TELEPHONE: 757-253-0040

#### SITE DATA:

(38-3)(1-02), (38-3)(1-34), (38-3)(1-07)TAX MAP PARCEL No. (38-3)(1-05), (38-3)(1-06), (38-3)(1-08)MU (MIXED USE) WITH PROFFERS 1,369,671 S.F.± 31.44 AC.± 100.00 % TOTAL PROJECT AREA: 49.40 % 15.53 AC IMPERVIOUS AREA: 50.60 % 15.91 AC GREEN SPACE: 1,087,693 S.F.± 24.97 AC.± DISTURGED AREA: FEMA PANEL NUMBER 510201 0035 B, DATED 2/6/91 FLOOD HAZARD MAP: NOTE: SITE IS LOCATED IN ZONE 'X' (AREAS DETERMINED TO BE OUTSIDE THE 500 YEAR FLOOD PLAIN)

COUNTY WATERSHED:

THIS PROJECT IS SITUATED IN SUBWATERSHEDS 209 AND 210. COUNTY CATCHMENTS ARE 209-101-1 AND 210-202-1 OF THE POWHATAN CREEK WATERSHED.

THIS PLAN WAS REVIEWED ON FEBRUARY 2, 2004 BY JAMES CITY COUNTY PLANNING COMMISSION IN ACCORDANCE

WITH SECTION 24-147 (a)(1)(d) OF ZONING ORDINANCE THE PROPOSED AMENDMENTS OF THIS PLAN WERE REVIEWED BY THE NEW TOWN DESIGN REVIEW BOARD AT A MEETING ON

		DEVISION / COMMENT / NOTE	RY
1	04/09/04	ADDRESSED COUNTY COMMENTS	AES
2	07/09/04	ADDRESSED COUNTY COMMENTS	AÉS
3	09/15/04	REVISED COUNTY COMMENTS	AES
4	10/11/04	REVISED COUNTY COMMENTS	AES
5	10/25/04	REVISED COUNTY COMMENTS	AES
$\Lambda$	1/12/05	SITE PLAN AMENDMENT	AES
/2\	4/28/05	REVISION TO SITE PLAN AMENDMENT	AES

RECORD DRAWING.: 3/1/2006 No. | DATE